HOPPING GREEN SAMS & SMITH

AND STREET date and an in the second ANTHOUGH NULLIZARD NICHARD & BRIGHTRAM HE WIN IN CONTRACTOR FETER C CONVINCMENT DALTH & DIMED INCHAS N. DINGSE NANDOLPH M GIDDINGS RILLIAN IN GREEN EINERBURG, GHIPPA RADE - HOPPING CARP'S HUNTER, .... Chatman 1. JOHNSON DEBENT A. MANNING FIRAL T MATTERS 11 C (A H 2) 21 H 3 ( 1 1 1 1 1

ATTORNEYS AND COUNSELORS

POST OFFICE HOA 6526

TALLAHASSEE, FLORIDA 32314

1850-222 1500

FAX (850) 224 8551 FAX (850) 425 3415

Writer's Direct Dial No. (904) 425-2313

October 1, 1998



OF COUNTER AMAN

× 11

Ms. Blanca S. Bayó Director, Records and Reporting Florida Public Service Commission 2540 Shumard Oak Boulevard Tallahassee, FL 32399-0850

> Re: Determination of Cost of Local Service --Docket No. 980696-TP Revised Rebuttal Testimony of James W. Wells, Jr.

Dear Ms. Bayó:

RECHIVED & FILED

AU OF RECORDS

Parties of Record

ACK

AFA

APP

CAF

CU

617

LE .

LIN OF C

RCH .....

SEC 1

OTH \_

WAS \_\_\_\_\_

EA

d

RDM/mee

d-cc:

Storp

Enclosures

Enclosed for filing on behalf of MCI Telecommunications Corporation and MCImetro Access Transmission Services, Inc. (colletively "MCI") are the original and fifteen REVISED copies of the redacted rebuttal testimony and exhibits of James W. Wells, Jr.

When MCI originally filed Mr. Wells' testimony and exhibits on September 2, 1998, it mistakenly redacted a substantial amount of information for which no party has claimed confidentiality.

The enclosed filing corrects this error. Please substitute this document for the testimony and exhibits previously filed. I / apologize for any inconvenience we have caused.

Very truly yours, 40

Richard L. Melson

DOCUMENT AT MOTR-DATE

40831 OCT-18

DAT 14 THE REPORT NO



### BEFORE THE

## FLORIDA PUBLIC SERVICE COMMISSION

# REBUTTAL TESTIMONY OF

JAMES W. WELLS, JR.

### ON BEHALF OF

## MCI TELECOMMUNICATIONS CORPORATION

Docket No. 980696-TF

September 2, 1998

## (REDACTIONS REVISED 10/1/98)

DOCUMENT NUMBER-DATE

#114962 v1 - MCI USF Wells Revised Rebuttal (Reducted)

FPSC-RECORDS/REPORTING

| 1  | I.   | INTRODUCTION  |
|----|------|---|
| 2  | Q.   | PLEASE STATE YOUR NAME AND BUSINESS ADDRESS.  |
| 3  | Α.   | My name is James W. Wells, Jr., and my office address is 5280 Laithbank Lane,             |
| 4  |      | Alpharetta, GA 30022  |
| 5  |      |   |
| 6  | Q.   | BY WHOM AND IN WHAT CAPACITY ARE YOU EMPLOYED?  |
| 7  | Α.   | I am the President of J. W. Wells, Inc. In this proceeding, I am providing                |
| 8  |      | consulting expertise in telecommunications Outside Plant ("OSP") infrastructure           |
| 9  |      | planning, design and construction, including costing aspects of the local loop.           |
| 10 |      |   |
| 11 | Q.   | ON WHOSE BEHALF ARE YOU TESTIFYING?   |
| 12 | Α.   | I am testifying on behalf of MCI Telecommunications Corporation.                          |
| 13 |      |   |
| 14 | п.   | PURPOSE   |
| 15 | Q.   | WHAT ARE THE PURPOSES OF YOUR TESTIMONY?  |
| 16 | Α.   | The purposes of my testimony are to:  |
| 17 |      | <ul> <li>analyze the OSP input values of the Incumbent Local Exchange Carriers</li> </ul> |
| 18 |      | ("ILECs") in comparison to those of AT&T/MCI,   |
| 19 |      | · examine the OSP modeling methodology and assumptions of the                             |
| 20 |      | Benchmark Cost Proxy Model Release 3.1 ("BCPM 3.1") in comparison                         |
| 21 |      | to those of the HAI Model Release 5 0a ("HM 5 0a"), formerly known as                     |
| 22 |      | the Hatfield Model, and   |
| 23 |      | · rebut specific OSP portions of the direct testimonies of the ILEC                       |
| 24 |      | witnesses.  |
|    | REDA | CTED.DOC Page 2   |

A Part - Low Bar

| 1  |      |   |
|----|------|---|
| 2  | Q.   | HAVE YOU PROVIDED OTHER TESTIMONY IN THIS                                       |
| 3  |      | PROCEEDING?   |
| 4  | A.   | Yes. I filed direct testimony in this proceeding.                               |
| 5  |      |   |
| 6  | ш.   | <b>QUALIFICATIONS AND EXPERIENCE</b>  |
| 7  | Q.   | PLEASE STATE YOUR EDUCATIONAL BACKGROUND AND OSP                                |
| 8  |      | WORK EXPERIENCE.  |
| 9  | Α.   | I have Bachelor of Engineering (Electrical Engineering) and Master of Business  |
| 10 |      | Administration degrees and certification as a Project Management Professional 1 |
| п  |      | have gained OSP experience in the following assignments with:                   |
| 12 |      | South Central Bell Telephone Company (now BellSouth) in Birmingham,             |
| 13 |      | AL: OSP Construction Foreman - 1 year, OSP Facilities Engineer - 4              |
| 14 |      | years, OSP Planning Engineer - 2 years,   |
| 15 |      | • Western Electric and AT&T Network Systems (now Lucent                         |
| 16 |      | Technologies): Technical Representative for OSP Products - 5 years and          |
| 17 |      | District Manager - OSP Engineering and Construction - 5 years,                  |
| 18 |      | AT&T Local Infrastructure and Access Management: District Manager               |
| 19 |      | OSP Engineering and Construction - 1 year,                                      |
| 20 |      | AT&T Local Services Division District Manager Outside Plant Cost                |
| 21 |      | Engineering - 1 year, and   |
| 22 |      | <ul> <li>J. W. Wells, Inc.: OSP Consultant – 2 months.</li> </ul>               |
| 23 |      |   |
| 24 | IV.  | SYNOPSIS  |
|    | REDA | CTED.DOC Page 3   |

| 1  | Q. | HOW DOES YOUR TESTIMONY FIT INTO THE OVERALL CASE?                                    |
|----|----|---|
| 2  | A. | My area of expertise is the OSP portion of the local loop, which is the network       |
| 3  |    | infrastructure from the main distributing frame in the wire center to the network     |
| 4  |    | interface device at the customer's premise. My testimony is complemented by the       |
| 5  |    | testimonies of:   |
| 6  |    | <ul> <li>Mr. Don Wood, which addresses the HM 5.0a methodology, design and</li> </ul> |
| 7  |    | several of the inputs, and  |
| 8  |    | <ul> <li>Mr. Brian Pitkin, which addresses the overall BCPM 3.1.</li> </ul>           |
| 9  |    |   |
| 10 | Q. | WOULD YOU PLEASE PROVIDE AN OVERVIEW OF YOUR  |
| 11 |    | CONCERNS REGARDING THE BCPM 3.1?  |
| 12 | A. | I have reviewed the OSP portions of the prefiled direct testimonies of the ILEC       |
| 13 |    | witnesses in this proceeding and the BCPM 3.1 Model Methodology (April 30,            |
| 14 |    | 1998 Edition). I have also participated in workshops where ILECs have                 |
| 15 |    | presented the BCPM. In Release 3.1, the BCPM modelers have taken steps to             |
| 16 |    | evolve their model by incorporating several of the concepts of earlier releases of    |
| 17 |    | the Hatfield Model plus some additional ideas to improve the accuracy and cost        |
| 18 |    | efficiency of their local loop model. However, upon thorough investigation, I         |
| 19 |    | have found that in the actual implementation of these ideas the BCPM 3.1 still        |
| 20 |    | falls well short of being the least-cost, most-efficient, forward-looking and         |
| 21 |    | reasonable local loop cost model based on currently available technology in the       |
| 22 |    | following ten areas:  |
| 23 |    | · The input values filed by BellSouth, GTE and Sprint vary widely, and in             |
| 74 |    | numerous instances the II ECs have utilized unreasonable OSP input                    |

24 numerous instances the ILECs have utilized unreasonable OSP input

| 1  |             | values. The OSP input values filed by AT&T/MCI for the HM 5.0a in        |
|----|-------------|--|
| 2  |             | this proceeding will be shown to be reasonable by comparison.            |
| 3  |             | The ILEC witnesses make misleading claims of superior transmission       |
| 4  |             | quality based on adhering to the constraints of the Carrier Serving Area |
| 5  |             | ("CSA") Concept. However, BCPM 3.1 very clearly does not adhere to       |
| 6  |             | those constraints. Both models appropriately design distribution to a    |
| 7  |             | maximum length of 18,000 feet from the Digital Loop Carrier Remote       |
| 8  |             | Terminal ("DLC RT") by employing range extension cards as required.      |
| 9  |             | BCPM 3.1 now models customer locations to the much smaller Census        |
| 10 |             | Block ("CB") level instead of the Census Block Group ("CBG") level.      |
| 11 |             | However, the HM 5.0a employs a superior customer location                |
| 12 |             | methodology to BCPM 3.1 in that it models most customer locations        |
| 13 |             | (70% for Florida) far more precisely by latitude and longitude geocoding |
| 14 |             | of their addresses. The remaining customers are located by HM 5.0a at    |
| 15 |             | the CB level of precision, which is the maximum level of precision that  |
| 16 |             | BCPM 3.1 attains for any customer. More precise customer location        |
| 17 |             | produces a more accurate and cost efficient network design               |
| 18 |             | BCPM 3.1 arbitrarily segments natural clusters of customers (i.e.,       |
| 19 |             | customers located in the same neighborhood or town) based on a fixed     |
| 20 |             | grid overlay. However, HM 5.0a clusters customers based on their         |
| 21 |             | proximity to each other and transmission design rules, which is what an  |
| 22 |             | OSP Engineer would realistically do in designing a least-cost local loop |
| 23 |             | network.   |
| 24 | •           | The BCPM 3.1 overstates costs because it models an excessive number of   |
| 25 |             | DLC RTs in locations serving geographical areas and numbers of           |
|    | REDACTED.DC | Page 5   |

customers that are far too small for a least-cost model DLC RT locations are costly, and thus it is more cost effective to fully utilize the capacity and transmission capabilities of currently available DLC systems, which is exactly what HM 5.0a does.

- BCPM 3.1 does not perform a quality check to determine if a loop
   exceeds 18,000 feet in length from the DLC RT. This is important
   because when a loop exceeds 18,000 feet, the quality of voice grade
   becomes substandard. In Florida and other states, the BCPM 3.1 has
   indeed modeled customer locations that are more than 18,000 feet from
   the DLC RT. By way of comparison, HM 5.0a performs a quality test to
   assure that none of the loops it models exceed this limit.
- BCPM 3.1 uses a fixed copper/fiber breakpoint and also automatically
   deploys fiber feeder and DLC for grids where customer demand exceeds
   the capacity of a single copper cable. However, fiber with DLC is clearly
   not the economical alternative to copper feeder cables for short loops.
   HM 5.0a methodology is far superior in its use of dynamic selection of
   copper versus fiber feeder based upon comparative life cycle economics
   of these two alternatives.
- BCPM 3.1 still overstates distribution cable length and cost by modeling
   square lots even though it is clearly more economical and realistic for
   cities and subdivisions to be modeled based on rectangular lots. The HAI
   Model has always been more real world and cost efficient in its modeling
   of 1 wide by 2 deep rectangular lots.
- 24

1

2

3

4

The BCPM 3.1 modeling methodology oversizes distribution cables by:

REDACTED.DOC

Page 6

「「「「「「」」」」

| 1    | 1. first sizing for the ultimate demand by providing up to two copper   |
|------|---|
| 2    | cable pairs to all houses, including empty houses;                      |
| 3    | 2. then increasing the ultimate number of pairs required by a cable     |
| 4    | sizing factor; and  |
| 5    | 3. finally rounding up this double inflated pair requirement to the     |
| 6    | next largest discrete cable size.                                       |
| 7    | • The BCPM 3.1 has three significant, but rather arbitrary, OSP network |
| 8    | design assumptions which cannot be readily subjected to sensitivity     |
| 9    | analysis because they are only user adjustable via the cumbersome and   |
| 10   | time consuming preprocessing application. These assumptions are:        |
| 11   | 1. The maximum threshold of 999 lines for determining Carrier           |
| 12   | Serving Area size.  |
| 13   | 2. The distance of 10,000 feet from the wire center in every feeder     |
| 14   | route in the state of Florida as being the appropriate distance         |
| 15   | where it is economical and feasible to split a feeder route. Also,      |
| 16   | this is the arbitrary distance from every wire center where the         |
| 17   | spacing of lateral subfeeder routes suddenly goes from                  |
| 18   | approximately every 1,600 feet to approximately every 13,000            |
| 19   | feet.   |
| 20   | 3. The sizing of the road reduced area in the distribution quadrant     |
| 21   | based on a 500-foot buffer along each side of the roads within that     |
| 22   | distribution quadrant.  |
| 12-2 |   |

23

Page 7

1

| 1  |    | As will be demonstrated in much greater detail in the remainder of this rebuttal   |
|----|----|--|
| 2  |    | testimony, the HM 5.0a is clearly the most appropriate model for determining the   |
| 3  |    | cost of the local loop network in Florida based on the relevant criteria of being: |
| 4  |    | <ul> <li>reasonable,</li> </ul>  |
| 5  |    | <ul> <li>least-cost,</li> </ul>  |
| 6  |    | <ul> <li>most-efficient, and</li> </ul>  |
| 7  |    | <ul> <li>based on currently available technology.</li> </ul>                       |
| 8  |    |  |
| 9  | v. | CONCERNS REGARDING THE OSP PORTION OF BCPM 3.1                                     |
| 10 | Q. | WHAT CONCERNS DO YOU HAVE REGARDING THE OSP INPUT                                  |
| 11 |    | VALUES FILED BY THE ILECs?   |
| 12 | Α. | My analysis of the OSP input values filed by BellSouth, GTE, Sprint and            |
| 13 |    | AT&T/MCI in this proceeding contradicts the following three representations        |
| 14 |    | generally promoted by the ILECs:   |
| 15 |    | 1. The ILECs somehow possess the only true knowledge of local loop                 |
| 16 |    | network costs in Florida and have also figured out how to appropriately            |
| 17 |    | apply their cost data to a bottoms-up model.                                       |
| 18 |    | 2. Because an input value reflects the ILEC's actual experience in its service     |
| 19 |    | territory, it is therefore indisputably the least-cost, most-efficient input       |
| 20 |    | value.   |
| 21 |    | 3. HM 5.0a is populated with unrealistic and low input values because the          |
| 22 |    | HAI OSP Engineering Team developed these input values on a national                |
| 23 |    | basis.   |
| 24 |    |  |

Page 8

| 1  | ILECs have been building local loop networks for decades and do indeed have a               |     |
|----|---|-----|
| 2  | great deal of data and experience with studies that perform top-down allocations            |     |
| 3  | of the embedded costs in their local loop networks which have been deployed                 |     |
| 4  | under rate base regulation However, BellSouth, GTE and Sprint are clearly                   |     |
| 5  | grappling with how to utilize a bottoms-up, forward-looking, least-cost, most-              |     |
| 6  | efficient model for a local loop network based on currently available technology            |     |
| 7  | under a "scorched node" assumption.   |     |
| 8  |   |     |
| 9  | Q. HAVE YOU COMPARED THE INPUT VALUES PROPOSED BY THE                                       |     |
| 10 | ILECs FOR BCPM 3.1 WITH THOSE OF HM 5.0a?   |     |
| 11 | A. Yes. This docket has created yet another opportunity for a side-by-side                  | NS. |
| 12 | comparison of input values for the same model in the same state in the same time            | 8   |
| 13 | frame from three independent ILECs. The following analysis will once again                  | 8   |
| 14 | show that:  |     |
| 15 | <ul> <li>There are a number of significant differences among the input values of</li> </ul> |     |
| 16 | the three ILECs for the same item.  |     |
| 17 | <ul> <li>ILECs have adopted the BCPM national default input values for several</li> </ul>   |     |
| 18 | items rather than determine their Florida-specific input values.                            |     |
| 19 | <ul> <li>In many areas there is a great deal of consistency between the input</li> </ul>    |     |
| 20 | values of the ILECs and AT&T/MCI.   |     |
| 21 | <ul> <li>In several instances, the input values of AT&amp;T/MCI to HM 5.0a are</li> </ul>   |     |
| 22 | significantly more costly than the same input value for the ILECs to                        |     |
| 23 | BCPM 3.1 because they reflect real world OSP Engineering judgment                           |     |
| 24 | <ul> <li>There are several major differences between the input values of</li> </ul>         | 52  |
| 25 | AT&T/MCI to HM 5.0a and the input values of the ILECs to BCPM 3.1                           |     |
|    | REDACTED.DOC Page   | 9   |
|    |   |     |

| 1        | in those areas where there are significantly differing modeling                              |
|----------|--|
| 2        | assumptions.   |
| 3        | <ul> <li>There are numerous examples of ILEC incorrect and illogical input values</li> </ul> |
| 4        | having been derived by top-down accounting methods absent direction, or                      |
| 5        | at least a reasonableness check, by OSP Engineers.   |
| 6        | <ul> <li>There appears to be no consistent patterns in these differences.</li> </ul>         |
| 7        |  |
| 8        | Thus, there is no substantiation to representations that ILEC input values are               |
| 9        | always the correct values and HM 5.0a input values always drive unreasonably                 |
| 10       | low costs. My conclusions are based on a side-by-side comparison of the                      |
| 11       | national default input values for the BCPM 3.1, with the BCPM 3.1 input values               |
| 12       | filed by BellSouth, Sprint and GTE on August 3, 1998, and the AT&T/MCI                       |
| 13       | input values to the HM 5.0a in this proceeding. This comparison is detailed in               |
| 14       | the attached Exhibit(JWW-4). The following are examples of some of the                       |
| 15       | analysis of these input values by category:  |
| 16       |  |
| 17       | Pole Costs: The input value comparison for the per unit installed cost of a pole             |
| 18       | with anchors and guys in density zone 650 - 850 is:  |
| 19       |  |
| 20<br>21 | BCPM 3.1<br>Default BellSouth Sprint GTE HM 5.0a   |
| 22       | \$775.20 \$406.77 \$596.14 \$801.11 \$417.00   |
| 23       | THE FRANKS, HERMAN, DEPARTURE (HERMAN), S.S. HERMAN,   |
| 24       | There is no explanation as to why GTE's input value is 96.9% higher than                     |
| 25       | BellSouth's for Florid <sub>4</sub> -specific installed pole cost. GTE used a mix of 30-foot |
|          |  |
|          |  |

non-shared poles and 40-foot shared poles. However, Sprint appears to have
 used only 45- foot poles, which are too tall and much too costly, especially for
 approximately half of the poles that Sprint does not share. There are obviously
 major inconsistencies among the ILECs on how to properly model and cost poles
 using BCPM 3.1.

7 The relevant question is "What is a reasonable input value in Florida for pole costs?" For a benchmark, the Federal Communications Commission ("FCC") has 8 9 gathered pole cost data from the ILECs regarding material and labor costs for 10 40-foot class 4 poles, which is summarized in Exhibit (JWW-2) of my Direct 11 Testimony in this proceeding. Even though it adds costs, HM 5.0a utilizes only 12 40-foot class 4 poles in order to accommodate sharing on any pole. However, 13 there is very little supporting documentation to ascertain the size and class of the 14 pole(s) being modeled by the ILECs or any underlying data regarding how pole 15 costs were derived or may have been validated.

16

6

The total pole costs submitted to the FCC for Florida were BellSouth - \$410.46,
 Sprint - \$270.00 and GTE - \$440.04. Note that the input values filed by Sprint
 and GTE in this proceeding are considerably higher.

20

The unweighted arithmetical mean of the FCC pole cost data is \$500.75 nationwide and \$373.49 for the three Florida ILECs. The nationwide median cost is \$422.14. Therefore, my conclusion is that the input value for pole costs for HM 5.0a of \$417.00 (even though it is indeed a national default value) is

#### REDACTED.DOC

actually quite reasonable for Florida based on the ILEC data collected by the FCC and the Florida-specific costs filed by BellSouth.

<u>Buried Distribution Structure</u>: The input value comparisons for normal buried
 distribution structure cost in density zone 0 - 5, which is the most rural and
 therefore most critical in this Universal Service Fund (USF) case, and the most
 urban density zone of 10,000 + are:

| e<br>10 | Density<br>Zone | BCPM 3.1<br>Default | BellSouth | Sprint  | GTE    | <u>HM 5.0a</u> |
|---------|-----------------|---------------------|-----------|---------|--------|----------------|
| 21      | 0 - 5           | \$ 1.47             | \$ 3.19   | \$ 2.31 | \$1.47 | \$ 1.77        |
| 12      | 10000+          | \$ 8.84             | \$ 7.77   | \$ 2.85 | \$8.84 | \$45.00        |

13

8

1

2

3

GTE has utilized BCPM national default values rather than its Florida-specific costs for burying cable, even though it is local contractors that typically bury cables. BellSouth's buried distribution structure cost in the lowest density zone (0 - 5), where USF funding is most applicable, is overstated by at least 75%.

18

BellSouth has not figured out how to, or for other reasons has chosen not to,
differentiate buried cable structure costs by type for input into the BCPM 3.1
bottom-up model. Specifically, BellSouth has filed the same cost of \$3.06 per
foot for plow, rocky plow, trench and backfill, rocky trench, backhoe trench and
hand dig for each density zone. This is simply wrong. It cost much less per foot
to plow cable than it does to trench and backfill.

25

REDACTED.DOC

Sprint has also made this same erroneous simplification in Florida, though it was
 able to provide costs specific to each type of buried cable trench in another state.
 However, it should be possible to derive these differing costs by type of buried
 structure from the ILEC's contracts.

The consequences of this inability, or refusal, of the ILECs to differentiate their 6 buried structure costs are profound in the most rural density zone where the USF 7 Fund would be applied. The reason is that the predominant method of burying 8 cable in rural areas is plowing (e.g., 96% in BellSouth's filing, Bates Stamp 9 000196), and plowing is by far the least costly of the BCPM 3.1 buried structure 10 11 types. Thus, ILEC buried cable structure costs are substantially overstated in 12 rural areas because the average cost for buried cable structures of all types of placing methods has been used as the input value. 13

14

5

15 Note that the HM 5.0a input value in this comparison is inside the range of the ILECs in the lowest density zone. However, in the most urban density zone, the 16 HM 5.0a input value is far more costly than the three ILECs. This is because the 17 18 HAI Model OSP Engineering Team has more reasonably determined that there are much higher costs for burying cable when the density is more than 10,000 19 20 lines per square mile. This is just one clear demonstration that the HM 5.0a input 21 values are more realistic and have not been derived to produce unreasonably low 22 costs for the local loop network.

23

Further analysis of the ILEC input values for below ground structure shows that
 BellSouth's buried and underground structure costs in density zone 10,000+ are
 REDACTED.DOC

| 1  | illogically lower than the same costs in density zones $2,550 - 5,000$ and $5,000 - $ |
|----|---|
| 2  | 10,000. It certainly appears that BellSouth has made input value entry errors         |
| 3  | which overstate structure costs in density zones 2,550 - 5,000 and 5,000 -            |
| 4  | 10,000. Also, Sprint's underground structure costs are approximately 10% less         |
| 5  | than its buried structure costs in each density zone. This is illogical because a     |
| 6  | conduit trench is wider than a buried cable trench, and the trench depth should be    |
| 7  | comparable.   |
| 8  |   |
| 9  | These few examples clearly demonstrate that the ILECs are using accountants to        |
| 10 | unrealistically spread ILEC top-down cost data for input into the bottom-up           |
| 11 | BCPM 3.1 without applying the judgment of OSP Engineers. Furthermore, it is           |
| 12 | apparent that even with access to the same pool of OSP Contractors in Florida         |
| 13 | that Sprint models buried cable structure at less than half the cost of BellSouth.    |
| 14 |   |
| 15 | Underground Feeder Structure: The input value comparisons for underground             |
| 16 | feeder structure cost in density zone 0 - 5 and the two most urban density zones      |
| 17 | are:  |
| 18 | Density BCPM 3.1  |
| 19 | Zone Default BellSouth Sprint GTE HM 5.0a   |
| 20 | 0-5 \$ 2.76 \$ 8.51 \$ 2.02 \$ 2.76 \$10.29   |
| 21 | 5000 -10000 \$ 8.22 \$16.51 \$ 2.58 \$ 8.22 \$50.10                                   |
| 22 | 10000+ \$ 8.84 \$14.88 \$ 2.58 \$ 8.84 \$75.00  |
| 23 |   |
| 24 | Since the ILECs have access to the same pool of contractors in Florida who            |
| 25 | place underground structure, why would BellSouth's costs for placing                  |

underground structure in the most rural density zone be more than four times that 1 of Sprint? In going from the 5,000 - 10,000 density zone to the 10,000+ density 2 zone, the HM 5.0a input value increases by 49.7%, GTE's input value (i.e., the 3 BCPM national default value) increase by 7.5%. Sprint's input value remains 4 constant, but the BellSouth input value inexplicably drops by 9.9%. 5 6 Unfortunately, there is no supporting ILEC documentation (e.g., the HM 5.0a Inputs Portfolio) that would help to explain such huge discrepancies. 7 8 The HM 5.0a input values in the urban area are far more costly compared to 9 10 those of the three ILECs. This is because the HAI Model OSP Engineering 11 Team has more reasonably determined that there are extra costs for placing 12 conduit when the density is more than 5,000 lines per square mile. This clearly 13 shows again that the HM 5.0a inputs have been derived from realistic OSP 14 Engineering judgment and certainly do not produce unreasonably low costs. 15 16 Note also that GTE's input values for both buried cable and for underground 17 conduit structure in the three highest density zones are identical to each other (Exhibit \_\_\_\_ (JWW-4), Pg. 1). However, the cost for underground conduit 18 structure should definitely be higher than for buried structure because it takes a 19 wider trench for conduit placement, plus several other cost in general 20 21 Conduit: The input value comparison for the material cost of 4-inch conduit is: 22 23 BCPM 3.1 24 25 Default BellSouth Sprint GTE HM 5.0a

REDACTED.DOC

| 1        | \$0.83 \$2.24 \$0.73 \$1.39 \$0.60  |
|----------|---|
| 2        |   |
| 3        | The HM 5.0a Inputs Portfolio shows validation data ranging from \$0.52 to             |
| 4        | \$0.65, which supports the HM 5.0a input value of \$0.60. However, BellSouth's        |
| 5        | input value of \$2.24 per foot for 4-inch conduit purchased in large quantities is at |
| 6        | least 150% too high. Once again, however, there is no ILEC supporting                 |
| 7        | documentation to explain why Sprint can obtain 4-inch conduit at a much more          |
| 8        | reasonable cost than BellSouth or GTE in Florida.                                     |
| 9        |   |
| 10       | Structure Sharing (% Paid by Telco) - Aerial: The input value comparisons for         |
| 11       | the sharing of aerial structure (after weighting for poles, anchors and guys) in the  |
| 12       | most rural and most urban density zones are:  |
| 13       |   |
| 14<br>15 | Density BCPM 3.1 HM 5.0a<br>Zone Default BellSouth Sprint GTE Model                   |
| 16       | 0 - 5 56.45% 45.70% 46.89% 55.11% 50.00%  |
| 17       | 10000+ 60.53% 49.60% 55.48% 55.11% 25.00%   |
| 18       |   |
| 19       | There is consistency among all input values in the most rural density zone.           |
| 20       | However, HM 5.0a shows considerably more structure sharing (i.e., a lower             |
| 21       | percentage prid by the telephone company) in the urban area than in the rural         |
| 22       | area. This is because there are, and certainly will be in the future, more utilities  |
| 23       | to share with in the urban area than in the rural area. The ILECs, on the other       |
| 24       | hand, have modeled little difference in the sharing in the urban area than the rural  |
|          |   |

| 1       | area. There is no supporting documentation to explain the ILEC's modeling        |
|---------|--|
| 2       | logic, which appears lacking in sound OSP Engineering judgment.                  |
| 3       |  |
| 4       | Structure Sharing (% Paid by Telco) - Buried Distribution Cable and              |
| 5       | Underground Feeder Conduit: The input value comparisons for the percentage       |
| 6       | paid by the telephone company for underground feeder structure in the most       |
| 7       | urban density zones are:   |
| 8       |  |
| 9<br>10 | Type of Density BCPM 3.1<br>Structure Zone Default BellSouth Sprint GTE HM 5.0a  |
| 10      | Structure Zone Default BellSouth Sprint GTE HM 5.0a                              |
| 11      | Buried Dist 10000+ 80.0% 96.0% 99.9% 100.0% 33.00%                               |
| 12      | UG Feeder 10000+ 85.0% 99.0% 95.0% 97.2% 33.00%                                  |
| 13      |  |
| 14      | These input values represent a most significant difference of OSP Subject Matter |
| 15      | Expert opinion regarding least-cost, most-efficient, forward-looking modeling of |
| 16      | the local loop network. In the most urban areas for below ground structures, the |
| 17      | forward-looking view of the HAI Model OSP Engineering Team is that the           |
| 18      | telephone company will be able to share underground costs with two other         |
| 19      | utilities on the average (HM 5.0a IP, App. B).                                   |
| 20      |  |
| 21      | In sharp contrast, BellSouth, GTE and Sprint foresee virtually zero amounts of   |
| 22      | sharing. However, the Lucent (formerly AT&T) OSP Engineering Handbook            |
| 23      | that "reflects standard engineering guidelines" supposedly modeled by BCPM 3.1   |
| 24      | (Bowman Direct, Pg. 7) states that "[i]n areas where both power and telephone    |

| 1        | utilities plan to bury their facilities, a joint trench is usually advantageous"     |  |  |  |  |  |  |  |  |  |
|----------|--|--|--|--|--|--|--|--|--|--|
| 2        | (Bowman Direct, Exhibit RMB 3, Pg. 5).   |  |  |  |  |  |  |  |  |  |
| 3        |  |  |  |  |  |  |  |  |  |  |
| 4        | The ILECs' viewpoint in regards to virtually zero below ground structure sharing     |  |  |  |  |  |  |  |  |  |
| 5        | is based on backward-looking, embedded network experience and is totally             |  |  |  |  |  |  |  |  |  |
| 6        | unreasonable for a least-cost, most-efficient, forward-looking model In a            |  |  |  |  |  |  |  |  |  |
| 7        | competitive environment, telephone companies will seek to lower their costs by       |  |  |  |  |  |  |  |  |  |
| 8        | sharing structure costs with other utilities. In a forward-looking environment,      |  |  |  |  |  |  |  |  |  |
| 9        | there will also be additional utilities out there that will be more willing to share |  |  |  |  |  |  |  |  |  |
| 10       | structure costs.   |  |  |  |  |  |  |  |  |  |
| 11       |  |  |  |  |  |  |  |  |  |  |
| 12       | Pole Spacing: The input value comparisons for pole spacing in the most rural         |  |  |  |  |  |  |  |  |  |
| 13       | and urban density zones are:   |  |  |  |  |  |  |  |  |  |
| 14       |  |  |  |  |  |  |  |  |  |  |
|          | IN COMPANY OF A  |  |  |  |  |  |  |  |  |  |
| 15<br>16 | Density BCPM 3.1<br>Zone Default BellSouth Sprint GTE HM 5.0a                        |  |  |  |  |  |  |  |  |  |
| 17       | 0 - 5 250 250 250 175 250  |  |  |  |  |  |  |  |  |  |
| 18       | 10000+ 150 150 150 175 150   |  |  |  |  |  |  |  |  |  |
| 19       |  |  |  |  |  |  |  |  |  |  |
| 20       | There is total agreement between the HM 5.0a, the BCPM national default values       |  |  |  |  |  |  |  |  |  |
| 21       | and two ILECs on these input values and on virtually all of the pole spacing input   |  |  |  |  |  |  |  |  |  |
| 22       | values in the intermediate density zones. GTE has determined that its Florida-       |  |  |  |  |  |  |  |  |  |
| 23       | specific pole spacing is 175 feet. However, in typical top-down accounting           |  |  |  |  |  |  |  |  |  |
| 24       | fashion, GTE used the same 175-foot pole span input value in all density zones,      |  |  |  |  |  |  |  |  |  |
| 25       | even though it is commor knowledge that poles are further apart in rural areas.      |  |  |  |  |  |  |  |  |  |

1 This demonstrates an appalling lack of OSP Engineering oversight. This also 2 results in GTE's cost for aerial plant in rural areas to be overstated because too 3 many poles are modeled per aerial cable route distance.

4

Copper Cable: BellSouth, GTE and Sprint all have input values for 3000, 3600 5 and 4200 pair 24 gauge cables. However, 24 gauge cables are simply not 6 manufactured in sizes larger than 2400 pairs. Therefore, it is rather obvious that 7 the ILECs are not using the actual existing prices that they pay for specific size 8 cables, since they could not possibly have purchased these particular cables for 9 which they have provided input values. Again, it is obvious that accountants are 10 determining the BCPM 3.1 input values for the ILECs without the input or 11 oversight of competent OSP Engineers. 12

13

16

14 The comparisons of the total cost input values for the smaller sizes of 24 gauge 15 buried cables, which would be used extensively in rural areas, are:

| 17<br>18 | Cable<br>Size | BCPM 3.1<br>Default | BellSouth | Sprint | GTE    | <u>HM 5.0a</u> |
|----------|---------------|---------------------|-----------|--------|--------|----------------|
| 19       | 200 pair      | \$4.45              | \$4.35    | \$4.51 | \$4.35 | \$4.42         |
| 20       | 50 pair       | \$2.50              | \$1.30    | \$2.55 | \$1.89 | \$1.70         |
| 21       | 25 pair       | \$2.08              | \$0.78    | \$2.27 | \$1.41 | \$1.24         |
| 22       | 12 pair       | \$2.05              | \$0.78    | \$1.98 | \$1.39 | \$0.79         |
| 23       | 6 pair        | \$1.97              | \$0.78    | \$1.73 | \$1.34 | \$0.66         |
|          |               |                     |           |        |        |                |

24

HM 5.0a models 6 and 12 pair 24 gauge cables when they satisfy cable size requirements because they represent currently available technology alternatives that have lower installed cost and are more efficient in terms of cable utilization than 25 pair cables. BellSouth has defaulted to the 25 pair cable costs for 6 and pair cable sizes. The rationale is that current (i.e., BellSouth's embedded) operating practices do not allow these small cables in their inventories.

The relevant criteria for determining USF support are least-cost and most-8 efficient based on currently available technology. The latest input values filed by 9 BellSouth in the BCPM 3.1 for 6 and 12 pair 24 gauge cable does not satisfy 10 these relevant criteria. Furthermore, the greatest manifestation of this excessive 11 cable costing will be in the most rural areas where the smallest cables are more 12 prevalent and where the USF support will be most required. BellSouth should 13 provide appropriate input values for 6 and 12 pair 24 gauge copper cables in 14 15 BCPM 3.1 for the purpose of determining appropriate local loop costs for USF support, which is what Sprint and GTE have done. 16

17

7

BellSouth utilizes the same copper cable prices for feeder and distribution cable applications. However, BellSouth's cable prices include cable terminals via a loading factor (BellSouth's Model Inputs and Assumptions, Bates Stamp 000157). Feeder cables simply do not have cable terminals, yet BellSouth's feeder cable costs obviously include a loading factor for terminals. This is a prime example of misapplying top-down costing principles in a bottom-up costing model without OSP Engineering judgment direction or oversight.

25

REDACTED.DOC

Another seemingly illogical phenomenon of BellSouth's cable costing is that its 26 gauge aerial cable costs are higher than its 24 gauge buried cable cost for each 3 pair size. Also, BellSouth's cost for 25 pair <u>26 gauge</u> aerial and buried cables are 4 higher than for the same cables in <u>24 gauge</u> Because 26 gauge copper 5 conductors are smaller than 24 gauge, 26 gauge cables are less costly than 24 6 gauge cables in the same pair size for the same application.

7

8

9

10

11

For some unexplained reason, Sprint's underground <u>cable</u> costs (i.e., without structure) are significantly higher than its aerial and buried cable cost for the same pair size and gauge of cables. This contradicts the appropriate relationship demonstrated by the comparable input values for HM 5.0a and the other ILECs.

12

Fiber Cable: The input value comparisons for aerial fiber cable total costs are

14

13

15 Fiber BCPM 3.1 16 Strands Default BellSouth Sprint GTE HM 5.0a 17 144 \$9.85 \$9.96 \$7.82 \$10.33 \$9.50 48 18 \$5.27 \$3.71 \$4.15 \$4.37 \$4.70 19 12 \$3.04 \$1.37 \$2.83 \$1.90 \$2.90

20

Thus, the HM 5.0a fiber cable costs are shown to be very reasonable. Also, HM 5.0a has a maximum size fiber cable of 216 strands versus 288 strands for the BCPM 3.1 and the three ILECs Thus, HM 5.0a will incur even higher fiber cable costs than BCPM 3.1 when the fiber strand requirements exceed 216

REDACTED.DOC

| 1      | because HM 5.0a will place an additional fiber cable with supporting structure at   |  |  |  |  |  |  |  |  |
|--------|---|--|--|--|--|--|--|--|--|
| 2      | multiples of 216 required strands instead of at multiples of 288 required strands   |  |  |  |  |  |  |  |  |
| 3      |   |  |  |  |  |  |  |  |  |
| 4      | Serving Area Interface ("SAI", also known as Feeder Distribution Interface)         |  |  |  |  |  |  |  |  |
| 5      | The input value comparison for the installed (i.e., material and installation) cost |  |  |  |  |  |  |  |  |
| 6      | of a 3600 pair indoor SAI is  |  |  |  |  |  |  |  |  |
| 7      |   |  |  |  |  |  |  |  |  |
|        | BCPM 3.1  |  |  |  |  |  |  |  |  |
| 8<br>9 | Default BellSouth Sprint GTE HM 5.0a  |  |  |  |  |  |  |  |  |
| 10     | \$19,605 \$73,534 \$32,175 \$19,605 \$4,928   |  |  |  |  |  |  |  |  |
| 11     |   |  |  |  |  |  |  |  |  |
| 12     | There are obviously incredible differences The HM 5.0a input value is described     |  |  |  |  |  |  |  |  |
| 13     | in Section 2.9 of the HM 5.0a Inputs Portfolio. There is no similar                 |  |  |  |  |  |  |  |  |
| 14     | documentation to explain the ILEC's costs. The material components consist of       |  |  |  |  |  |  |  |  |
| 15     | a plywood backboard, modular protector units, connecting blocks and jumper          |  |  |  |  |  |  |  |  |
| 16     | wire. BellSouth's cost level could cover several weeks of engineering and labor     |  |  |  |  |  |  |  |  |
| 17     | plus \$14,418 in supply costs, all of which are exorbitant. Note that GTE has       |  |  |  |  |  |  |  |  |
| 18     | defaulted to the BCPM national input value rather than ascertain its Florida-       |  |  |  |  |  |  |  |  |
| 19     | specific costs.   |  |  |  |  |  |  |  |  |
| 20     |   |  |  |  |  |  |  |  |  |
| 21     | Only BellSouth furnished detailed SAI costs (Exhibit (JWW-4), Pg. 15 -              |  |  |  |  |  |  |  |  |
| 22     | 18). Note how the "engineering" costs have been applied linearly based on the       |  |  |  |  |  |  |  |  |
| 23     | pair count of the SAI For example, BellSouth has costed \$312.66 to engineer a      |  |  |  |  |  |  |  |  |
| 24     | 100 pair indoor SAI and \$13,131.68 to engineer a 4200 pair indoor SAI (i.e., 42    |  |  |  |  |  |  |  |  |
| 25     | times more). However, real world engineering costs for an indoor SAI vary little    |  |  |  |  |  |  |  |  |
|        |   |  |  |  |  |  |  |  |  |

| 1  | by pair size. This is                       | an example of     | the top-down   | n accountii  | ng applica  | tion of ILEC   |  |  |  |
|----|---|-------------------|----------------|--------------|-------------|----------------|--|--|--|
| 2  | cost data without OSP Engineering judgment. |                   |                |              |             |                |  |  |  |
| 3  |   |                   |                |              |             |                |  |  |  |
| 4  | Drop Wire Placem                            | ent – Aerial a    | nd Buried: 7   | The compa    | irisons of  | LEC input      |  |  |  |
| 5  | values for the aerial                       | and buried tota   | l drop wire c  | osts are:    |             |                |  |  |  |
| 6  |   |                   |                |              |             |                |  |  |  |
| 7  | Drop Densit                                 | ty BCPM 3.1       |                |              |             |                |  |  |  |
| 8  | Type Zon                                    |                   | BellSouth      | Sprint       | GTE         | HM 5.0a        |  |  |  |
| 9  | Aerial 0 –                                  | 5 \$ 0.77         | \$ 0.26        | \$ 0.80      | \$0.62      | \$0.26         |  |  |  |
| 10 | Aerial 1000                                 | 00+ \$ 0.77       | \$ 0.2 >       | \$ 0.80      | \$0.62      | \$0.33         |  |  |  |
| 11 | Buried 0-                                   | 5 \$ 0.77         | \$ 0.7 )       | \$ 0.74      | \$0.62      | \$0.74         |  |  |  |
| 12 | Buried 1000                                 | 00+ \$ 0.77       | \$ 0.70        | \$ 0.74      | \$0.62      | \$5.14         |  |  |  |
| 13 |   |                   |                |              |             |                |  |  |  |
| 14 | HM 5.0a appropria                           | tely reflects the | real world b   | y modelinį   | g higher d  | rop costs for  |  |  |  |
| 15 | the urban versus ru                         | iral areas, 27%   | higher for a   | erial drops  | and 595     | % higher for   |  |  |  |
| 16 | buried drops. The                           | ILECs model t     | he same cost   | per foot     | in all den  | isity areas by |  |  |  |
| 17 | drop type. This sh                          | ows a lack of (   | OSP Engineer   | ring judgm   | ent and a   | lso results in |  |  |  |
| 18 | higher drop costs in                        | rural areas bec   | ause the : ver | age drop c   | ost is bein | ig applied.    |  |  |  |
| 19 |   |                   |                |              |             |                |  |  |  |
| 20 | Drop costs have a                           | major impact of   | on total loop  | costs bec    | cause they  | v represent a  |  |  |  |
| 21 | significant amount of                       | of investment th  | hat occurs at  | virtually e  | ach custo   | mer location.  |  |  |  |
| 22 | The impact of inap                          | ppropriate drop   | o costing on   | a per foc    | ot basis i  | s even more    |  |  |  |
| 23 | profound in rural ar                        | eas because of p  | generally long | ger drops lo | engths.     |                |  |  |  |
| 24 |   |                   |                |              |             |                |  |  |  |
|    |   |                   |                |              |             |                |  |  |  |

| a. | Buried drops simply cost more than aerial drops. Note that BellSouth more than   |                |                   |                |               |                 |  |  |  |  |
|----|--|----------------|-------------------|----------------|---------------|-----------------|--|--|--|--|
| 2  | doubles its installed cost for buried drops versus aerial drops, while HM 5.0a   |                |                   |                |               |                 |  |  |  |  |
| 3  | increases range from 184% to 1458%. In contrast, Sprint's costing of aerial      |                |                   |                |               |                 |  |  |  |  |
| 4  | drops higher than buried drops is astonishingly illogical                        |                |                   |                |               |                 |  |  |  |  |
| 5  |  |                |                   |                |               |                 |  |  |  |  |
| 6  | Note that GTE  | 's buried and  | i aerial drop in  | nput values (i | e, the BCI    | PM 3.1 national |  |  |  |  |
| 7  | default values)  | are the sam    | e, and they a     | re at the mu   | ch higher bu  | uried drop cost |  |  |  |  |
| 8  | level. This is   | because GT     | E is modeling     | g 100% buri    | ed drop cos   | sts, which cost |  |  |  |  |
| 9  | more than zeria  | al drops. This | s is a clear viol | ation of the l | FCC Criteria  | No. 1 that the  |  |  |  |  |
| 10 | model be "reas   | onable" and    | "least-cost" ba   | ised on curre  | ntly availabl | e technology.   |  |  |  |  |
| 11 |  |                |                   |                |               |                 |  |  |  |  |
| 12 | The drop wire  | input values   | s of the HM       | 5.0a are clea  | rly realistic | and reasonable  |  |  |  |  |
| 13 | compared to th   | nose of the II | LECs. Furth       | ermore, in ur  | ban density   | zones, the HM   |  |  |  |  |
| 14 | 5.0a drops costs are significantly higher. This reflects sound OSP Engineering   |                |                   |                |               |                 |  |  |  |  |
| 15 | judgment of real world higher costs that has been consistently incorporated into |                |                   |                |               |                 |  |  |  |  |
| 16 | the HM 5.0a input values as appropriate.   |                |                   |                |               |                 |  |  |  |  |
| 17 |  | 2              |                   |                |               |                 |  |  |  |  |
| 18 | Network Inter  | face Device    | ("NID"), Pro      | etector and    | Interface: T  | he input value  |  |  |  |  |
| 19 | comparison for   | the total cos  | sts of NID, Pro   | otector and I  | nterfaces is: |                 |  |  |  |  |
| 20 |  |                |                   |                |               |                 |  |  |  |  |
|    | NUD  | DCDM 2.1       |                   |                |               |                 |  |  |  |  |
| 21 | NID  | BCPM 3.1       | DallCouth         | Coriet         | CTU           | ID ( CO)        |  |  |  |  |
| 22 | Type   | Default        | BellSouth         | Sprint         | GTE           | HM 5.0a         |  |  |  |  |
| 23 | Residential  | \$30.73        | \$56.61           | \$58.95        | \$29.49       | <b>\$</b> 29.00 |  |  |  |  |
| 24 | Business   | \$30.73        | \$56.61           | \$99.85        | \$29.49       | \$44.00         |  |  |  |  |
| 25 |  |                |                   |                |               |                 |  |  |  |  |

| 1  | BellSouth and GTE utilize the same cost for residential and business NIDs,     |  |  |  |  |  |  |  |  |  |
|----|--|--|--|--|--|--|--|--|--|--|
| 2  | whereas Sprint and HM 5.0a appropriately reflect lower cost for residential    |  |  |  |  |  |  |  |  |  |
| 3  | NIDs. Why are Sprint's business NID costs so much higher? HM 5.0a costs are    |  |  |  |  |  |  |  |  |  |
| 4  | within the range of the ILEC costs.  |  |  |  |  |  |  |  |  |  |
| 5  |  |  |  |  |  |  |  |  |  |  |
| 6  | Digital Loop Carrier: The comparisons of ILEC input values for digital loop    |  |  |  |  |  |  |  |  |  |
| 7  | carrier costs are:   |  |  |  |  |  |  |  |  |  |
| 8  |  |  |  |  |  |  |  |  |  |  |
|    |  |  |  |  |  |  |  |  |  |  |
| 9  | Cost Line BCPM 3.1   |  |  |  |  |  |  |  |  |  |
| 10 | Type Size Default BellSouth Sprint GTE HM 5.0a                                 |  |  |  |  |  |  |  |  |  |
| 11 | Fixed 25 \$19,204 \$ 19,204 \$ 23,159 \$ 23,754 \$18,300                       |  |  |  |  |  |  |  |  |  |
| 12 | Fixed 673 \$96,859 \$96,859 \$128,569 \$113,125 \$88,500                       |  |  |  |  |  |  |  |  |  |
| 13 | Per Line 0 – 192 \$94.00 \$94.00 \$98.59 \$72.39 \$100.00                      |  |  |  |  |  |  |  |  |  |
| 14 | Per Line 192 – 2016 \$89.11 \$89.11 \$68.02 \$72.39 \$ 77.50                   |  |  |  |  |  |  |  |  |  |
| 15 |  |  |  |  |  |  |  |  |  |  |
| 16 | Why does GTE input the same cost for low density and high density line cards?  |  |  |  |  |  |  |  |  |  |
| 17 | The ILEC's fixed costs for DLC RT locations are extremely high considering     |  |  |  |  |  |  |  |  |  |
| 18 | that these locations would be generally much smaller than 999 lines, the BCPM  |  |  |  |  |  |  |  |  |  |
| 19 | 3.1 threshold. In other words, the smaller size DLC RTs modeled by BCPM 3.1    |  |  |  |  |  |  |  |  |  |
| 20 | should be housed predominantly in cabinets and not require more expensive huts |  |  |  |  |  |  |  |  |  |
| 21 | or controlled environment vaults ("CEVs"). It appears that ILEC accountants    |  |  |  |  |  |  |  |  |  |
| 22 | have loaded DLC RT site input values reflecting the embedded network           |  |  |  |  |  |  |  |  |  |
| 23 | investment including huts and CEVs. There is no supporting documentation that  |  |  |  |  |  |  |  |  |  |
| 24 | would reflect appropriate OSP Engineering judgment.                            |  |  |  |  |  |  |  |  |  |
| 25 |  |  |  |  |  |  |  |  |  |  |

Why are high density DLC system costs per line significantly less for Sprint and 1 GTE than for BellSouth? The conclusion of the Staff of the Louisiana Public 2 Service Commission was that the BCPM inappropriately modeled the expensive 1 REUVG range extension line card for high density DLC systems (Louisiana 4 Staff's Final Recommendation, Docket No. U-20833, March 27, 1998, Pg. 14). 5 BellSouth has adopted the BCPM national default value that still includes the 6 exorbitant REUVG range extension line cards, whereas, Sprint and GTE appear 7 to have made the appropriate adjustment to the lower cost RUVG2 range 8 extension line card. 9

10

HM 5.0a models sufficient costs for range extension line cards as required. For 11 the CSAs requiring low density DLC Systems, HM 5.0a models the Advanced 12 Fiber Systems UMC 1000. HM 5.0a has costed these systems with 100% 13 utilization of UMC Remote Terminal Range Extension RST POTS Channel Units 14 (R-EPOTS or simply EPOTS), even though the less expensive standard RPOTS 15 card is sufficient for loops up to 12,000 feet from the DLC RT. Note that this is 16 reflected in the HM 5.0a low density per line costs, which are higher than those 17 of the ILECs. 18

19

For high density CSAs, HM 5.0a models the DSC Litespan 2000 DLC System. HM 5.0a incorporates costs for the DSC Litespan 2000 RPOTS channel unit for customers served by large DLC RT units to a distance of 17,600 feet. DSC recommends the use of the RUVG2 card for those customers exceeding 17,600 feet in distribution length. Since the maximum distribution length in limited to

#### REDACTED DOC

18,000 feet in HM 5.0a, the number of customers requiring this card from a high density DLC system is de minimis.

ı

2

3

To add some further perspective to the debate over range extension requirements 4 and appropriate costs, BCPM 3.1 recommends range extension only for loops 5 exceeding 13,600 feet from the DLC RT (BCPM 3.1 Description, Pg. 55). 6 According to Mr. Brian Pitkin, an AT&T/MCI Witness in this proceeding, the 7 HM 5.0a network designed for Florida has less than 0.05% of its loops exceeding 8 9 13,600 feet in distribution length from the DLC RT. Furthermore, most of these 10 loops will be served by low density DLC systems, which have 100% range 11 extension line cards in HM 5.0a. My conclusion is that HM 5.0a models more than sufficient costs for the required range extension line cards. 12 13 Fiber/Copper Breakpoint: The input value comparison for the fiber/copper 14 breakpoint is: 15 16 **BCPM 3.1** 17 18 Default BellSouth Sprint GTE HM 5.0a 19 12,000 12,000 12,000 12,000 9,000 20 21 The explanation for the 3,000 foot difference between BCPM 3.1 modeled by the ILECs and HM 5.0a is that BCPM 3.1 is measuring the longest total loop length 22 in a CSA whereas HM 5.0a is measuring the feeder distance from the wire center 23 24 to the Feeder Distribution Interface ("FDI"). The overall impact of this difference in modeling methodologies is not that significant. However, the latest 25 26 dynamic copper versus fiber feeder selection methodology employed by the HM REDACTED.DOC

| 1  | 5.0a (HM 5.0a Methodology, Sec. 4.5) is the one that replicates the process         |  |  |  |  |  |  |  |  |
|----|---|--|--|--|--|--|--|--|--|
| 2  | utilized by a real world OSP Engineer.  |  |  |  |  |  |  |  |  |
| 3  |   |  |  |  |  |  |  |  |  |
| 4  | Plant Mix - Distribution: The input value comparisons for the percentage of         |  |  |  |  |  |  |  |  |
| 5  | distribution plant are:   |  |  |  |  |  |  |  |  |
| 6  |   |  |  |  |  |  |  |  |  |
| 7  | Density BCPM 3.1  |  |  |  |  |  |  |  |  |
| 8  | Type of Plant Zone Default BellSouth Sprint GTE HM 5.0a                             |  |  |  |  |  |  |  |  |
| 9  | Underground 10000+ 90.00% 90.00% 1.50% 1.96% 10.00%                                 |  |  |  |  |  |  |  |  |
| 10 | Buried 0-5 60.00% 60.00% 87.50% 78.11% 75.00%                                       |  |  |  |  |  |  |  |  |
| 11 | Aerial 10000+ 0.00% 0.00% 13.20% 73.90% 5.00%                                       |  |  |  |  |  |  |  |  |
| 12 |   |  |  |  |  |  |  |  |  |
| 13 | BellSouth has adopted the BCPM 3.1 national default input values for all of its     |  |  |  |  |  |  |  |  |
| 14 | plant mix inputs because it cannot ascertain from its own Florida-specific data the |  |  |  |  |  |  |  |  |
| 15 | appropriate mix of plant in Florida There are huge differences among the ILEC       |  |  |  |  |  |  |  |  |
| 16 | input values.   |  |  |  |  |  |  |  |  |
| 17 |   |  |  |  |  |  |  |  |  |
| 18 | The BCPM 3.1 national default input, which BellSouth has adopted, is 90%            |  |  |  |  |  |  |  |  |
| 19 | underground distribution plant in the 10000+ density zone. However, in this         |  |  |  |  |  |  |  |  |
| 20 | most urban, high density zone, most feeder cables go into buildings, and most of    |  |  |  |  |  |  |  |  |
| 21 | the distribution cables are either inside of or attached to buildings or placed in  |  |  |  |  |  |  |  |  |
| 22 | ducts provided by property owners. Thus, when BellSouth models 90% of the           |  |  |  |  |  |  |  |  |
| 23 | distribution plant as underground, it is adding substantial costs for underground   |  |  |  |  |  |  |  |  |
| 24 | conduit and manholes that are simply not required                                   |  |  |  |  |  |  |  |  |
| 25 |   |  |  |  |  |  |  |  |  |
|    |   |  |  |  |  |  |  |  |  |

Page 28

1

1 In sharp contrast, HM 5.0a has a more reasoned input value of 10% as described in the HAI Model Release 5.0a Inputs Portfolio Section 2.5. Also, note that 2 Sprint and GTE have even smaller input values of less than 2.0% for 3 4 underground distribution plant in urban areas. 5 Another example of flawed modeling logic is the fact that BellSouth, again using the BCPM national default input value, shows 0.00% for aerial plant in the most 7 8 urban density zone. Moreover Sprint has modeled 83.5% of its distribution cables in the highest density zone as buried plant, which would be cost 9 prohibitive, if not impossible, to place in a congested urban area. Neither of 10 these ILEC input values reflects sound OSP Engineering judgment. 11 12 13 Plant Mix - Fiber Feeder: The input value comparisons for the percentage of 14 fiber feeder plant are: 15 16 Density BCPM 3.1 17 Type of Plant Zone Default BellSouth Sprint GTE HM 5.0a Underground 0 - 5 10.00% 86.91% 5.00% 18 10.00% 23.50% 19 GTE's high input value of 86.91% for underground fiber feeder percentage in the 20 rural areas is simply ridiculous. Feeder routes in rural areas consist of only one 21 22 fiber cable that will never need to be reinforced. Such situations clearly call for less costly buried or aerial plant. No cost-efficient telephone company would 23 24 incur the exorbitant cost of building a conduit and manhole system for 86.91% of 25 its fiber feeder in rural areas. This is an even more profound issue given that the

#### REDACTED.DOC

BCPM 3.1 also models excessive fiber feeder to far too many DLC RT locations (detailed elsewhere in this testimony). The impact of this egregious error in plant mix is to greatly inflate GTE's rural costs, which results in an artificially high Universal Service Fund.

- Investment Loop Cap: BCPM 3.1 employs an investment loop cap to allow for a
   maximum individual loop investment based on either potential regulatory policy
   or a wireless technology alternative (BCPM Methodology, Pg. 56). The default
   value is \$10,000, which has been commonly accepted in numerous proceedings
   by all parties. In this proceeding however, BellSouth has filed an Investment
   Loop Cap of only \$4,350, without any explanation or supporting documentation
- 13 BellSouth's In-Plant Loading Factors: BellSouth's engineering and labor costs 14 are derived from BellSouth's in-plant loading factors that convert the material 15 prices to an installed investment. Having analyzed BellSouth's in-plant loading 16 factors in UNE Cost Dockets in eight states, including Florida, I believe that 17 BellSouth's OSP loadings are not forward-looking and, instead, are utilized to 18 recover the costs of BellSouth's embedded methods of operation. I have several concerns with BellSouth's cost modeling methodology base on its use of top-19 20 down loading factors.
- 21

5

12

22 BellSouth applies a material loading factor to the <u>inflated</u> (Caldwell Direct, Pg. 9) 23 direct material cost for copper and fiber cables in its OSP Field Reporting Codes. 24 These material loading factors are modeled primarily to recover 25 telecommunications engineering and labor, vendor engineering and installation,

REDACTED.DOC

exempt (i.e., minor) material, and sales tax (Caldwell Direct, Pg. 11). BellSouth's methodology is to calculate a ratio of these associated expenses to its nonexempt (i.e., major) material investments for the year 1995, and then multiply this ratio by the inflated direct cable material cost.

I do not believe that BellSouth's ratio of material loading expenses to cable 6 investment in 1995 should be considered least-cost, most-efficient, or forward-7 looking based on currently available technology. Mr. William Zarakas, 8 BellSouth's Cost Modeling Witness in the UNE Cost Dockets, stated in his 9 10 deposition in Louisiana that, "our assumption there would be that the cost of installing a pole in the future would basically be the same as it was in the past. 11 because we see no change in the technology. And we did that for each 12 individual factor or loading" (Zarakas Deposition, LA Docket U-22022/U-13 22093, 8/19/97, Pg. 110, with italics added for emphasis). However, the BCPM 14 15 proponents contradict this statement by saying that "the Model does not rely 16 upon embedded costs for facilities, functions or elements" (BCPM Methodology, Pg. 12). 17

18

5

Going beyond the fundamental methodology question and looking into the data provided on the material loading factors raises additional questions. These material loading factors for cable are huge contributors to the total loop investment. The following examples of these in-plant loadings will demonstrate how they are used to drive enormous underlying costs that make up BellSouth's input values to the BCPM 3.1:

#### REDACTED.DOC

A prime example of the impact of these loadings can be found in the . BellSouth's application of in-plant loading factors to SAIs. In BellSouth's costing of a 4200 pai, indoor SAI, \$13,689 worth of material becomes \$85,789 in installed costs. Thus, the in-plant loading factors account for 4 84% of the total costs.

ILEC Engineering and placing costs have been allocated based on cable 6 size or material costs. For example, BellSouth's placing input values for 7 24 gauge underground cable are \$1.03 for 100 pair and \$22.96 for 2400 8 pair. Likewise, BellSouth's engineering input values for these same 9 cables are \$0.15 and \$3.37. It simply does not cost 22 times as much to 10 engineer or place a 2400 pair underground cable than a 100 pair 11 underground cable. In reality, there is very little difference in the costs to 12 engineer and place an underground copper cable based on its pair size. 13

BellSouth has double counted placing costs for buried copper and fiber 14 cables because it zeroed out the splicing column instead of the placing 15 column in its buried cable tables. Buried cable placement costs are 16 appropriately included in the buried structure costs and should not be 17 included in the cost of the buried cables themselves. Furthermore, based 18. on a comparison of these additional buried placement costs to the splicing 19 cost for aerial and underground cables, this double-counting does not 20 seem to have been a simple matter of BellSouth putting its splicing costs 21 in the placing costs column. Thus, BellSouth's installed buried cable 22 costs are overstated. 23

REDACTED DOC

1

2

3

5

| 1  |   | There as   | re a signif | ficantly h | igher supply    | costs for aerial  | versus b   | uried and  |  |
|----|---|--|-------------|------------|-----------------|-------------------|------------|------------|--|
| 2  |   | underground copper cables of the same gauge and pair count as shown in |             |            |                 |                   |            |            |  |
| 3  |   | the following table:   |             |            |                 |                   |            |            |  |
| 4  |   |  | Be          | llSouth's  | Copper Cabl     | le Supply Costs   |            |            |  |
| 5  |   |  |             |            |                 |                   |            |            |  |
| 6  |   | Size/  |             |            |                 |                   |            |            |  |
| 7  |   | Type   | 24 (        | Gauge Ca   | bles            | 26                | Gauge C    | ables      |  |
| 8  |   |  |             |            |                 |                   |            |            |  |
| 9  |   | Pairs  | 4200        | 200        | 25              | 4200              | 900        | 25         |  |
| 10 |   | Aerial   | \$22.64     | \$4.87     | \$0.30          | \$19.72           | \$4.50     | \$0.34     |  |
| 11 |   | Buried   | \$13.32     | \$2.86     | \$0.13          | \$12.70           | \$2.81     | \$0.17     |  |
| 12 |   | UG   | \$18.21     | \$5.63     | \$0.12          | \$16.68           | \$4.02     | \$0.11     |  |
| 13 |   |  |             |            |                 |                   |            |            |  |
| 14 |   | The exp  | olanation   | cannot b   | e that BellSo   | outh includes to  | erminal o  | costs as a |  |
| 15 |   | cable lo   | ading fac   | tor beca   | use there are   | no comparabl      | e supply   | costs for  |  |
| 16 |   | buried o   | ables tha   | t also ha  | ve terminals.   | Furthermore,      | compara    | ble supply |  |
| 17 |   | costs have been applied to the larger size cables, which rarely have   |             |            |                 |                   |            |            |  |
| 18 |   | terminal   | s. Also,    | the expl   | anation canno   | ot be due to st   | rand and   | pole line  |  |
| 19 |   | hardwar  | e costs b   | ecause ti  | here are no c   | omparable supp    | oly costs  | for aerial |  |
| 20 |   | fiber cal  | oles?       |            |                 |                   |            |            |  |
| 21 | ٠ | BellSou  | th's costs  | for splig  | cing aerial cal | bles are unreali  | stically h | igher than |  |
| 22 |   | splicing   | costs for   | undergro   | ound cables of  | f the same pair s | ize and g  | auge.      |  |
| 23 | • | BellSou  | th's filing | g also sh  | ows that it is  | s more costly t   | o place    | 26 gauge   |  |
| 24 |   | undergr  | ound cab    | les than l | arger and hea   | avier 24 gauge    | cables of  | the same   |  |
| 25 |   | pair size  | 2.          |            |                 |                   |            |            |  |
| 26 | • | BellSou  | th's engin  | eering co  | osts vary cons  | iderably betwee   | n 24 and   | 26 gauge   |  |
| 27 |   | cables o   | f the same  | e pair siz | e and type of   | plant.            |            |            |  |
|    |   |  |             |            |                 |                   |            |            |  |

 Furthermore, since fiber cable sheaths are the virtually the same regardless of fiber count, there is no rationale for BellSouth to model a much higher cost to place a fiber cable of higher fiber count. This discrepancy causes BellSouth's fiber cable placement costs for larger fiber cables to be overstated.

7 These are but a few examples where BellSouth has taken an illogical, top-down 8 accounting approach to deriving input values that simply contradict real world 9 OSP Engineering. BellSouth's filing shows a lack of OSP Engineering judgment 10 in the determination or review its cable input values. Noteworthy is the 11 observation that GTE and Sprint simply did not file the underlying costing details 12 for their cable input values for analysis.

13

t

2

3

4

5

6

Drop Wires: Responses to Data Requests in this proceeding show that ILECs 14 serve fewer than xxxx lines per residence. Yet, BCPM 3.1 assumes five-pair 15 buried drops for both residences and businesses. While ILECs can certainly 16 choose to invest in five-pair buried drops to every residence to preclude ever 17 18 having to reinforce any of them, it does not seem reasonable that the Universal Service Fund should fully support the excessive spare capacity. Furthermore, the 19 availability of two-channel DSL Systems provides a viable alternative for up to 20 four subscriber lines on a two-pair buried drop for those residential customers 21 22 who may someday require more than two lines. My recommendation, for the purpose of USF costing, is that all residence buried drops should be two pair. 23

24

REDACTED.DOC

 Lack of Real World Variation in Input Values: The ILECs have filed in BCPM

 3.1 input values in a manner that totally disregards clearly understood differences

 by density zone. There is no appropriate variation in many of the ILEC input

 values by density zone for such input values as pole structure sharing, aerial and

 buried drop costs, or distribution fill factors. The following examples will further

 illustrate the lack of OSP Engineering judgment in deriving ILEC input values.

BellSouth utilizes the same costs per foot for conduit installation and cost
 per foot for buried cable installation for each trenching method: Trench
 and Backfill, Rocky Trench, Backhoe Trench and Hand Dig Trench.
 Sprint does likewise. Furthermore, BellSouth does not vary its buried
 cable trenching costs for differing terrain conditions of normal, soft rock
 and hard rock.

Sprint even uses the same base cost per foot installed for both conduit 13 and cable placement for all methods, all soil types, and all density zones. 14 Sprint's explanation is that "the contract does not differentiate among 15 16 these activities" (Sprint's Response to AT&T's First Set of 17 Interrogatories, Att. 24) As an OSP Engineer, I find that statement 18 rather amazing. As an example of the impact of these simplified input values, For Hard Rock - Feeder Conduit Trench and Backfill, BellSouth 19 has filed a base cost per foot installed of \$60.98 compared to Sprint's 20 21 filing of \$1.90, a difference of 3,209%. This contradicts real world OSP costing, because trench costs vary considerably by method, density zone 22 and type of soil condition. 23

24

REDACTED.DOC

BCPM 3.1 contains extensive input value tables that have been developed to appropriately differentiate pole, buried cable and underground conduit placement costs by type of method, by density zone, and by soil conditions. The ILECs may rationalize that by populating these input tables with average values that "it all averages out." However, the abject failure of the ILECs to populate the cells of these input value tables with realistic costs raises considerable doubt regarding the validity of BCPM 3.1 output in any particular density zone.

Contract Prices: Ms. Caldwell states that "BellSouth's structure placement costs 9 (contractor costs) for placing conduit, trenching/plowing buried cable, and 10 placing poles are based on an average of the ten existing BellSouth contracts with 11 outside plant contractors in Florida" (Caldwell Direct, Pg. 9). ILECs use such 12 "Master Contracts" to award day-to-day small-scale routine work and smaller-13 scale projects. However, in accordance with the "least-cost, most-efficient" 14 assumptions of FCC Criterion 1, the appropriate contractor costs for these 15 models should be lower than these averages to reflect only large-scale projects 16 that are put out for competitive bids. This would produce more appropriate 17 18 contractor costs consistent with the underlying "scorched node" assumption of these models. 19

20

8

The supposedly proper application of the "scorched node" assumption by BCPM 3.1 has been testified to by Dr. Staihr when he stated that, "the BCPM 3.1 model assumes that the entire network is built at a single point in time. This allows the service provider to realize certain 'efficiencies' and 'economies of scale' that could not have been realized historically" (Staihr Direct, Pg. 7 with italics added

REDACTED.DOC

least-cost model. It is also apparent that the ILEC OSP input values for many
 items have been derived via accounting methods that have not been subjected to
 a reasonableness check by OSP Engineers.

how to identify and/or correctly apply their data as input values into a bottom-up.

Some BCPM witnesses have frankly admitted this. One stated that, "GTE does not necessarily maintain data that can be easily translated into all of the input values for the BCPM or HAI models" (Robinson Direct, NC Docket P-100, SUB 133b, 12/10/97, Pg. 5). Another ILEC witness has testified that "it is difficult and time consuming to make all model default inputs company-specific. Therefore, in producing costs using a cost proxy model, GTE must rely on many default inputs" (Collins Direct, TX Docket 18515, 2/17/98, Pg. 4).

19

7

It is indeed difficult for the ILECs to properly define and properly apply OSP input values, even though they have volumes of state-specific cost data. On the other hand, HM 5.0a employs national default input values developed by the HAI OSP Engineering Team that work within the HM 5.0a to produce <u>Florida-</u> specific outputs because:

### REDACTED.DOC

| 1  |      | · The labor content of OSP costs are reduced from national levels by a             |
|----|------|--|
| 2  |      | Florida-specific factor of 68% (HM 5.0a IP, Sec 7.)                                |
| 3  |      | · Placing costs are increased appropriately for difficult terrain, surface         |
| 4  |      | texture, rock depth, rock hardness and water depth statistics that are             |
| 5  |      | Florida-specific at the CBG level.   |
| 6  |      | Customer and wire center locations are Florida-specific at the individual          |
| 7  |      | location level.  |
| 8  |      | Material costs for a least-cost model representing large ILECs should not          |
| 9  |      | vary significantly from nationwide material costs.                                 |
| 10 |      |  |
| 11 | Q.   | HAS THE BCPM 3.1 ACHIEVED THE MOST REALISTICALLY                                   |
| 12 |      | ATTAINABLE LEVEL OF ACCURACY FOR IDENTIFYING                                       |
| 13 |      | CUSTOMER LOCATIONS?  |
| 14 | Α.   | No. One of the primary goals of a superior local loop model is precise customer    |
| 15 |      | location because this is the basis for accurate and cost-efficient network design. |
| 16 |      | The BCPM 1.0 and the Hatfield Model up through Release 4.0 located or              |
| 17 |      | assigned customers at the CBG level. The BCPM 2.0 and now BCPM 3.1 use             |
| 18 |      | housing and business line data at the CB level to better locate customers. On      |
| 19 |      | average, there are about 30 CBs per CBG (BCPM 3.1 Description, Pg. 6).             |
| 20 |      | However, the HM 5.0a is much more precise in locating customers through            |
| 21 |      | latitude and longitude geocoding to six decimal places of the customer's           |
| 22 |      | addresses (HM 5.0a Description, Sec. 5.4.3).                                       |
| 23 |      |  |
| 24 |      | The overall geocoding success rate for HM 5.0a, as calculated by Mr. Pitkin, was   |
| 25 |      | 70% of the Florida customers in this proceeding. It is higher in the urban areas   |
|    | REDA | CTED.DOC Page 38   |

because customer locations have more geographically definite addresses and 1 2 lower in rural areas for the opposite reason. 3 4 BCPM 3.1 does not actually locate any customers. In essence, it locates roads 5 and then assumes that customers in the CB are uniformly distributed along those 6 roads (Duffy-Deno Direct, Pg. 3). The testimonies of Messrs. Pitkin and Wood 7 critique the BCPM 3.1 grid based customer location methodology in detail 8 9 0. HOW WELL DOES THE BCPM 3.1 GROUP CUSTOMERS AS AN OSP 10 ENGINEER WOULD IN DESIGNING A LOCAL LOOP NETWORK? 11 Α. Not nearly as well as HM 5.0a. The BCPM 3.1 translates the CB level customer 12 information into a microgrid that has its boundaries based on fixed latitude and 13 longitude lines. As these microgrids are subsequently combined into ultimate 14 grids, or CSAs, for the purpose of modeling the OSP network, their boundaries 15 are still arbitrarily fixed. The BCPM 3.1 CSAs are then divided into four 16 Distribution Area ("DA") guadrants 17 One unintended consequence of this BCPM 3.1 modeling methodology is that 18 19 some natural clusters of customers (e.g., a small town or subdivision) will be 20 arbitrarily segmented into different DAs, CSAs or feeder routes in contradiction to the way that they would in reality be engineered. As an OSP Engineer, I thus 21 22 take exception to the assertion that "BCPM designs a network the way actual 23 telephone companies design networks" (Bowman Direct, Pg. 6). Furthermore, 24 the current FCC Public Notice states that, "we consider a model platform that 25 groups customers using a clustering approach because it appears to have REDACTED.DOC Page 39

| 1  | advantages over gridding approaches" (FCC Public Notice DA 98-1587, 8/7/98,                 |
|----|---|
| 2  | Pg. 4).   |
| 3  |   |
| 4  | The BCPM 3.1 road-reduced DA (BCPM 3.1 Methodology, Pg. 49) is based on                     |
| 5  | two questionable assumptions:   |
| 6  | 1. That simply designating "a 500 foot buffer along each side of the roads                  |
| 7  | within the distribution quadrant" in all density zones will model the                       |
| 8  | correct size DA for distribution cable design. Because the arbitrariness of                 |
| 9  | this assumption can result in oversizing the DA, the BCPM 3.1 has had to                    |
| 10 | add a check to constrain the area of the DA so that it does not exceed the                  |
| 11 | actual area of the microgrid itself (BCPM 3.1 Methodology, Pg. 49,                          |
| 12 | Footnote 36).   |
| 13 | 2. The center of each quadrant's DA should be placed at the road centroid                   |
| 14 | of the quadrant because customers are uniformly distributed along the                       |
| 15 | roads. While this is an improvement over locating them at the centroid of                   |
| 16 | a CBG, in reality the road centroid could be in the middle of a lake, on                    |
| 17 | top of a mountain, or in any number of inaccessible places.                                 |
| 18 |   |
| 19 | On the other hand, HM 5.0a clusters its more precisely located customers like an            |
| 20 | OSP Engineer would do in designing a local loop network (HM 5.0a Description,               |
| 21 | Sec. 5.5) based on:   |
| 22 | <ul> <li>assuring a reasonable proximity of the customer locations to each other</li> </ul> |
| 23 | (i.e., two miles),  |
|    |   |

11.2.7

REDACTED.DOC

Page 40

1

| 1  |       | · maximizing the copper distribution length up to 18,000 feet from the                      |
|----|-------|---|
| 2  |       | DLC RT based on fully utilizing the capabilities of currently available                     |
| 3  |       | technology,   |
| 4  |       | <ul> <li>maximizing the customer line size of the DLC RT up to 1,800 lines based</li> </ul> |
| 5  |       | on 90% utilization of a 2,016 line DLC system,  |
| 6  |       | · designing the shortest distance between customer clusters (however,                       |
| 7  |       | based on right angle routing to assure sufficient cable length), and                        |
| 11 |       | <ul> <li>efficiently linking "outlier clusters" to main clusters.</li> </ul>                |
| 9  |       |   |
| 10 |       | "One of the major challenges of building a proxy model is clustering customers in           |
| 11 |       | a fashion that integrates engineering practices based on this CSA approach"                 |
| 12 |       | (BCPM 3.1 Methodology, Pg. 24). I certainly agree, and conclude that the HM                 |
| 13 |       | 5.0a methodology of grouping customer locations into clusters based on OSP                  |
| 14 |       | Engineering principles is clearly superior to the BCPM 3.1 methodology of                   |
| 15 |       | assembling and dividing grids with fixed boundaries at various latitude and                 |
| 16 |       | longitude lines.  |
| 17 |       |   |
| 18 | Q.    | DOES EITHER BCPM 3.1 OR HM 5.0a ACTUALLY DESIGN   |
| 19 |       | DISTRIBUTION CABLES TO EACH AND EVERY CUSTOMER  |
| 20 |       | LOCATION?   |
| 21 | Α.    | No. Each model sizes and centers its DAs using different methodologies. Each                |
| 22 |       | model then effectively lays out a grid of backbone and branch distribution cables           |
| 23 |       | to serve the defined DAs areas from the defined DA centers. However, "[t]he                 |
| 24 |       | [BCPM 3.1] road-reduced area is not used to locate customers, but as a                      |
| 25 |       | modeling tool to determine likely cable distances required to serve customers in            |
|    | REDAC | TED.DOC Page 11   |

| 1  | the distribution quadrant" (BCPM 3.1 Methodology, Pg. 20, with italics added        |
|----|---|
| 2  | for emphasis). Dr. Duffy-Deno helps to further clarify the BCPM 3.1 distribution    |
| 3  | cable modeling methodology by stating:  |
| 4  | It is important to make clear that BCPM does not locate customers within            |
| 5  | the road-reduced areas. Estimated customer locations reside in the                  |
| 6  | microgrids and are not "moved" to the road-reduced areas. Rather, the               |
| 7  | road-reduced area is used as a tool to estimate the amount of cable                 |
| 8  | needed to serve the estimated customer locations that reside within the             |
| 9  | microgrids in populated distribution quads (Duffy-Deno Direct, Pg. 20,              |
| 10 | with italics added for emphasis).   |
| 11 | 1.20  |
| 12 | Claims that either model "moves customers" or "comes up short" of reaching a        |
| 13 | particular customer location must be evaluated with the above understanding of      |
| 14 | what these two models do, and do not do, in regards to distribution cable           |
| 15 | modeling. For example, the BCPM 3.1 Model Methodology makes the following           |
| 16 | false and very misleading statement when it states that, "BCPM places cable to      |
| 17 | the actual customer locations, rather than moving the customers to some             |
| 18 | hypothetical distribution cable network" (BCPM 3.1 Methodology, Pg. 34, with        |
| 19 | italics added for emphasis). The truth is that neither mcdel designs a distribution |
| 20 | cable to each and every precise customer location, and neither model physically     |
| 21 | "moves customers."  |
| 22 |   |
| 23 | The relevant issue then is to determine which model has the most accurate, most     |
| 24 | reasonable, least-cost, most-efficient methodology based on currently available     |
| 25 | technology for modeling sufficient distribution cable and structure investment to   |
|    |   |

serve all of the customers located in the CSA/DA. The relevant evaluation

27 criteria are:

28

26

· precisely locating customers,

## REDACTED.DOC

| 1  |    | <ul> <li>clustering customers into CSA/DAs in a manner consistent with that of an</li> </ul>     |
|----|----|--|
| 2  |    | OPS Engineer,  |
| 3  |    | <ul> <li>cost-effectively sizing the CSA/DAs,</li> </ul>   |
| 4  |    | <ul> <li>realistically shaping the CSA/DAs,</li> </ul>   |
| 5  |    | <ul> <li>determining the center of the CSA/DAs relative to the customer</li> </ul>               |
| ú  |    | locations,   |
| 7  |    | <ul> <li>determining the number of FDIs needed,</li> </ul>                                       |
| 8  |    | <ul> <li>laying out the distribution cable grid in realistic and cost-efficient</li> </ul>       |
| 9  |    | configuration (e.g., rectangular lots),  |
| 10 |    | <ul> <li>sufficiently sizing the distribution cables to serve existing customers only</li> </ul> |
| 11 |    | with appropriate administrative and maintenance spare capacity, and                              |
| 12 |    | <ul> <li>conforming to transmission requirements for loop resistance and loss.</li> </ul>        |
| 13 |    |  |
| 14 |    | The CSA/DA modeling methodology, assumptions and input values of HM 5.0a                         |
| 15 |    | are superior to those of BCPM 3.1 in regards to each of the above criterion.                     |
| 16 |    |  |
| 17 | Q. | DOES THE BCPM 3.1 METHODOLOGY FOR MODELING CSAs  |
| 18 |    | PRODUCE THE LEAST-COST, MOST-EFFICIENT, FORWARD-   |
| 19 |    | LOOKING AND REASONABLE LOCAL LOOP MODEL BASED ON   |
| 20 |    | CURRENTLY AVAILABLE TECHNOLOGY?  |
| 21 | Α. | Absolutely not. There are two major shortcomings in the BCPM 3.1                                 |
| 22 |    | methodology for modeling CSAs that result in an overestimate of network costs                    |
| 23 |    | with an excessive number of DLC RT locations. The BCPM 3.1 CSAs are                              |

Page 43

1

1.11

| а. | a too small accorrectionly because they are derived for beneath the                    |
|----|--|
| 1  | <ul> <li>too small geographically because they are designed far beneath the</li> </ul> |
| 2  | maximum distribution cable distance reachable with currently available                 |
| 3  | technology, and  |
| 4  | · too small in terms of the number of customers served because the                     |
| 5  | maximum line threshold for an ultimate grid CSA is well below the                      |
| 6  | capacity of the DLC RT to serve customers in a CSA.                                    |
| 7  |  |
| 8  | There is a major difference between HM 5.0a and BCPM 3.1 regarding the                 |
| 9  | design of distribution cable lengths from the DLC RT. The ILEC proponents              |
| 10 | incorrectly emphasize that BCPM 3.1 designs an outside plant network that              |
| 11 | maximizes loop lengths for copper at 12,000 feet. For example, the BCPM 3.1            |
| 12 | proponents make the following partially true statements (with italics added for        |
| 13 | emphasis):   |
| 14 | The engineering protocols most central to the design of this model                     |
| 15 | include a maximum loop length for each CSA that is less than 12,000                    |
| 16 | feet. To ensure attainment of this standard, the maximum ultimate grid                 |
| 17 | size is typically constrained to 1/25th of a degree of latitude and                    |
| 18 | longitude (BCPM 3.1 Description, Pg. 42).  |
| 19 |  |
| 20 | BCPM 3.1 constrains the size of the ultimate grids to be no larger than                |
| 21 | approximately 12,000 feet by 14,000 feet. The rationale for this                       |
| 22 | constraint on the ultimate grid size is to limit copper loop lengths from              |
| 23 | the DLC to the farthest customer to approximately 12,000 feet (Bowman                  |
| 24 | Direct, Pg. 4).  |
| 25 | - B. J.  |
| 26 | By utilizing the DSC architecture and the maximum 12 Kft copper loop,                  |
| 27 | BCPM3 assures that the requirements for advanced telecommunications                    |
| 28 | service access for remote rural customers is reasonably comparable to the              |
| 29 | enjoyed by urban customers, as mandated by the 1996 Act (Bowman                        |
| 30 | Direct, Exhibit RMB 3, Pg. 9).   |
| 31 | Direct, Exhibit Rives 5, Fg. 9).   |
| 32 | The whole truth in regards to this matter is that BCPM 3.1 routinely designs           |
| 33 | copper loops in excess of 12,000 feet in length from the DLC RT because it adds        |
| 34 | partial grids to the 12,000 x 14,000 foot ultimate grids. This is quite evident        |
|    |  |

| 1  |    | from the following statements from the BCPM 3.1 Model Methodology itself         |
|----|----|--|
| 2  |    | (with italics added for emphasis):   |
| 3  |    | BCPM 3.1 - Tends to limit average copper loop lengths from the DLC to            |
| 4  |    | the customer by generally limiting the maximum ultimate grid size to             |
| 5  |    | 12,000 feet by 14,000 feet, latitude and longitude. If copper cable              |
| 6  |    | lengths from the DLC to the customer exceed 12,000 feet, the cable               |
| 7  |    | gauge is reduced to 24 gauge cable and extended range plug-ins are               |
| 8  |    | installed on loops extending beyond 13,600 feet. The ultimate grids are          |
| 9  |    | designed such that copper 1 op lengths from the DLC to the customer are          |
| 10 |    | unlikely to exceed 18,000 fe-1. (BCPM Description, Pg. 125).                     |
| 11 |    | uninely to exceed 10,000 Jen. (BCPM Description, Fg. 125).                       |
|    |    | The design of the ultimate wide surgery that the mentioner common form           |
| 12 |    | The design of the ultimate kinds ensures that the maximum copper loop            |
| 13 |    | length from the DLC site to the customer for any individual customer             |
| 14 |    | should not exceed 18,000 feet. (BCPM 3.1 Description, Pg. 42)                    |
| 15 |    |  |
| 16 |    | Thus, BCPM 3.1 clearly allows for copper loops of up to 18,000 feet, and         |
| 17 |    | occasionally even further, from the DLC RT in its distribution network. It is an |
| 18 |    | indisputable fact that currently vailable DLC technology will support            |
| 19 |    | distribution cable lengths up to 18,0 0 feet from the DLC RT. And, both HM       |
| 20 |    | 5.0a and BCPM 3.1 design loops to t <sup>1</sup> is limit.                       |
| 21 |    |  |
| 22 |    | The telling difference is that HM 5.04 designs up to 18,000 foot copper loops    |
| 23 |    | purposefully because it conforms to network transmission design standards and    |
| 24 |    | produces a least-cost network design. On the other hand, BCPM 3.1 designs up     |
| 25 |    | to 18,000 foot copper loops on an exception basis due to the arbitrarily fixed   |
| 26 |    | dimensions of its grid structure   |
| 27 |    |  |
| 28 | Q. | DOES BCPM 3.1 "ENSURE" SUPERIOR TRANSMISSION QUALITY                             |
| 29 |    | AND "ASSURE ADVANCED TELECOMMUNICATIONS SERVICES"                                |
| 30 |    | BY "CONSTRAINING" COPPER LOOPS TO 12,000 FEET?                                   |
|    |    |  |

Page 45

1

| <ul> <li>begs a question regarding the quality of service the proponents of BCPM believe they would be providing to those customers who are actually modeled BCPM 3.1 to be more than 12,000 feet from the DLC RT.</li> <li>BCPM 3.1 states as an objective the minimization of the distribution portion the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-of most-efficient network design. On the other hand, HM 5.0a seeks to maxing the distribution portion of the plant in order to minimize the number of conditional portion of the plant in order to minimize the number of conditional subfeeder cable and structure require reach them. Sensitivity runs of HM 5.0a with the maximum distribution contained to 12,000 feet have actually produced higher loop costs. It is because the expected reductions in distribution cable investment are more offset by increased investments in feeder cable and structure and additional It RT sites.</li> <li>It is commonly understood in the local loop telecommunications industry that ultimate minimization of distribution cable length is achieved by putting if feeder further into the network and closer to the customer in what is know Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplot FTTC on a wide scale basis for the simple reason that it is a very costly network.</li> </ul>  |    |    | 38   |
|---|----|----|--|
| 3       believe they would be providing to those customers who are actually modeled         4       BCPM 3.1 to be more than 12,000 feet from the DLC RT         5       5         6       BCPM 3.1 states as an objective the minimization of the distribution portion         7       the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-of         8       most-efficient network design. On the other hand, HM 5.0a seeks to maxin         9       the distribution portion of the plant in order to minimize the number of co         10       DLC RT locations and the additional subfeeder cable and structure require         11       reach them. Sensitivity runs of HM 5.0a with the maximum distribution of         12       length constrained to 12,000 feet have actually produced higher loop costs.         13       is because the expected reductions in distribution cable investment are more         14       offset by increased investments in feeder cable and structure and additional 1         15       RT sites.         16       11         17       It is commonly understood in the local loop telecommunications industry that         18       ultimate minimization of distribution cable length is achieved by putting 1         19       feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not depl | 1  | Α. | No. Not only has this been incorrectly stated by the ILEC proponents, but it       |
| 4       BCPM 3.1 to be more than 12,000 feet from the DLC RT         5       5         6       BCPM 3.1 states as an objective the minimization of the distribution portion         7       the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-or         8       most-efficient network design. On the other hand, HM 5.0a seeks to maxim         9       the distribution portion of the plant in order to minimize the number of cor         10       DLC RT locations and the additional subfeeder cable and structure require         11       reach them. Sensitivity runs of HM 5.0a with the maximum distribution or         12       length constrained to 12,000 feet have actually produced higher loop costs.         13       is because the expected reductions in distribution cable investment are more         14       offset by increased investments in feeder cable and structure and additional I         15       RT sites.         16       17         17       It is commonly understood in the local loop telecommunications industry that         18       ultimate minimization of distribution cable length is achieved by putting I         19       feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not depleded         21       FTTC on a wide scale basis for the simple reason that it is a very co | 2  |    | begs a question regarding the quality of service the proponents of BCPM 3.1        |
| 5         6       BCPM 3.1 states as an objective the minimization of the distribution portion         7       the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-or         8       most-efficient network design. On the other hand, HM 5.0a seeks to maxim         9       the distribution portion of the plant in order to minimize the number of co         10       DLC RT locations and the additional subfeeder cable and structure require         11       reach them. Sensitivity runs of HM 5.0a with the maximum distribution of         12       length constrained to 12,000 feet have actually produced higher loop costs.         13       is because the expected reductions in distribution cable investment are more         14       offset by increased investments in feeder cable and structure and additional I         15       RT sites.         16       11         17       It is commonly understood in the local loop telecommunications industry that         18       ultimate minimization of distribution cable length is achieved by putting I         19       feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deple         21       FTTC on a wide scale basis for the simple reason that it is a very costly network  | 3  |    | believe they would be providing to those customers who are actually modeled by     |
| <ul> <li>BCPM 3.1 states as an objective the minimization of the distribution portion</li> <li>the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-or</li> <li>most-efficient network design. On the other hand, HM 5.0a seeks to maxin</li> <li>the distribution portion of the plant in order to minimize the number of co</li> <li>DLC RT locations and the additional subfeeder cable and structure require</li> <li>reach them. Sensitivity runs of HM 5.0a with the maximum distribution or</li> <li>length constrained to 12,000 feet have actually produced higher loop costs.</li> <li>is because the expected reductions in distribution cable investment are more</li> <li>offset by increased investments in feeder cable and structure and additional I</li> <li>RT sites.</li> </ul> 16 17 It is commonly understood in the local loop telecommunications industry that 18 ultimate minimization of distribution cable length is achieved by putting I 19 feeder further into the network and closer to the customer in what is know 20 Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deple 21 FTTC on a wide scale basis for the simple reason that it is a very costly network  | 4  |    | BCPM 3.1 to be more than 12,000 feet from the DLC RT                               |
| 7       the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-ormost-efficient network design. On the other hand, HM 5.0a seeks to maximate the distribution portion of the plant in order to minimize the number of constrained to DLC RT locations and the additional subfeeder cable and structure require reach them. Sensitivity runs of HM 5.0a with the maximum distribution of length constrained to 12,000 feet have actually produced higher loop costs.         12       length constrained to 12,000 feet have actually produced higher loop costs.         13       is because the expected reductions in distribution cable investment are more offset by increased investments in feeder cable and structure and additional I RT sites.         16       17         18       ultimate minimization of distribution cable length is achieved by putting I feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplot         21       FTTC on a wide scale basis for the simple reason that it is a very costly network.  | 5  |    |  |
| <ul> <li>most-efficient network design. On the other hand, HM 5.0a seeks to maximum the distribution portion of the plant in order to minimize the number of constrained to 12 pLC RT locations and the additional subfeeder cable and structure requires reach them. Sensitivity runs of HM 5.0a with the maximum distribution of length constrained to 12,000 feet have actually produced higher loop costs.</li> <li>is because the expected reductions in distribution cable investment are more offset by increased investments in feeder cable and structure and additional I RT sites.</li> <li>It is commonly understood in the local loop telecommunications industry that ultimate minimization of distribution cable length is achieved by putting feeder further into the network and closer to the customer in what is know Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deploe TTTC on a wide scale basis for the simple reason that it is a very costly network.</li> </ul>  | 6  |    | BCPM 3.1 states as an objective the minimization of the distribution portion of    |
| <ul> <li>the distribution portion of the plant in order to minimize the number of conditional DLC RT locations and the additional subfeeder cable and structure requires reach them. Sensitivity runs of HM 5.0a with the maximum distribution of length constrained to 12,000 feet have actually produced higher loop costs.</li> <li>is because the expected reductions in distribution cable investment are more offset by increased investments in feeder cable and structure and additional I RT sites.</li> <li>It is commonly understood in the local loop telecommunications industry that ultimate minimization of distribution cable length is achieved by putting feeder further into the network and closer to the customer in what is know Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deple</li> <li>FTTC on a wide scale basis for the simple reason that it is a very costly network.</li> </ul>   | 7  |    | the plant (BCPM 3.1 Methodology, Pg. 24), which is contrary to a least-cost,       |
| 10       DLC RT locations and the additional subfeeder cable and structure require         11       reach them. Sensitivity runs of HM 5.0a with the maximum distribution of         12       length constrained to 12,000 feet have actually produced higher loop costs.         13       is because the expected reductions in distribution cable investment are more         14       offset by increased investments in feeder cable and structure and additional I         15       RT sites.         16       17         17       It is commonly understood in the local loop telecommunications industry that         18       ultimate minimization of distribution cable length is achieved by putting 10         19       feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplot         21       FTTC on a wide scale basis for the simple reason that it is a very costly network  | 8  |    | most-efficient network design. On the other hand, HM 5.0a seeks to maximize        |
| <ul> <li>reach them. Sensitivity runs of HM 5.0a with the maximum distribution of</li> <li>length constrained to 12,000 feet have actually produced higher loop costs.</li> <li>is because the expected reductions in distribution cable investment are more</li> <li>offset by increased investments in feeder cable and structure and additional I</li> <li>RT sites.</li> <li>It is commonly understood in the local loop telecommunications industry that</li> <li>ultimate minimization of distribution cable length is achieved by putting if</li> <li>feeder further into the network and closer to the customer in what is know</li> <li>Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplo</li> <li>FTTC on a wide scale basis for the simple reason that it is a very costly network</li> </ul>   | 9  |    | the distribution portion of the plant in order to minimize the number of costly    |
| 12       length constrained to 12,000 feet have actually produced higher loop costs.         13       is because the expected reductions in distribution cable investment are more         14       offset by increased investments in feeder cable and structure and additional I         15       RT sites.         16       17         17       It is commonly understood in the local loop telecommunications industry that         18       ultimate minimization of distribution cable length is achieved by putting in         19       feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplot         21       FTTC on a wide scale basis for the simple reason that it is a very costly network   | 10 |    | DLC RT locations and the additional subfeeder cable and structure required to      |
| <ul> <li>is because the expected reductions in distribution cable investment are more</li> <li>offset by increased investments in feeder cable and structure and additional I</li> <li>RT sites.</li> <li>It is commonly understood in the local loop telecommunications industry that</li> <li>ultimate minimization of distribution cable length is achieved by putting i</li> <li>feeder further into the network and closer to the customer in what is know</li> <li>Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplo</li> <li>FTTC on a wide scale basis for the simple reason that it is a very costly network</li> </ul>   | 11 |    | reach them. Sensitivity runs of HM 5.0a with the maximum distribution cable        |
| 14       offset by increased investments in feeder cable and structure and additional I         15       RT sites.         16   | 12 |    | length constrained to 12,000 feet have actually produced higher loop costs. This   |
| 15       RT sites.         16   | 13 |    | is because the expected reductions in distribution cable investment are more than  |
| 16         17       It is commonly understood in the local loop telecommunications industry that         18       ultimate minimization of distribution cable length is achieved by putting to         19       feeder further into the network and closer to the customer in what is know         20       Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deploy         21       FTTC on a wide scale basis for the simple reason that it is a very costly network  | 14 |    | offset by increased investments in feeder cable and structure and additional DLC   |
| 17It is commonly understood in the local loop telecommunications industry that18ultimate minimization of distribution cable length is achieved by putting 119feeder further into the network and closer to the customer in what is know20Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplo21FTTC on a wide scale basis for the simple reason that it is a very costly network  | 15 |    | RT sites.  |
| <ul> <li>ultimate minimization of distribution cable length is achieved by putting 1</li> <li>feeder further into the network and closer to the customer in what is know</li> <li>Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplo</li> <li>FTTC on a wide scale basis for the simple reason that it is a very costly network</li> </ul>  | 16 |    |  |
| <ul> <li>feeder further into the network and closer to the customer in what is know</li> <li>Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplo</li> <li>FTTC on a wide scale basis for the simple reason that it is a very costly network</li> </ul>   | 17 |    | It is commonly understood in the local loop telecommunications industry that the   |
| <ul> <li>Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deplo</li> <li>FTTC on a wide scale basis for the simple reason that it is a very costly network.</li> </ul>  | 18 |    | ultimate minimization of distribution cable length is achieved by putting fiber    |
| 21 FTTC on a wide scale basis for the simple reason that it is a very costly network  | 19 |    | feeder further into the network and closer to the customer in what is known as     |
|   | 20 |    | Fiber-to-the Curb ("FTTC") architecture. However, ILECs have not deployed          |
| 22 architecture. This is even more true for the basic types of narrowband service   | 21 |    | FTTC on a wide scale basis for the simple reason that it is a very costly network  |
|   | 22 |    | architecture. This is even more true for the basic types of narrowband services to |

23 be supported by these networks, especially in rural areas.

24

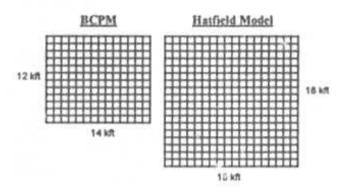
REDACTED.DOC

OSP Engineering design guidelines typically state limits that assure 1 2 quality transmission performance of the network. Both BCPM 3.1 and HM 5.0a agree that the maximum limit for copper distribution cable is 18,000 feet from the 3 DLC RT. HM 5.0a very purposefully designs non-loaded copper distribution 4 loops out to 18,000 feet from the DLC RT and models subsidiary remote 5 terminals on T1 extensions to "outlier clusters" or copper cable far beyond 6 18,000 feet (HM 5.0a Description, Sec. 6.2 and HM 5.0a, IP, Sec. 2.8) because 7 this is the least-cost, most-efficient network design utilizing currently available 8 technology. 9

11 The following diagrams compare the geographical coverage of just the copper 12 distribution cables for these two differing modeling assumptions:

13

10



14

Furthermore, the effective geographice! area covered from a single DLC RT by the HM 5.0a is actually even more than 93% greater than the 12 Kft x 14 Kft CSA of the BCPM 3.1 (as illustrated above) when the road cables on the T1 extensions to "outlier clusters" are taken into consideration.

19

REDACTED.DOC

| 1  |    | The conclusion from these diagrams is that the BCPM 3.1 must model many           |
|----|----|---|
| 2  |    | more CSAs to cover the same geographical area. The consequences of this           |
| 3  |    | aspect of the BCPM 3.1 modeling methodology are excessive fixed investments       |
| 4  |    | and recurring operations and maintenance cost for many more DLC RTs. These        |
| 5  |    | costly consequences are even more profound in the extensive rural geographical    |
| 6  |    | areas, which are the primary areas for support from the Universal Service Fund.   |
| 7  |    |   |
| 8  | Q. | HOW DOES THE BCPM 3.1 ASSUMPTION LIMITING THE                                     |
| 9  |    | MAXIMUM NUMBER OF LINES SERVED IN EACH CSA TO 999                                 |
| 10 |    | RESULT IN EXCESSIVE COSTS?  |
| 11 | A. | The second costly flaw in the CSA modeling methodology of BCPM 3.1 is that        |
| 12 |    | the maximum number of lines modeled for each CSA is simply too few based on       |
| 13 |    | the most economic application of currently available technology. The BCPM 3.1     |
| 14 |    | preprocessing program limits ultimate grids (i.e., CSAs) to a maximum of 999      |
| 15 |    | lines (BCPM 3.1 Description, Pg. 119).  |
| 16 |    |   |
| 17 |    | A BCPM 3.1 witness states that "a Carrier Serving Area typically contains no      |
| 18 |    | more than 1,000 living units, while a Distribution Area typically contains 200 to |
| 19 |    | 600 living units" (Bowman Direct, Pg. 6 with italics added for emphasis). This    |
| 20 |    | statement clearly shows that the BCPM 3.1 modeling methodology for sizing         |
| 21 |    | CSAs and DAs is based on the backward-looking inefficiencies of the embedded      |
| 22 |    | network in violation of the long-run, least-cost principles in the FCC guidelines |
| 23 |    | for these models. This preprocessing assumption drives excessive costs into the   |
| 24 |    | BCPM 3.1 network because it models many more CSAs and with excessive fixed        |
|    |    |   |

investments and recurring operations and maintenance cost for many more DLC RTs than does HM 5.0a.

| 3  |   |
|----|---|
| 4  | A "least-cost, most-efficient" network design based on "currently available         |
| 5  | technology" would seek to maximize the utilization of the 1,800 line capability     |
| 6  | (i.e., 90% of 2,016 line capacity) of the DLC RT serving a CSA without              |
| 7  | exceeding the limitation of 18,000 feet of copper distribution cable. The BCPM      |
| 8  | 3.1 modelers do support a DLC RT site capable of 2,016 lines and do agree that      |
| 9  | 2,016 line DLC systems optimize the utilization of fiber feeder cables (BCPM 3.1    |
| 10 | Description, Pg. 49). However, BCPM 3.1 has a maximum threshold of 999              |
| 11 | lines per CSA, which is far below the "most-efficient" 2,016-line capacity of a     |
| 12 | DLC RT site. Thus, the BCPM 3.1 modeling assumption of a 999 line maximum           |
| 13 | CSA results in a network design that is certainly not "least-cost, most-efficient." |
| 14 |   |
| 15 | All of the unnecessary additional DLC RT sites modeled by the BCPM 3.1 drive        |
| 16 | excessive costs, because each one has incremental investment associated with:       |
| 17 | <ul> <li>site acquisition and preparation,</li> </ul>                               |
| 18 | <ul> <li>cabinetry (or perhaps huts and CEVs),</li> </ul>                           |
| 19 | <ul> <li>common equipment,</li> </ul>   |
| 20 | <ul> <li>standard and emergency power source,</li> </ul>                            |
| 21 | <ul> <li>additional strands in the main fiber feeder cables,</li> </ul>             |
| 22 | <ul> <li>subfeeder fiber cables with associated structure</li> </ul>                |
| 23 | <ul> <li>and optical patch panel.</li> </ul>  |
| 24 |   |

REDACTED.DOC

1

2

| 12 | According to Mr. Pitkin, the BCPM 3.1 networks modeled by the ILECs for                       |
|----|---|
| 1  | recording to built than, the perint of herbories moneted by the hards for                     |
| 2  | Florida in this proceeding include 223 CSAs that have only one customer                       |
| 3  | location. Thus, BCPM 3.1 models each of these customer locations with the                     |
| 4  | exorbitant costs of its own dedicated feeder fibers and its own dedicated DLC                 |
| 5  | RT. The cost-effective HM 5.0a alternative for narrowband services is to model                |
| 6  | isolated individual and tiny groups of customers as "outlier clusters" on T1 road             |
| 7  | cables from a "main cluster" CSA. BCPM 3.1 is definitely not the "least-cost,                 |
| 8  | most-efficient" network model for isolated customer locations based on                        |
| 9  | "currently available technology," and thus it inflates the loop cost basis for the            |
| 10 | Universal Service Fund.   |
| 11 |   |
| 12 | Furthermore, there are greater operational expenses resulting from having a                   |
| 13 | larger number of DLC RT sites (e.g., maintaining service during a power failure).             |
| 14 | Thus, the BCPM 3.1 does not use the forward-looking, least-cost, most-efficient               |
| 15 | engineering design for determining the number of CSAs and DAs, particularly                   |
| 16 | when compared to HM 5.0a.   |
| 17 |   |
| 18 | CSAs and DAs in a forward-looking model should be modeled based on                            |
| 19 | <ul> <li>clustering customer locations that are within reasonable proximity to one</li> </ul> |
| 20 | another,  |
| 21 | <ul> <li>keeping natural clusters of customers together,</li> </ul>                           |
| 22 | <ul> <li>utilizing the transmission design capabilities of currently available</li> </ul>     |
| 23 | technology, and   |
| 24 | <ul> <li>allowing the cost-efficient utilization of the maximum size of IDLC</li> </ul>       |
| 25 | system (2,016 lines) and FDI (7,200 pairs).   |
|    | REDACTED.DOC Page 50  |

| 1  |      |  |
|----|------|--|
| 2  |      | The CSA/DA modeling methodology, assumptions and input valuez of HM 5.0a                   |
| 3  |      | are superior to those of BCPM 3.1 in regards to the above criteria.                        |
| 4  |      |  |
| 5  | Q.   | WHAT IS THE CARRIER SERVING AREA CONCEPT?  |
| 6  | Α.   | The CSA Concept is an OSP Engineering guideline that was formulated around                 |
| 7  |      | 1980 and has been documented as a part of the record for this proceeding                   |
| 8  |      | (Bowman Direct, Exhibit RMB 3, Pg. 6). The source document for the CSA                     |
| 9  |      | design criteria used by the BCPM modelers is the Lucent Technologies (formerly             |
| 10 |      | AT&T) Outside Plant Engineering Handbook (BCPM 3-1 Description, Pg. 18).                   |
| ĥ. |      | Incidentally, I was a member of the AT&T OSP organization that did the 1994                |
| 12 |      | update of the handbook. The relevant parts of the CSA Concept for this                     |
| 13 |      | proceeding are (with italics added for emphasis):  |
| 14 |      | <ul> <li>No loop can exceed 900 ohms of resistance, which generally equates to:</li> </ul> |
| 15 |      | - 9,000 feet of 26 gauge copper cable or   |
| 16 |      | - 12,000 feet of 24 gauge copper cable. [Note: cables with 26 gauge                        |
| 17 |      | copper conductors are smaller, less costly and have greater resistance                     |
| 18 |      | and loss than 24 gauge cables.]  |
| 19 |      | • Extended range line cards are available which extend the range of the                    |
| 20 |      | DLC remote terminal beyond 12,000 feet.  |
| 21 |      |  |
| 22 | Q.   | DOES BCPM 3.1 CONFORM TO THE CSA CONCEPT?  |
| 23 | Α.   | No. The ILEC proponents have incorrectly implied that BCPM 3.1 is designed                 |
| 24 |      | around and conforms to the CSA Concept as evidenced by the following                       |
| 25 |      | statements (with italics added for emphasis):  |
|    | RED/ | ACTED.DOC Page 51  |

| 1        | CSA engineering guidelines do not recommend copper loop lengths  |
|----------|--|
| 2        | greater than 12,000 feet The 26/24 gauging used in the distribution  |
| 3        | takes into account the industry standard 900 ohm Carrier Serving Area  |
| 4        | (CSA) design criteria of no more than 12,000 feet of copper regardless   |
| 5        | of gauge. (BCPM Description, Pg. 18)   |
| 6        |  |
| 7        | These engineering constraints conform to the specifications of a   |
| 8        | forward-looking, efficient network design. That efficient network is   |
| 9        | based on the designation of a Carrier Serving Area. A Carrier Serving  |
| 10       | Area is a standard telephone design concept that consists of a geographic  |
| 1        | area that can be served by a single digital loop carrier (DLC) site.   |
| 12       | (Bowman Direct, Pg. 4)   |
| 13       |  |
| 4        | The Carrier Serving Area (CSA) concept was specifically designed to  |
| 15       | allow for access to advance telecommunications services within the   |
| 16       | context of an efficient local exchange distribution network. (Bowman   |
| 17       | Direct, Exhibit RMB 3, Pg. 7)  |
| 18       |  |
| 19       | Yet, the truth is that the BCPM 3.1 does not conform to the "constraints" of the   |
| 20       | CSA Concept as evidenced by the following enlightening statements from the   |
| 21       | ILEC testimonies (with italics added for emphasis):  |
| 22       | BCPM 3.1 uses 24 gauge cable only when the copper loop from the DLC  |
| 23       | to the furthest customer exceeds 11,100 feet. This distance is based on  |
| 24       | complying with engineering standards for the maximum dB loss   |
| 2.5      | permissible to maintain adequate service quality. An extended range line   |
| 26       | card is included for loops that extend beyond 13,600 feet from the DLC   |
| 27       | to the customer. This also is an engineering standard, but is a user   |
| 28       | adjustable input in the model. (Bowman Direct, Pg. 5)  |
| 29       | adherment adhar ar ann ann ann an ann a' Brail   |
| 30       | BCPM 3.1 uses 26/24 gauge cable in distribution. 12,000 ft of 26 gauge   |
| 31       | copper has resistance value of 999.6 ohms (83.3.ohms per thousand feet   |
| 32       | @ 68deg.), well within the 1500 ohm supervisory limit of today's digita  |
| 33       | switches. The 26/24 gauging used in the distribution takes into account  |
| 34       | the industry standard 900 ohm Carrier Serving Area (CSA) design criteria   |
| 35       | of no more than 12,000 feet of copper regardless of gauge. In the few  |
| 36       | cases where BCPM 3.1 finds grid Quadrants with copper loops greater  |
| 37       | than 12,000 and up to 18,000 feet in the distribution network, it uses the   |
| 38       | Extended CSA (ECSA) design with 24 gauge cable throughout that   |
|          |  |
| 39       | quadrant. Extended range line cards are used to serve all customers in   |
| 40       | the distribution area (Grid quadrant) for distribution distances over  |
| 41       | 13,600 feet. (BCPM 3.1 Methodology, Pg. 18 - 19)   |
| 42       | With a set of the local of the set of the se |
| 43       | Within a grid, if the length of copper from the DLC to the last lot in a   |
| 44       | quadrant is less than 11,100 feet, 26 gauge cable is used to serve all   |
| 45<br>46 | customers. In those circumstances where the distance from the DLC to<br>the last lot is greater than 11,100 feet, 24 gauge wire is used in all cables  |
|          | the last lot is provident from 11 100 first 34 measure trians is trand in all and lot  |

Where distances exceed 13,600 feet, to and within the quadrant. 1 extended range plug-ins are installed on lines that exceed 13,600 feet. 2 (BCPM 3.1 Methodology, Pg. 54 - 55) 3 4 5 Thus, BCPM 3.1 clearly violates the CSA Concept in the following four ways: 6 BCPM 3.1 models 26 gauge cable out to 11,100 feet from the DLC RT. 7 which clearly exceeds the 9,000 foot limit on 26 gauge cable of the CSA я Concept The 9,000 foot CSA Concept limit on 26 gauge cable is based 9 on cable loss, not 900 ohms of resistance. Therefore, BCPM 3.1 would 10 appear to be modeling customers that are located 9,000 to 11,100 feet 11 from the DLC RT with excessive loss and thus poor quality service. 12 There is no BCPM 3.1 supporting documentation (like the HAI 5.0a 13 Inputs Portfolio) that explains how or why the BCPM developers 14 changed the CSA Concept maximum loop distance for 26 gauge 15 distribution cable from the DLC RT from 9,000 feet to 11,100 feet. 16 BCPM 3.1 models loops between 12,000 and 13,600 feet from the DLC 17 RT without range extension line cards in violation of the CSA Concept 18 19 requirement that all loops in excess of 12,000 feet should have range extension line cards. Do these particular BCPM 3.1 customers have 20 substandard quality service and/or impeded access to advanced services 21 on a reasonably comparable basis? Again, there is no BCPM 3.1 22 supporting documentation for this deviation from the CSA Concept. 23 BCPM 3.1 actually models the Extended (or Expanded) CSA Concept, 24 which supports the design of loops out to 18,000 feet from the DLC RT 25 BCPM 3.1 allows the distance at which the extended range line cards are 26 applied to be a user adjustable input, instead of conforming to the CSA 27

REDACTED.DOC

Concept requirement of 12,000 feet or any particular standard. The 1 statement is made that the 13,600 foot distance to begin employing range 2 extension cards "also is an engineering standard," but there is no 3 supporting documentation for this deviation from the CSA Concept. 4 5 DOES BCPM 3.1 MODEL DISTRIBUTION CABLE REALISTICALLY Q. 6 AND COST-EFFECTIVELY? 7 No. When a single lot in a DA exceeds 11,100 feet distance from the DLC RT, 8 A. BCPM 3.1 then designs all of the distribution cables to and within the DA from 9 26 gauge to more costly 24 gauge conductor cables. This is a grossly 10 oversimplified and needlessly costly modeling assumption. In the real world, 11 OSP Engineers do not simply increase the gauge of every single cable in a DA to 12 satisfy the transmission requirements of the longest loop when only a few 13 14 customers exceed the limit for 26 gauge cables. In the real world of OSP 15 Engineering, the larger distribution cables closer to the DLC RT would remain 16 26 gauge, and the smaller cables closer to the customer would be 24 gauge such that the combined 26/24 gauge loop resistance and loss would be within 17 transmission limits. 18 19 In comparison, HM 5.0a models 24 gauge copper conductors for cables less than 20

400 pairs and 26 gauge conductors for cables 400 pairs and larger (HM 5.0a IP,
 2.3.2). Since distribution cable loops more than 9,000 feet from a DLC RT of no
 greater than 1,800 line capacity will invariably be less than 400 pairs, <u>HM 5.0a</u>
 <u>does satisfy the CSA Concept constraint on 26 gauge cable distance</u>

### REDACTED DOC

Furthermore, HM 5.0a does this in a "least-cost" manner that is consistent with
 real world OSP Engineering practice.

3

### 4 Q. WHAT CSA DESIGN STANDARD DOES HM 5.0a EMPLOY?

The more cost-efficient design employed by HM 5.0a conforms to OSP 5 Α. transmission requirements for acceptable loop loss of 8.5 dB from the DLC RT 6 7 based on currently available technology. OSP Engineering guidelines are always subject to "engineering judgment", and currently available technology continually 8 drives the evolution of such guidelines. For example, when the CSA design 9 concept was originally formulated around 1980, ISDN was then limited to less 10 than 12,000 feet on copper. Such service is now routinely guaranteed to any 11 12 subscriber served on copper cable within 18,000 feet of their serving wire center.

13

19

20

21

The realistic and cost-effective gauging of the copper distribution cables by HM
 5.0a has been described above. For its Integrated DLC systems, HM 5.0a uses
 two types:

- Low density DLC system applications are based on the Advanced Fiber
   Communications UMC 1000A.
  - High density DLC system applications are based on the DSC Communications Litespan-2000.
- The line cards costed for each of these DLC systems allows for the utilization of extended range line cards as required to support distribution cable lengths out to 18,000 feet from the DLC RT. The low density DLC system, which is more likely to be deploy d in rural areas, actually uses the cost for UMC Remote REDACTED.DOC Page 55

1 Terminal Extended Range RST POTS Channel Units (R-EPOTS) for all channel 2 units. The high density DLC system uses its "regular" R-POTS channel unit to 3 meet transmission requirements for loops up to 17,600 feet from the DLC RT 4 (Exhibit \_\_\_ (JWW-5)). Should there be any instances of customers between 5 17,600 to 18,000 feet from a high density DLC system, the Litespan-2000 6 RUVG2 card is utilized.

7

In the USF Hearings in Louisiana (Docket U-20883), the Staff's Final Recommendation dated April 3, 1998, reported on page 15 (with italics added for emphasis) that, "Dr. Bowman did concede that Hatfield's [i.e., *HAI 5.0a's] use of 18,000 feet for copper cable beyond the DLC remote terminal would provide quality telecommunications services, as long as the proper electronics were installed in those instances.*" HM 5.0a does indeed use the proper electronics, which are the range extension line cards described above.

15

16Moreover, the Louisiana Staff also found (pages 17 - 18) that "the BCPM17overstates cost because the input for extended line range cards are for the more18expensive REUVG card." For comparison, the RUVG2 card, used by HM 5.0a19for any customers located between 17,600 and 18,000 feet f.om a high density20DLC RT, is approximately 25% more than the standard RPOTS card. However,21the REUVG card used by BCPM 3.1 for customers between 13,600 and 18,00022feet is twice as expensive as the standard RPOTS card.

Q. WHAT IS THE COST COMPARISON BETWEEN MODEL RUNS
 BASED ON 12,000-FOOT GRIDS VERSUS 18,000-FOOT GRIDS?

REDACTED.DOC

| 1  | Α.   | The ILEC proponents claim that "the 12,000-foot grids result in lower per-line             |
|----|------|--|
| 2  |      | loop cost than the 18,000-foot grids." (Bowman Direct, Pg. 5) This claim is not            |
| 3  |      | surprising, nor particularly persuasive, given that:                                       |
| 4  |      | <ul> <li>BCPM 3.1 defaults to all 24 gauge cable when any customer in a DA is</li> </ul>   |
| 5  |      | beyond 11,100 feet from the DLC RT.  |
| 6  |      | <ul> <li>BCPM 3.1 greatly exaggerates the cost of range extension line cards by</li> </ul> |
| 2  |      | utilizing the very expensive REUVG card beyond 13,600 feet when the                        |
| 8  |      | RPOTS card, at half the cost, is good out to 17,600 feet. At the very                      |
| 9  |      | least, BCPM 3.1 should be costing the RUVG2 card, which is only 25%                        |
| 10 |      | more expensive than the standard RPOTS card.   |
| 11 |      |  |
| 12 |      | Sensitivity runs of HM 5.0a with the maximum distribution cable length                     |
| 13 |      | constrained to 12,000 feet have actually produced higher loop costs. This is               |
| 14 |      | because the expected reductions in distribution cable investment are more than             |
| 15 |      | offset by increased investments in feeder cable and structure and additional DLC           |
| 16 |      | RT sites.  |
| 17 |      |  |
| 18 | Q.   | DO YOU HAVE OTHER TRANSMISSION CONCERNS REGARDING  |
| 19 |      | THE BCPM 3.1?  |
| 20 | Α.   | Yes. There is no explicit test in BCPM 3.1 to ensure that customers do not                 |
| 21 |      | exceed 18,000 feet in loop length from the DLC RT. The BCPM 3.1 Model                      |
| 22 |      | Methodology states that "ultimate grids are designed such that loop lengths from           |
| 23 |      | the DLC to the customer are unlikely to exceed 18,000 feet" (BCPM 3.1                      |
| 24 |      | Description, Pg. 125, with italics added for emphasis). However, BCPM 3.1                  |
| 25 |      | does indeed model customers more than 18,000 feet from the DLC RT, and Mr.                 |
|    | REDA | CTED.DOC Page 57   |

Pitkin has determined that BellSouth, GTE and Sprint have all modeled loops
 exceeding 18,000 feet from the DLC RT in this proceeding. By comparison, the
 HM 5.0a explicitly tests to ensure that no copper loops exceed the 18,000 feet
 limit from the DLC RT.

The reason that this is important is that copper loops in excess of 18,000 feet require load coils to meet transmission requirements for quality voice grade service. However, load coils are unacceptable in these models because they would inhibit the provisioning of advanced services per FCC Criterion No. 1. On the other hand, non-loaded copper loops longer than 18,000 feet from the DLC RT would violate network design standards and result in poor quality service to those customers.

13

5

# Q. DO YOU HAVE A CONCERN WITH THE BCPM 3.1 MODELING METHODOLOGY THAT PLACES FIBER FEEDER CABLE TO LARGE CAPACITY GRIDS BY DEFAULT?

17 A. Yes. The BCPM 3.1 deploys DLC systems for voice grade services rather than analog copper facilities when demand within a particular grid "exceeds the user 18 designated capacity of the largest copper distribution cable" (BCPM 3.1 19 20 Methodology, Pg. 19). I have serious engineering and economic concerns 21 regarding this modeling assumption because no consideration is given to the 22 distance of the particular grid from the wire center. Consequently, BCPM 3.1 23 will uneconomically deploy fiber and DLC to a large spariment/office building 24 directly across the street from the wire center.

25

REDACTED.DOC

This is not an acceptable assumption for a "least-cost" local loop network. The reason is that there are insufficient savings realized in the substitution of fiber feeder cable for copper feeder cable to offset the additional cost of the DLC electronics for loops generally less than 12,000 feet in total length from the wire center, which is the BCPM 3.1 copper to fiber breakpoint. So, this particular BCPM 3.1 modeling assumption is an unreasonable cost adder to the network and thus unreasonably increases the cost of an average loop.

\$

The justification offered by the BCPM proponents is that this modeling 9 10 assumption "avoids the typical duct congestion in urban rights of way where utilities and urban services vie for below ground space" (BCPM 3.1 11 Methodology, Pg. 19). That is a backward-looking justification based on the 12 ILEC's embedded network and is inconsistent with the "long-run, forward-13 looking cost" economic assumptions applicable to these models per FCC 14 15 Criterion 3. In other words, in accordance with the "scorched node" assumption, a conduit system would need to be installed anyway with sufficient 4-inch ducts 16 17 to handle whatever copper and fiber feeder cables might be required. So, 18 BCPM3.1's uneconomic substitution of one fiber cable with substantial DLC 19 system costs instead of placing two, more economical copper cables, saves only 20 the minimal cost of one duct and certainly avoids no congestion.

21

HM 5.0a, on the other hand, performs a life cycle cost analysis of fiber versus
 copper feeder on the route to determine if fiber with DLC is the more economical
 alternative (HM 5.0a Description, Sec. 6.3.5). Thus, the HM 5.0a model

REDACTED.DOC

methodology again more realistically represents the decision process of an OSP
 Engineer in designing a feeder route.

Q. DOES BCPM 3.1 SYSTEMATICALLY OVERSTATE THE AMOUNT OF
 DISTRIBUTION CABLE REQUIRED BECAUSE IT MODELS SQUARE
 LOTS?

A. Yes. The BCPM 3.1 developers continue to assert the assumption that customer
 locations should be modeled as square lots. This is not only unrealistic; it results
 in the modeling of excessive distribution cable and associated structure
 investment. HM 5.0a makes a much more realistic assumption that lots are
 rectangular based on observations of a number of zoning maps and field
 experience.

14

34

Furthermore, as will be detailed below, city and subdivision planners know that any given geographical area can be served with fewer streets, sidewalks, sewers, streetlights, etc. if the lots are rectangular rather than square. Since utilities typically follow the streets or rear lot lines, it follows that rectangular lot layouts are also more efficient and less costly for the power, water, cable and telecommunications utilities to serve their customers as illustrated by the diagrams in Exhibit (JWW-6).

22

The square lot assumption that has been perpetuated in BCPM 3.1 results in more distribution cable than would be necessary with rectangular lots. Let's consider two generic examples. Assume there are 256 households within a DA.

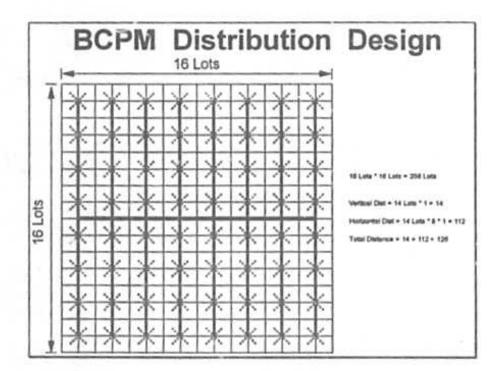
### REDACTED.DOC

The square DA in the BCPM 3.1 will have 256 square lots, or 16 by 16 as can be

seen below.

3

2



- Each square lot represents a customer location with a drop going to it (dotted line). The thicker lines represent the distribution cable needed to reach each customer location. For simplicity sake let's assume the area of each lot is one. This means each side of a lot has a length and a width of one. Thus, from the diagram one can see that the amount of distribution cable needed by the BCPM 3.1 in this example is enough to run past 126 lots.
- 12

4

5

6

7

8

9

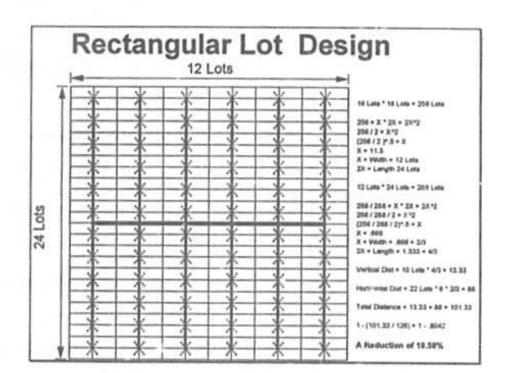
10

11

Now consider the next diagram, which roughly represents the way rectangular customer locations could be distributed within the same DA. The total DA remains the same; however, in order to fit this into a square serving area that is somewhat similar, I have taken the liberty of using 288 lots to avoid rounding REDACTED.DOC Page 61

1

problems. Again, to be conservative, we will assume that the HAI Model will
 design the distribution cable to reach all 288 lots in this DA, and that none are
 empty. Refer to the following figure to see how the HAI Model designs the
 distribution plant.



6

5

8 Recall the BCPM 3.1 DA was 256 lots. The area of each lot in BCPM 3.1 was 9 1. The area of each lot in the HAI Model is the distribution area divided by the 10 number of lots, 256/288 = 5/9. Since the length of a lot is twice its width in HM 11 5.0a, the width must be 2/3. You can see that this is correct by multiplying the 12 width times twice the width,  $2/3^{*}(2^{*}2/3) = 8/9$ . Now all we need to do is to add 13 up the cable used by the HAI Model, which equals 101.33 to serve 288 14 rectangular lots. Now, compare this number to the BCPM 3.1 design, which 15 needed cable for a distance of 126 to serve only 256 square lots.

REDACTED.DOC

The amount of distribution cable needed for the same distribution area as modeled by the HM 5.0a is 19.58% less than that modeled by the BCPM 3.1 — a significant difference that also reflects the reality of city and subdivision planning. BCPM 3.1 consistently models excessive distribution cable length to serve a modeled area of customers occupying lots of identical area.

7

1

# Q. DOES BCPM 3.1 HAVE TO LIMIT THE AMOUNT OF CABLE THAT 9 CAN BE MODELED WITHIN A DISTRIBUTION QUADRANT?

As an indication of just how seriously BCPM 3.1 overstates total 10 Α. Yes. distribution cable length, there is a check that had to be built into the BCPM 3.1 11 12 that "constrains the total length of cables (including the backbone, branch, vertical and horizontal connecting cables) within a distribution quadrant to not 13 exceed the length of the road network in that distribution quadrant (BCPM 3.1 14 15 Methodology, Pg. 54). According to Mr. Pitkin, over half of the distribution 16 quadrants have to invoke this constraint in order to limit the amount of excessive distribution cable otherwise modeled by BCPM 3.1 based on the square lot 17 18 assumption.

19

This difference in modeling assumptions between the HAI Model and the BCPM is further accentuated when the distance from the center of the street to the front of the lot is taken into consideration. The 1 x 2 rectangular lots of the HAI Model and the 1 x 1 square lots of the BCPM include the entire area being modeled and thus go to the center of the street or road. When the distance from the center of the road to the actual front of the lot, which is typically 25 - 30 feet,

REDACTED.DOC

| 1  |    | is subtracted, the HAI Model still has a rectangular lot where the depth is greater        |
|----|----|--|
| 2  |    | than its width. However, the BCPM is now left with a rectangular lot where the             |
| 3  |    | width is greater than the depth with the distribution cables having to traverse the        |
| 4  |    | longer width. This further elucidates just how unrealistic it is for BCPM 3.1 to           |
| 5  |    | model square lots.   |
| 6  |    |  |
| 7  | Q. | DOES BCPM 3.1 OVERSIZE DISTRIBUTION CABLES?  |
| 8  | A. | Yes. In regards to distribution cable sizing, the BCPM 3.1 Model Methodology               |
| 9  |    | states the following:  |
| 10 |    | · "Branch cables are sized to the number of pairs for housing units and                    |
| 11 |    | business locations. This calculation takes the number of housing units                     |
| 12 |    | times pairs per housing unit and the greater of actual business pairs per                  |
| 13 |    | location or business locations times pairs per location." (BCPM 3.1                        |
| 14 |    | Methodology, Pg. 55)   |
| 15 |    | <ul> <li>"The Model default inputs assume two pairs for a resident unit and six</li> </ul> |
| 16 |    | pairs for a business unit." (BCPM 3.1 Methodology, Pg. 56)                                 |
| 17 |    |  |
| 18 |    | These "default minimums" in BCPM 3.1 are based on a guideline from the                     |
| 19 |    | outdated practice on Detailed Distribution Area Planning (DDAP) for a minimum              |
| 20 |    | of two pairs per ultimate living unit and five pairs per small business, which may         |
| 21 |    | be modified based on the judgment of the engineer (BSP 901-350-250, Pg. 20-                |
| 22 |    | 21). However, technological advances have superseded these "minimum" values.               |
| 23 |    | For example, two-channel DSL Systems have become a viable means of rapidly                 |
| 24 |    | providing additional lines for loops up to 18,000 feet. A primary advantage of             |
| 25 |    | incorporating these systems into local loop distribution planning for additional           |
| 26 |    | lines is that the investment in two-channel DSL Systems is only needed if, when,           |
| 27 |    | and for as long as the additional customer demand is there.                                |

28

1 There is excessive cost in oversizing copper distribution cables based on 2 historically low utilization rates that can no longer be justified. The ILECs like 3 to raise a big scare over the time, expense and disruption of digging up streets and yards to place a second distribution cable or drop to serve additional 4 5 customer demand With the widespread use of two-channel DSL Systems, the addition of a second cable is no longer the primary alternative. Thus, the ILECs 6 can no longer justify exorbitant levels of spare cable pairs by using their 7 8 historically low average distribution cables utilization, typically in the 40% range 9 (Dickerson Direct, Pg. 11). Indeed, GTE's deployment practice prescribes distribution cable fills in excess of xxxx% based on the planned selective 10 utilization of two-channel DSL Systems. ILEC cable utilization rates should be 11 rising from their historical levels. 12

13

14 In regards to these historically embedded distribution cable fills, BellSouth 15 testifies that, "These [distribution cable sizing] factors are designed to produce a fill representative of BellSouth's projection of actual fill, based on experience 16 17 over time, for Florida" (Caldwell Direct, Pg. 12 with italics added for emphasis). 18 However, in response to AT&T's First Set of Interrogatories, Item No. 26, 19 which tried to ascertain the historical utilization of distribution cables, BellSouth 20 responded that, "No record is kept of distribution cable status on statewide 21 basis." Thus, BellSouth could not produce any distribution cable "actual fill, 22 based on experience over time, for Florida", and BellSouth's interrogatory 23 response appears to contradict Ms. Caldwell's testimony.

24

REDACTED DOC

1 Similarly, Sprint testifies it "calculated actual feeder fill based on working pairs 2 (cable pairs in service) divided by total pairs available as tracked in the Customer 3 Loop Assignment System, Sprint's internal system for maintaining cable pair 4 inventory" (Dickerson Direct, Pg. 10 with italics added for emphasis). However, 5 in response to AT&T's First Set of Interrogatories, Item No. 26, which tried to ascertain the historical utilization of feeder cables. Sprint responded that, 6 "Without waiving its objection. Sprint states that the information requested does 7 8 not exist." Thus, Sprint's interrogatory response appears to contradict Mr. 9 Dickerson's testimony.

10

From other proceedings that I have participated in, I know that BellSouth has reduced its distribution cable sizing guidelines for pairs per house, or living unit BellSouth, GTE and Sprint have filed 2.0 pairs per housing unit in this proceeding. However, I recommend that the BCPM 3.1 input value for distribution pairs per residential housing unit for the ILECs should be reduced to 1.5.

17

18 BCPM 3.1 takes the greater of actual business pairs per location or business 19 locations times the input value for business pairs per location. Based on data 20 from several other dockets, I know that the number of business lines per small 21 business location is definitely less than 3.0. However, BellSouth, GTE and 22 Sprint all have filed input values of 6.0 pairs per business location. This is much 23 too high given that the actual number of lines are modeled for large businesses. 24 Therefore, I recommend that the input value for the minimum number of pairs 25 per business location should be reduced from 6 to 3.

REDACTED.DOC

2 BCPM 3.1 utilizes distribution cable sizing factors to increase the demand 3 numbers that are already based on the ultimate pair requirements. In addition, 4 there is one more step of rounding up to the next discrete cable size, which is 5 necessary, but in the case of the BCPM 3.1 is based on already overinflated pair 6 requirements as detailed above. Intere tingly, the ILECs have begun to realize 7 the excess that has been built into the BCPM 3.1 distribution cable sizing 8 methodology and have more appropriately filed distribution cable sizing factors 9 ranging from 98.0% to 100.0% in this proceeding. Nevertheless, the resulting distribution cable fills are still aimed at maintaining historical embedded 10 11 utilization levels rather than "least-cost, most-efficient, forward-looking" cable 12 fills based on "currently available technolc gy."

13

1

## IS THERE ANY EMPIRICAL EVIDENCE THAT ILEC COPPER CABLE UTILIZATION RATES BEING MODELED ARE TOO LOW?

A. Yes. I believe that ILEC historical copper utilization rates, the basis upon which
 ILEC copper cable fills for BCPM 3.1 have been developed, can be shown to be
 low based on empirical evidence. This is because an excessive defective pair rate
 can be attributed in large part to excessive spare capacity, which reduces the
 incentive to clear defective copper cable pairs.

21

The cost of a loop is being estimated by the ILECs in this proceeding to be
 approximately \$1,300 per loop. The ILEC cost to clear a defective pair is \$xxxx \$xxxx per pair (ILEC Responses to AT&T's First Set of Interrogatories, Item
 No. 33). Thus, there should be ample economic incentive to clear defective cable
 REDACTED.DOC Page 67

pairs and keep the cable pair inventory in high working order, unless there was an excessive surplus of spare cable pairs.

- An acceptable defective copper pair rate in the industry is 2% 3%. AT&T's First Set of Interrogatories, Item No. 25 requested data on defective pair rates. GTE's defective pair rate was reported to be within industry standards. Furthermore, there were practices and data produced that indicate that GTE makes clearing defective pairs and effectively managing the defective pair rate a priority.
- 10

1

2

3

However, BellSouth's defective pair rate is more than xxxx times the industry standard, and growing. Furthermore, in response to AT&T's First Set of Interrogatories, Item No. 33, BellSouth responded that, "No data is kept on the quantity and percentage of copper pairs and iber stands cleared."

15

Also interesting is Sprint's response that, "Without waiving its objection, Sprint states that the information does not exist." However, in response to AT&T's First Request for Production of Document, Item No. 12, Sprint furnished an extensive practice on its "Defective Cable Identification and Prioritization Process" that appeared to include a statistical reporting system.

21

It is difficult for me to believe that an ILEC would not keep track of and try to effectively manage its defective pair rate. Unless, however, that ILEC had such a large surplus of spare cable pairs that it was actually uneconomical to expend resources to reclaim oven excessive numbers of defective pairs.

REDACTED DOC

- 1 DOES THE EMPLOYMENT OF THE TIGER ROAD NETWORK BY 2 0. THE BCPM 3.1 MAKE THE MODEL MORE REALISTIC? 3 Α. Not really. This is another modeling idea that sounds good at first, but when its 4 5 implementation in BCPM 3.1 is investigated reveals a number of concerns and 6 uncovers just how shallow the perceived benefits really are. 7 8 BCPM 3.1 relies on a straightforward premise that households and business 9 typically reside near roads (Duffy-Deno Direct, Pg. 16). However, it is the 10 converse of this premise upon which the BCPM 3.1 really operates. The actual 11 modeling premise being that the presence of a road ensures the uniform 12 distribution of households and businesses along that road. As stated in the BCPM Model Methodology, "[c]ustomers, assigned to microgrids within 13 14 distribution quadrants, are subsequently placed uniformly in Road Reduced 15 Areas" (BCPM 3.1 Methodology, Pg. 122 with italics added for emphasis). This 16 is simply not the best premise for modeling customer locations.
- 17

Indeed, there are many roads that have no households or businesses, and many roads along which customers are not uniformly distributed. In rural areas, customers tend to be more concentrated at the end of their road, which may traverse several grids without any customer locations, before it gets to them. These models are supposed to design a network to serve all of the customer locations, not all of the roads.

24

However, if a model accurately locates the customers, then it can be reasonably assumed that roads exist to reach those customers without having to identify particular roads from a separate database. This is the modeling premise of HM 5.0a.

5

6 The BCPM 3.1 Model Methodology states another simple fact that "rights of 7 way for provisioning telecom cables are most frequently found along roadways" (BCPM 3.1 Methodology, Pg. 6). Once again, if a model such as HM 5.0a 8 9 locates customers, then it can be reasonably assumed that roads exist with rights 10 of way for cables to reach those customer locations. BCPM 3.1 thus has no 11 claim to any superiority in the matter of rights of way. Furthermore, BCPM 3.1 12 makes absolutely no use of the road network information to determine pathways that engineers would use to place facilities. 13

14

15 On the contrary, the need for road right of way actually indicts another assumption in the BCPM 3.1 in that it is necessary to model sufficient route 16 distance to allow for the meandering of the road network. Typically, this is done 17 18 in HM 5.0a and the BCPM 3.1 via right angle, or rectilinear, routing of the 19 cables. However, in BCPM 3.1 the split, or angled, feeder route appears to take 20 a direct route towards "the population centroid of the entire feeder quadrant" 21 (BCPM Methodology, Pg. 43). If no allowance is made for conversion of "airline" route to "road" route distances, as is done in HM 5.0a, then the BCPM 22 23 3.1 will not model sufficient investment for the split feeder route to reach its 24 destination.

25

REDACTED.DOC

1 Any perceived added value of applying the road network to locate customers 2 below the CB level is suspect. As an example of how the road network is used 1 to allocate customers from CBs to microgrids, the BCPM 3.1 Model 4 Methodology (Pg. 30) uses an illustration of 20 miles of roads traversing a 5 microgrid. However, a microgrid is only 1,500 feet by 1,700 feet and could not 6 realistically contain a even minuscule fraction of 20 miles of roads.

7

#### 8 0. DO YOU HAVE CONCERNS WITH THE OSP SENSITIVITY ANALYSIS CAPABILITY OF THE BCPM 3.1? 9

- Yes. The BCPM 3.1 has two major, rather arbitrary, OSP network design 10 Α. 11 assumptions which cannot be readily subjected to sensitivity analysis because they 12 are only user adjustable via the cumbersome and time consuming one day 13 preprocessing application. These two assumptions are:
- 14 1. The preprocessor has a maximum threshold of 999 lines (or households plus 15 business lines) for determining if microgrids are re-aggregating to form 16 CSAs. As detailed earlier in my testimony, I believe that the BCPM 3.1 17 models far too many DLC RT sites because the number of lines modeled in 18 its CSAs and DAs is well below capacity. It is very difficult to run a 19 sensitivity analysis in the BCPM 3.1 to verify this and develop a more cost-20 efficient alternative threshold because it is only changeable in the one day preprocessing cycle. 21
- 22 The preprocessing routine has a fixed distance of 10,000 feet from every wire 23 center as the appropriate distance where it is economical and feasible to split 24 a feeder route. This is also the fixed distance where the spacing of lateral 25 subfeeder routes suddenly goes from roughly every 1,600 feet to roughly REDACTED.DOC

| 1  |      | every 13,000 feet (BCPM 3.1 Methodology, Pg. 46). The BCPM Model                   |
|----|------|--|
| 2  |      | Methodology rationale is "that within 10,000 feet [of the wire center],            |
| 3  |      | customers are generally located within the perimeter of a town and that the        |
| 4  |      | town has some sort of gridded street complex" (BCPM 3.1 Methodology,               |
| 5  |      | Pg. 43).   |
| 6  |      |  |
| 7  |      | BCPM 3.1 then applies this questionable fixed assumption to every feeder           |
| 8  |      | route in every wire center in every geographical area in Florida. Furthermore,     |
| 9  |      | there is no economic justification offered by the BCPM modelers that 10,000        |
| 10 |      | feet is the realistic or least-cost, most-efficient distance for any feeder route, |
| 11 |      | much less for every feeder route in every wire center. This number needs to        |
| 12 |      | be more easily adjustable for sensitivity testing. Furthermore, this assumption    |
| 13 |      | should be variable (perhaps in a look-up table) that is based on the size of the   |
| 14 |      | wire center and/or the density of customers along the feeder route.                |
| 15 |      |  |
| 16 | VI.  | OTHER CRITICISMS REGARDING THE HAI MODEL   |
| 17 | Q.   | WOULD YOU PLEASE RESPOND TO ANY OTHER BCPM 3.1                                     |
| 18 |      | CLAIMS OR HM 5.0a CRITICISMS REGARDING OSP?  |
| 19 | A.   | Yes. There are six.  |
| 20 |      |  |
| 21 |      | 1. The BCPM 3.1 alleges superiority in sizing distribution cables based on         |
| 22 |      | ultimate pairs per house instead of current households. There is no                |
| 23 |      | shortcoming of HM 5.0A in this regard. The distribution cable fill factors in      |
| 24 |      | HM 5.0a are more than adequate to serve the number of empty houses that            |
| 25 |      | may exceed the number of households in an area, even though this is not a          |
|    | REDA | CTED.DOC Page 72   |

| 1  |    | requirement of the model. Furthermore, the BCPM 3.1's modeling of              |
|----|----|--|
| 2  |    | distribution cables sized specifically to serve empty houses has been rejected |
| 3  |    | (Staff's Final Recommendation, LA Docket U-20833, 3/27/98, Pg. 16).            |
| 4  |    |  |
| 5  | 2. | The BCPM 3.1 Model Methodology still continues show the Hatfield Model         |
| 6  |    | Release 4.0 ("HM 4.0") methodology for distribution road cables in rural       |
| 7  |    | areas. This methodology has been totally superseded by the clustering          |
| 8  |    | algorithms of HM 5.0a. Furthermore, BCPM 3.1 continues to misrepresent         |
| 9  |    | the road cables of HM 4.0 as two cables running in a straight line from the    |
| 10 |    | center to opposite corners of the quadrant (BCPM 3.1 Methodology, App. A,      |
| 11 |    | Ex. 2). What HM 4.0 did with road cables was model road cable investment       |
| 12 |    | based on twice the rectilinear distance from the centroid to the corner of the |
| 13 |    | occupied area of the quadrant. The relevant points being that there could be   |
| 14 |    | more than two cables within the modeled total length and the total distance    |
| 15 |    | modeled is significantly understated in the BCPM 3.1 illustration.             |
| 16 |    |  |
| 17 | 3. | The BCPM proponents are also still making outdated and totally irrelevant      |
| 18 |    | assertions in regards to 85% of the rural customers modeled as being in        |
| 19 |    | towns and served via a distribution cable grid on maximum three acre lots in   |
| 20 |    | HM 4.0 (BCPM 3.1 Methodology, Pg. 24). For many months, HM 5.0a has            |
| 21 |    | modeled main and outlier clusters in a way that is more precise and            |
| 22 |    | representative of the way that local loop networks are designed. (A            |
| 23 |    | description of the OSP enhancements of HM 5.0a is covered in the direct        |
| 24 |    | testimony that I filed in this proceeding.)                                    |
| 25 |    |  |

REDACTED.DOC

1 The BCPM proponents cite a study of five states performed for the FCC that 2 concludes that 12,000-foot grids result in lower per-line loop costs than 18,000-foot grids (Bowman Direct, Pg. 5). I have little doubt regarding the 3 reported results given the longer loop cost inefficiencies inherent in the 4 5 BCPM 3.1. Specifically, the previously documented excessive costs of the 6 REUVG range extension card for all loops in excess of 13,600 feet in length and the use of 24 gauge cable only for the entire CSA when the copper loop 7 8 to any customer in the CSA exceeds 11,100 feet. If this study had been 9 conducted using the HM 5.0a assumptions of less costly RUVG2 range 10 extension card and 24 gauge for cables less than 400 pairs, the results would no doubt have been markedly different. 11 12 13 5. In regards to the sharing of buried cable trenching, it has been written that, 14 "Such proposals [for sharing buried cable trenches in the future] conveniently 15 overlook the fact that GTE's network is in place today .... With respect to buried cable, these parties [i.e., AT&T and MCI] apparently believe that GTE 16 17 will dig up its existing cable in order to immediately rebury in a shared 18 trench" (Tucek Direct, Pg. 8). These statements reflect a serious lack of 19 understanding of the "scorched node" assumption that is to be applied to 20 these models. As stated very clearly by another ILEC witness, "the BCPM 21 3.1 model assumes that the entire network is built at a single point in time". 22 (Staihr Direct, Pg. 7). 23 6 The BCPM sponsors have unilaterally declared that "data transmission over a 24 25 28.8 Kbps modum" constitutes "access to advanced services" for the purpose

REDACTED.DOC

| 1  | of implementing FCC Criterion 1 (Bowman Direct, Exhibit RMB 3, Pg. 2).         |
|----|--|
| 2  | The FCC Criterion actually states that, "[t]he loop design incorporated into a |
| 3  | forward-looking economic cost study or model should not impede the             |
| 4  | provision of advanced services. For example, loading coils should not be       |
| 5  | used because they impede the provision of advanced services." (FCC Report      |
| 0  | and Order, May 8, 1997, Paragraph 250, Criterion 1). While the FCC does        |
| 7  | not specifically define "advanced services," its use of the words "not impede" |
| 8  | and the example of "load coils," which would actually preclude the             |
| 9  | transmission of digital signals, does provide ample guidance in this matter.   |
| 10 |  |
| 11 | My understanding of "impeding advanced services" in regards to the issue       |
| 1. | raised in Exhibit RMB 3 would be to deny modern access to rural customers,     |
| 13 | which the existing ILEC networks certainly do today. The attempt by the        |
| 14 | BCPM sponsors to declare 28.8 Kbps modem access as the standard for            |
| 15 | advanced services (as opposed to say 14.4 Kbps or 56 Kbps) is blatantly self-  |
| 16 | serving and misleading.  |
| 17 |  |
| 18 | Proponents of BCPM have noted a Bellcore Technical Memorandum TM-              |
| 19 | 25704 as support for why the Hatfield Model will not support modem speeds      |
| 20 | of 28.8 Kbps (Bowman Direct, Exhibit RMB 3, Pg. 10). This TM is not a          |
| 21 | transmission standard and was specifically developed as a worst-case           |
| 22 | scenario. Mr. John Donovan, the leader of the HAI OSP Engineering Team         |
| 23 | has reviewed this TM, calked with its author and makes the following           |
| 24 | observations, which I support:   |
|    |  |

REDACTED.DOC

A close reading of the TM indicates exactly what I have been saying regarding the inexactness of analog modern performance. Worthy of note is page 12 of that TM, which tabulates the actual experiments performed. The purpose of the tests was not to validate the transmission characteristics of either the BCPM or Hatfield Models, but to examine worst-case scenarios. In fact the worst case is so bad, that none of the loops used in experiment meet tariff requirements, since all loops exceed the 8.5 dB maximum for POTS loops. Since other empirical data is not readily available on short notice, however, we can make certain observations about the data. First of all, I personally spoke with Rick Perez, the Bellcore author. He told me that the worst-case test loops had many gauge changes and many splices. This would cause high reflection losses in each splice, and is the most likely cause of the abnormal dB losses at the standard test frequency of 1004 Hz.

1 2

3

4

5

6

7 8

9 10

11 12

13 14

15

25

Test loop number 1 was 18,000 feet with no bridge tap. It supported 16 17 24.0 kbps on a 28.8 modem, but had a horrendous loss of 14.3 dB, 5.8 18 dB above the maximum allowed by tariff. Since each 3dB attenuation 19 halves the signal strength, this means that the signal on this loop was at 20 about 1/4 or 25% of the strength it should be at 8.5 dB. The next longest 21 loop was test loop number 6 which was 17,500 feet with 1,000 feet of 22 bridge tap. Yet this loop still had 12.8 dB of loss, or about 3/8ths of the 23 signal strength the Hatfield Model would provide at 8.5 dB. Still, this 24 loop readily supported 26.4 kbps with a 28.8 kbps modem.

As one would surmise from the Bellcore Technical Memorandum, determining 26 27 predicted modem speeds is not an exact science. The HAI OSP Engineering Team has estimated that the HM 5.0a will support minimum modem speeds of 21 28 29 - 24 Kbps for any loop, and 28.8 Kbps, or better, for most loops. I believe that this level of performance more than complies with a reasonable interpretation of 30 the FCC requirement to provide access to "advanced telecommunications and 31 REDACTED DOC

information services that are reasonably comparable to those services provided in urban areas."

- 4 The conclusion of this exhibit stated that, "[b]y utilizing the DSC architecture 5 and the maximum 12 Kft copper loop, BCPM3 assures that the requirements for 6 advanced telecommunications service access for remote rural customers is 7 reasonably comparable to that enjoyed by urban customers, as mandated by the 1996 Act" (Bowman Direct, Exhibit RMB 3, Pg. 9, with italics added for 8 9 emphasis). In this testimony it has been shown that the BCPM 3.1 clearly 10 designs copper loops out to 18 Kft and even beyond. Not only is the conclusion 11 statement above rather questionable, but any undue concern raised by Exhibit 12 RMB 3 regarding modem speed is applicable to BCPM 3.1.
- 13

t

2

3

# 14 VIL SUMMARY

# 15 Q. WOULD YOU PLEASE SUMMARIZE YOUR TESTIMONY?

16 Α. I recommend that the Commission adopt the HM 5.0a as the most appropriate 17 model for determining the local loop cost of basic local exchange service in 18 Florida. In Release 3.1, the BCPM modelers have taken steps to evolve their 19 model by incorporating several of the concepts of the Hatfield Model plus some 20 additional ideas to improve the accuracy and cost efficiency of the local loop 21 model. Most of the evolutionary changes in this particular release of the BCPM have the initial conceptual appearance of being cost improvements. However, 22 23 upon investigation, I have found that in the implementation of these ideas the 24 BCPM 3.1 still falls we'l short of being the least-cost, most-efficient, forward-

# REDACTED.DOC

looking and reasonable local loop cost model based on currently available
 technology, particularly in comparison to the HAI Model Release 5.0a.

- Second, I recommend that many of the OSP input values proposed by BellSouth,
   GTE and Sprint be rejected, since these inputs contain numerous fallacies and are
   not the least-cost, most-efficient and forward-looking set of input values that are
   required in this proceeding. The HAI Model 5.0a and the input values proposed
   by AT&T and MCI for OSP are more appropriate to use in this proceeding for
   determining the cost of the local loop network in Florida in order to size the
   Universal Service Fund.
- 11

3

- 12 Q. DOES THIS CONCLUDE YOUR TESTIMONY?
- 13 A. Yes.

Docket No. 9800995-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

5.620

1

|  |  | BCPM 3.1   | BOPM 2.1  | BOPM 3.1   | BOPM 8.1   | HM 8.0+              |
|--|--|--|---|--|--|----------------------|
| INPUT VALUE DESCRIPTION  | Density Zone   | BellBouth -<br>Default   | Balldouth FL  | Eprint-FL  | GTE - FL   | Floride              |
|  |  | [1/16/96]  | (8/3/94)  | (8/2/94)   | (8/3/94)   | (e/3/94)             |
| Itrusture Cost - Aerial (Poles) - Distribu   | 00000 · 00005  | ¥ 780.58   | 4 408.44  | 4 001.38   | 0 B01.11   | 4 417.0              |
| Before Structure Shering)  | 00005 - 00100  | 4 780.58   | \$ 408.44   | 4 601,28   | 4 801,11   | \$ 417.00            |
|  | 00100 - 00200  | Y80,58   | 4 408.44  | 8 601.38   | 8 801,11   | 4 417.0              |
|  | 0/200-00650  | \$ 790,58  | 4 408,44  | 4 601.38   | 4 B01.11   | 4 417.0              |
|  | 00810 - 00850  | 4 775,20   | 408,77  | \$ 500,14  | 6 801,11<br>6 801,11   | 8 417.0<br>8 417.0   |
|  | 00850 - 02550<br>02550 - 05000   | 4 823.05<br>4 923.05   | 8 421,84<br>9 421,84  | 6 643.28<br>6 643.28   | 6 801.11   | \$ 417.0<br>\$ 417.0 |
|  | 05000 - 10000  | 4 823.05   | # 421.84  | 4 643.20   | 8 B01.11   | 4 417.0              |
|  | 10000 +  | 4 823.05   | 4 421.84  | 0 643.28   | 4 801.11   | 4 417.0              |
| Itructure Cost - Aerial - Feeder   | 00000 - 00005  | \$ 760.58  | 408.44  | 8 601.58   | \$ 801.11  | 4 417.0              |
| Before Structure Shering)  | 00005 - 00100  | \$ 760.58  | 408.44  | 8 601.38   | \$ 601.11  | 6 417.0              |
| SCELOLE JEAGESTICH, JUSIE LINE   | 00100 - 00200  | \$ 780.55  | \$ 408.44   | \$ 601.38  | \$ 801.11  | \$ 417.0             |
|  | 00200 - 00650  | \$ 780.58  | \$ 408,44   | \$ 601,38  | \$ 801.11  | 4 417.0              |
|  | 00650 - 00850  | \$ 775,20  | \$ 406.77   | \$ 598,14  | \$ 801,11  | 4 417.0              |
|  | 00850 - 02550  | \$ 823.65  | \$ 421.84   | \$ 643.28  | \$ 801,11  | \$ 417.0             |
|  | 02550 - 05000  | \$ 823.65  | 1 221.84  | \$ 843.26  | 3 801.11   | 4 417.0              |
|  | 05000 - 10000  | \$ \$23.65   | \$ 421.84   | \$ 643.28  | \$ 801.11  | 4 417.0              |
|  | 10000 +  | \$ 623.65  | \$ 421.64   | \$ 643.20<br>\$ 2.31   | \$ 501.11  | 4 417.0              |
| Invoture Cost - Buried - Distribution  | 00000 - 00005  | 0 1.47   | 6 3,19<br>6 3,27  | Carl and the second sec | 4 1.73   | \$ 1.7               |
| (Before Structure Sharing)   | 00005 - 00100<br>00100 - 00200   | 6 1.73   |   | 1 2,30   | \$ 2,48  | 4 1.7                |
|  | 00200 - 00850  | 4 4.30   |   | 4 2.52   | 0 4.30   | 4 1.0                |
|  | 00850 - 00850  | 4 6.22   |   | 0 2,61   | 8 8.22   | 4 2.1                |
| a second de la constante de la | 00850 - 02550  | 8 8.22   | 0 0,10  | 4 2.69   | 8 8.22   | 9 3.5                |
|  | 02550 - 05000  | 0 0.23   | - C   | 4 2.77   | 9 9.23   | 4 4.2                |
|  | 05000 - 10000  | 4 8.23   |   | 4 2.05   | .0 0.23  | \$ 13.0              |
|  | 10000 +  | 4 8,84   |   | 8 2,85   | A distance of the local distance of the loca | 4 45.0               |
| Structure Cost - Buried - Feeder   | 00000 - 00005  | 4 1.35   | 4 3,19  | 0 2.31   | 4 1,35   | 4 1.7                |
| (Before Structure Sharing)   | 00005 - 00100  | 4 1.79   |   | 9 2.30   | 4 1,70   | 6 1.7                |
|  | 00100 - 00200  | 4 2.99   | 4.40  | 9 2.44   | 4 2.98   | 4 1.7                |
|  | 00200 - 00850  | 6 4.18   | 6 6.69  | 4 2.82   | ¥ 4.10   | <u>\$ 1.0</u>        |
|  | 00850 - 00850  | 6 5.18   |   | 9 2.61   | 4 5,18   | e 2.1<br>e 3.6       |
|  | 00850 - 02550<br>02550 - 05000   |  | and the second se   | 8 2.60   | 4 8.22   | 6 3.6<br>8 4.2       |
|  | 05000 - 10000  | 6 0.22<br>6 0.22   | 6 8,15<br>4 8,16  |  | 0 0.22   | 6 13.0               |
|  | 10000 +  | 8 8.84   | and a second s | 8 2.85   | 6 8.84   | 8 45.0               |
| Structure Cost - Underground - Distribu  | and the second | And the second sec |   | \$ 2,02  | 4 2.70   | 4 10.2               |
| (Before Structure Sharing)   | 00005 - 00100  |  | 9 8,60  | \$ 2.07  | 4 3.04   | 4 10.2               |
|  | 00100 - 00200  |  |   | and the second sec   | 4 3,66   |                      |
|  | 00200 - 00680  |  |   |  | 4 4.47   |                      |
|  | 00850 - 00850  |  | 0.70  |  | 4 6.22   |                      |
|  | 00850 - 02550  | Carlo Constanting Constanting  |   |  | 4 8.28   | 0 10.4               |
|  | 02550 - 05000  | and the second se  | 4 10,61   | 9 2,60   | 6 8,23<br>9 8,23   | 9 21.6               |
|  | 10000 +  | 6 8.23<br>6 8.84   | 14.88   |  | 8 8.84   |                      |
| Structure Cost - Underground - Feeder  | 60000 - 6000E  | 4 2.70   | 4 8.61  | 4 2.02   | 9 2.70   |                      |
| (Before Structure Shering)   | 00005-00100  |  |   |  | 0 3.04   | 6 10.2               |
| ANTER, SCHOOL STREET   | 00100 - 00200  |  | 8 9.76  |  | 4 3.93   |                      |
|  | 00200 - 00650  | 4.53   | 10,09   |  | 4.63   | 14 11.3              |
|  | 00650 - 00850  | 4 8.27   | 4 9.62  | 4 2,33   | 0 6.27   | 4 11.8               |
|  | 00850 - 02550  | 4 8.27<br>9 8.27   | 4 9.62  | 1 8 2.41   | 9 5.27   | 6 10,4               |
|  | 02550 - 05000  | 4 8.22   | 4 10,51   | 1 2,80   | 8.22   | 0 21.0               |
|  | 05000 - 10000  | 0 0.22   | 4 16,61   |  |  |                      |
|  | 10000 +  | 8 8,84   |   |  |  |                      |
| Etructure Cost - Conduit (Before Bitrust   | 4 Inch<br>nd Hole: 3*8 or  | 8 0.83<br>8 844.00   |   | 5 644.00   |  |                      |
| Structure Cost - Manholee - Meterial<br>(Before Sharing)   | enhole: 4*8*6 /  |  |   |  | 15 0,200,17  |                      |
| Liberora prisr Pagi  | Innhole ()*12*7 /  |  |   | \$ 3,200,00  | \$ 11,288,70   |                      |
|  | Adder 6*12*7   |  | and the second se   | \$ 2,800.00  |  |                      |
| Structure Cost - Manholes - Installation   | nd Hole: 3*8 or  | \$ 400.00  | \$ 443,10   |  |  | 0 220.0              |
| (Before Bharing)   | anhole: 4*8*6 /  | \$ 1,645.00  | 18 .  | 1 1,645.00   |  | 4 2,800.0            |
|  | enhole 6*12*7 /  | \$ 2,431.00  |   | \$ 2,431,00  |  | # 5,000.0            |
|  | Adder 6*12*7   |  |   | \$ \$00.00   |  |                      |
| % Paid by Yeloo - Aarial - Distribution  | 00000 - 00005  |  |   |  |  |                      |
| (Poles)  | 00005 - 00100  |  |   |  |  |                      |
|  | 00100 - 00200  |  |   |  | 53.58%   |                      |
|  | 00200 - 00850<br>00850 - 00850   |  |   |  |  |                      |
|  | 00850 - 02550  |  |   |  |  |                      |
|  | 02550 - 05000  |  |   | 50.00%   | 63.56%   |                      |
|  | 08000 - 10000  |  |   |  | 83.58%   |                      |
|  | 10000 +  | 50.00%   |   | \$0.00%  | 63.50%   |                      |
| % Paid by Taloo - Aarial - Distribution  | 00000 - 00005  | 100.00%  | 100.001   | 100.00%  | 100.00%  |                      |
|  | 00 05 - 00100  | 100.00%  |   |  |  |                      |
| (Anchore & Guye)   |  | the second se  | 100.009   | 100.00%  | 100.00%  |                      |
| (Anchore & Guye)   | 00100 - 00200  |  |   |  |  |                      |
| (Anchora & Guya)   | 00100 - 00200<br>00200 - 00650<br>00650 - 00850  | 100,00%  | 100.009   | 100.00%  | 100.00%  |                      |

2,0301,328

#### Docket No. 900595-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zona                   | BCPM 3.1<br>BallBouth -<br>Default<br>(1/10/50) | BCPM 5.1<br>Belliserh-FL<br>(8/3/96) | 8CPM 2.1<br>8print-FL<br>(8/3/08) | 8CPM 8.1<br>GTE - FL<br>(8/3/94) | Hild S.Co<br>Florida<br>(S/3/94) |
|--|--------------------------------|---|--------------------------------------|-----------------------------------|----------------------------------|----------------------------------|
|  | 02550 - 05000                  | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
|  | 05000 - 10000                  | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
|  | 10000 +                        | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
| N Paid by Telon - Aerial - Distribution  | 00000 - 00005                  | 50.45%  | 45.70%                               | 40.03%                            | 66.11%                           | 50,009                           |
| Weighted (Poles, enchors & guys)   | 00005 - 00100<br>00100 - 00200 | 50.45%<br>50.45%                                | 45,70%                               | 40.09%                            | 55.11%                           | 25,003                           |
|  | 00200 - 00850                  | 58.45%  | 48.70%                               | 40.89%                            | 65.11%<br>65.11%                 | 25.003                           |
| and the second sec | 00850 - 00850                  | 85.88%  | 45.17%                               | 45.58%                            | \$5,11%                          | 28.009                           |
|  | 00850 - 02550                  | 60.53%  | 49,60%                               | 65.48%                            | 58.11%                           | 25,00%                           |
|  | 02550 - 05000                  | 80,53%  | 49.80%                               | \$5,48%                           | 85.11%                           | 25.00%                           |
|  | 05000 - 10000                  | 60.83%  | 49.00%                               | 55,48%                            | 65,11%                           | \$,009                           |
| V Paid by Taloo - Aarial - Feeder  | 10000 +                        | 60,53%  | 49,60%                               | 55.48%                            | 55,11%                           | 28.005                           |
| (Poles)  | 00005 - 00100                  | \$0.00%   | 39.88%                               | 30,00%                            | 63.80%                           |                                  |
| E WAT  | 00100 - 00200                  | 60,00%  | 20.88%                               | 30.00%                            | 63.68%                           |                                  |
|  | 00200 - 00650                  | 60.00%  | 39,88%                               | 30,00%                            | 63.68%                           |                                  |
|  | 00850 - 00850                  | 60.00%  | 39,68%                               | 30.00%                            | 63,50%                           |                                  |
|  | 00850 - 02550                  | 60,00%  | 30,00%                               | 20.00%                            | 63,68%                           |                                  |
|  | 02550 - 05000                  | 60.00%<br>60.00%                                | 39,88%                               | 30,00%                            | 53,58%                           |                                  |
| N Paid by Telco - Aarial - Feeder  | 10000 +                        | 80.00%  | 39.88%                               | 30.00%                            | 63.68%                           |                                  |
| (Anchors & Guys)   | 00000 - 00005                  | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
| ALAN ALAN ALAN ALAN  | 00005 - 00100                  | 100.00%   | 100.00%                              | 100,00%                           | 100.00%                          |                                  |
|  | 00100 - 00200                  | 100.00%   | 100.00%                              | 100.00%                           | 100,00%                          |                                  |
|  | 00200 - 00650                  | 100.00%   | 100,00%                              | 100.00%                           | 100,00%                          |                                  |
|  | 00650 - 00850                  | 100.00%   | 100,00%                              | 100,00%                           | 100,00%                          | _                                |
|  | 00850 - 02550<br>02550 - 05000 | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
|  | 05000 - 10000                  | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
|  | 10000 +                        | 100.00%   | 100.00%                              | 100.00%                           | 100.00%                          |                                  |
| % Paid by Telco - Aarial - Feeder  | 00000 - 00005                  | 50.45%  | 45,70%                               | 40.00%                            | 85.11%                           | 60,005                           |
| (Poles, anchors & guye)  | 00005 - 00100                  | 60.45%  | 45.70%                               | 48,89%                            | \$5.11%                          | 33.00%                           |
|  | 00100 - 00200                  | 58.45%  | 45,70%                               | 46,89%                            | 65,11%                           | 25.005                           |
|  | 00200 - 00650<br>00650 - 00850 | 80,45%<br>85,88%                                | 45,70%                               | 46,89%                            | 55,11%                           | 25.005                           |
|  | 00850 - 02550                  | 60.63%  | 49.60%                               | 65.48%                            | 55,11%                           | 25.009                           |
|  | 02550 - 05000                  | 60.53%  | 49.80 1                              | \$5,48%                           | 55,11%                           | 25.00%                           |
|  | 05000 - 10000                  | 00,53%  | 49,00%                               | \$5,48%                           | 65,11%                           | 25.009                           |
|  | 10000 +                        | 60.53%  | 48,60%                               | 65,48%                            | 65,11%                           | 25.005                           |
| % Paid by Taloo - Buried - Distribution<br>(Structure sharing % = [1] minus % pe   | 00000 - 00005                  | 100.00%   | \$6,00%<br>\$6,00%                   | 98.64%                            | 100.00%                          | 33.009                           |
| requiring a start of the - Til tisking to be   | 00100 - 00200                  | 66.90%  | 96.00%                               | 99,25%                            | 100.00%                          | 33,007                           |
|  | 00200 - 00650                  | 84.20%  | \$6.00%                              | 09.10%                            | 100.00%                          | 33.009                           |
|  | 00850 - 00850                  | 84.00%  | 96.00%                               | 60.14%                            | 100.00%                          | 33,001                           |
|  | 00850 - 02850                  | 84.00%  | \$6.00%                              | 69.10%                            | 100.00%                          | 33.009                           |
|  | 02550 - 05000<br>05000 - 10000 | 80.00%  | 96.00%<br>96.00%                     | 99.04%                            | 100.00%                          | 33,009                           |
|  | 10000 +                        | 80.00%  | 86.00%                               | 60.00%                            | 100.00%                          | 33.009                           |
| % Paid by Telco - Buried - Feeder  | 00000 - 00008                  | 100.00%   | 69,00%                               | 100.00%                           | 100.00%                          | 40.005                           |
| (Structure sharing % - [1] minus % ps  |                                | 99.45%  | 4/00.08                              | 00.E2%                            | 100.00%                          | 40,009                           |
|  | 00100 - 00200                  | \$40.00%  | \$9.00%                              | 00.02%                            | 100.00%                          | 40.001                           |
|  | 00200 - 00650                  | 94,96%  | 99,00%                               | 00.59%<br>00.57%                  | 100.00%                          | 40.001                           |
|  | 00850 - 00850<br>00850 - 02550 | 01.50%  | 99.00%                               | 99.57%                            | 100.00%                          | 40,001                           |
| a second and the second se   | 02550 - 05000                  | 65.00%  | 69.00%                               | 80.52%                            | 100.00%                          | 40.001                           |
|  | 05000 - 10000                  | 65.00%  | 89,00%                               | 89.50%                            | 100.00%                          | 40,009                           |
|  | 10000 +                        | 85.00%  | 89,00%                               | 99.50%                            | 100.00%                          | 40.003                           |
| % Paid by Telco - Underground - Distrib  |                                | 100.00%   | 99.00%                               | 100.00%                           | \$7,18%                          | 100,001                          |
| Estructure sharing % = [1] minus % pa  |                                | 85.00%  | 19.00%                               | 85.00%                            | 67.18%                           | 50,001                           |
|  | 00100 - 00200<br>00200 - 00050 | 80.00%<br>80.00%                                | 89.00%<br>99.00%                     | \$0.00%<br>\$0.00%                | 97,18%                           | 50,001                           |
|  | 00850 - 00850                  | 80.00%  | 80.00%                               | 90.00%                            | 07.18%                           | 40.001                           |
|  | 00850 - 02550                  | 80.00%  | \$9.00%                              | 60.00%                            | 97.18%                           | 33,001                           |
|  | 02550 - 05000                  | #00.06  | \$9.00%                              | 80.00%                            | 97,18%                           | 33,009                           |
|  | 06000 - 10000                  | 80.00%  | 99,00%                               | \$0.00%                           | 97.18%                           | 33.001                           |
| % Peid by Teloo - Underground - Feeder   | 10000 +                        | 80.00%<br>100.00%                               | 69.00%                               | 100.00%                           | 07.10%<br>07.16%                 | 33,001                           |
| % Peid by Teloo - Underground - Feeder<br>(Structure sharing % ~ [1] minus % pa  |                                | 87,50%  | 66.00%                               | 07,50%                            | 07.18%                           | \$0,001                          |
| ALL DESCRIPTION OF TAXABLE PARTY   | 00100 - 00200                  | 85.00%  | 99,00%                               | 95.00 m                           | 97.16%                           | 40.001                           |
|  | 00200 - 00650                  | 92.50%  | \$9.00%                              | \$4.99%                           | 97,18%                           | 33,009                           |
|  | 00650 - 00850                  | 90.00%  | 00,00%                               | 95.01%                            | 97,18%                           | 33,001                           |
|  | 00850 - 02550                  | \$6.00%   | 89.00%                               | 64.09%                            | 97.18%<br>97.18%                 | 33,001                           |
|  | 02580 - 05000                  | 85.00%  | 99.00%<br>99.00%                     | 85.00%<br>85.00%                  | 87.18%                           | 33,001                           |
|  | 10000 +                        | 85.00%  | 89.70%                               | 85.00%                            | 87,18%                           | 33,009                           |
| % Paid by Talco - Manholas   | rid Hole: 3*5 or               | 75.00%  | 60.00%                               | 78.00%                            | 97,18%                           | N//                              |
| h  | fanhole: 4*8*0 /               | 90.00%  | \$9.00%                              | 80.00%                            | 97.18%                           | N//                              |
| M  | anhole 0*12*7/                 | 80,00%  | 89,00%                               | 80.00%                            | 07,18%                           | N//                              |
|  | Adder 6*12*7                   | #00.06  | 89.00%                               | 80.00%                            | 97.10%                           | N//                              |

4,0001\_31.8

### Docket No. 860696-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

|  | Density Zone   | BCPM 3.1<br>BellBouth -<br>Defeult<br>(1/16/98)  | BOPM 3.1<br>BellSouth-FL<br>[8/3/94]   | BOPM 3.1<br>Burles-FL<br>(8/3/94)  | BCPM 3.1<br>GTE - FL<br>(8/5/96)  | HM 8.0.e<br>Flurida<br>(9/3/99)  |
|--|--|--|--|--|---|--|
| Post Sharing Cost - Aarial - Distributio   | 00000 - 00005  | of the local division of the local divisiono | \$ 172.60  | \$ 217.08  | \$ 435.91   | 1 208.50   |
| Poles, Anchers & guys)   | 00005 - 00100  |  | \$ 172.96  | \$ 217.08  |   | 8 137.61   |
| provide, Perspectra & gorphi   | 00100 - 00200  |  | \$ 172.06  | \$ 217.08  | 1 435.91  |  |
|  |  |  |  |  |   |  |
|  | 00200 - 00850  |  | \$ 172.96  |  |   |  |
|  | 00650 - 00850  |  | \$ 171.28  | \$ 211.84  |   | 104.25   |
|  | 00850 - 02550  | \$ 460.28  | \$ 188.35  | \$ 258.98  | \$ 435.91   | 0 104.25   |
|  | 02550 - 05000  | \$ 460.28  | \$ 186.35  | \$ 258.98  |   | 9 104.25   |
| the second se  | 05000 - 10000  | \$ 400.26  | \$ 188.55  | \$ 258.98  | \$ 435.91   | Contraction of the Area of the |
|  | and all all all all all a formers that the ball of a   |  |  |  |   | 4 104.26   |
|  | 10000 +  | 460.28   |  |  |   | 104.28   |
| Post Sharing Cost - Asrial - Feeder  | 00000 - 000005   | 5 417.21   | 3 172.00   | \$ 217.08  | \$ 435.01   | \$ 208.60  |
| (Poles, Anchors & guys)  | 00005-00100  | \$ 417.21  | \$ 172.88  | \$ 217.08  | \$ 435.91   | 0 137.61   |
| P. WITH PRINCIPAL MARTIN   | 00100 - 00200  |  |  |  |   |  |
|  | and the state of the second state of the secon | وسرادتها برود بدوه مستعد والما   |  |  |   | \$ 104.25  |
|  | 00200 - 00850  |  |  | \$ 217.08  |   | 4 104,25   |
|  | 00850 - 00850  | \$ 411.83  | \$ 171.28  | \$ 211.84  | \$ 435.91   | 0 104.25   |
|  | 00850 - 02560  | \$ 460.28  | \$ 180.35  | \$ 258.98  | \$ 435.91   | 4 104,25   |
|  | 02550 - 05000  |  | \$ 186.35  | \$ 258.90  | \$ 45.01  |  |
|  |  | And a summer of the second sec | and the second sec   |  |   |  |
|  | 05000 - 10000  |  |  |  |   |  |
|  | 10000 +  | \$ 400.28  | \$ 188.55  | \$ 258.98  | \$ 435.91   | \$ 104.25  |
| Post Sharing Cost - Buried - Distribution  | 00000 - 00005  | 4 1.47   | \$ 3,00  | 4 2.31   | 1.47  | 0.58   |
| and a state of the second  | 00006 - 00100  | THE REPORT OF THE PARTY OF THE  |  |  |   |  |
|  |  |  |  | 4 2.33   | 4 1.73  | 0.58   |
|  | 00100 - 00200  |  | 4 2,83   | 4 2.38   | 0 2,48  | 0.58   |
|  | 00200 - 00650  | 4 3.54   | 4 5,60   | 4 2.45   | 4 4,30  | \$ 0,64  |
|  | 00850 - 00850  | 4 4.23   |  | 4 2.52   | 4 6.22  |  |
|  | 00850 - 02550  | 4.23   |  | 4 2.60   | 4 4 4 4 4   | 0.72   |
|  |  |  |  |  | 4 6.22  |  |
|  | 02650 - 05000  | 6.58   | 4 7.84   | 4 · 2.67   |   | 4 1,41   |
|  | 05000 - 10000  | 4 0,58   | \$ 7.84  | \$ 2.74  | 6 0.23  | 4.28   |
|  | 10000 +  | \$ 7.07  |  | \$ 2.74  | 4 8.84  | 0 14.05  |
| Post Sharing Cost - Buried - Feeder  | 00000 - 00005  |  |  | Management of the local date   | and the second se | and the second se  |
| Lost oversig Cost - annieg - Leeder  |  |  |  | 9 2.31   | 4 1.35  | 0.71   |
|  | 00005 - 00100  | 1.77   | 4 3.24   | 4 2.35   | \$ 1,70   | 0.71   |
|  | 00100 - 00200  | 9 2.85   | 4 4,30   | 6 2.41   | 0 2.00  | 0.71   |
|  | 00200 - 00650  | 9 3.80   | 6 6.83   | 8 2.49   |   |  |
|  | CONTRACTOR CONTRACTOR OF A DATA  |  |  | the first sector of the sector | 4,18  | 4 0,77   |
|  | 00650 - 00850  | 10.000   | 4 6,87   | 1 2,56   | 4 5,10  | \$ 0,87  |
|  | 00850 - 02550  | 4 4.68   | 4 6.87   | 4 2.64   | 4 5,18  | 1.42   |
|  | 02580 - 05000  | 0.08   | 4 8.07   | 4 2.72   | 4 8.22  | 0 1,71   |
|  | 05000 - 10000  | 4 0.90   | and examine and the date   |  |   |  |
|  |  |  | Contraction of the local division of the loc | 4 2,80   |   | 4 5,20   |
| and the party of the game in the spiritual second se  | 10000 +  | 4 7.51   | \$ 7,69  | \$ 2,80  |   | 1 18.00  |
| Post Sharing Cost - Underground - Dist   | 00000 - 00005  | \$ 2.70  | 4 8,42   | \$ 2.02  | 4 2.03  | 0 10.29  |
|  | 00005 - 00100  | 1 2.88   | 4 8.51   | \$ 1,97  | 4 2.05  | 9 5,14   |
|  | 00100 - 00200  |  |  | \$ 1.94  | \$ 3.65   |  |
|  |  |  |  |  |   | 6 5,14   |
|  | 00200 - 00650  | 4 3.57   |  | \$ 2.02  | 4 4,34  | \$ 5,65  |
|  | 00650 - 00850  |  | 6 9,60   | 1 2.10   | 4 5,14  | 4 4.75   |
|  | 00850 - 02550  | 6 4,23   | \$ 9,60  | 6 2.17   | 5 5.14  | 8 5.41   |
|  | 02550 - 05000  |  | \$ 16.25   | \$ 2.25  | 6 7.00  | 0 7.13   |
| the second se  | 05000 - 10000  |  |  |  |   |  |
|  |  | the first second se   | the local data was a set of the local data of th | 1 2.33   | 4 7.99  | 0 10.53  |
| and the second sec   | 10000 +  | 1 7,07   |  | 9 2.33   | 0.50  | 4 24.75  |
| Poet Sharing Coet - Underground - Feet   | 00000 - 00005  | \$ 2.78  | 4 8.42   | 4 2.02   | 4 2.08  | \$ 5,14  |
|  | 00005 - 00100  |  | 4 8.51   | \$ 2.02  | 4 2.05  | \$ 6,14  |
|  | 00100 - 00200  |  |  |  |   |  |
|  |  | the second se  | 9.08   | 4 2.05   | 4 3,82  | 4 4,11   |
|  | 00200 - 00850  |  |  | 1 2,13   | 4.40  | 4 3.78   |
|  | 00650 - 00850  | \$ 4,74  | 4 0.52   | 6 2.21   | 8 6.12  | \$ 3.92  |
|  | 00850 - 02550  |  | 4 9,82   | 9 2.29   | 4 6,12  | 4 5.41   |
|  | 02550 . 05000  |  | 8 10.34  | 4 4 4 7  |   |  |
|  |  |  |  | 9 2.37   | 9 7,98  | 4 7,13   |
|  | 05000 - 10000  |  | 4 10,34  | 9 2.45   | 4 7.00  |  |
| and the second se  | 10000 +  | 6 7.51   | 6 14.74  | \$ 2.45  |   |  |
| Poet Sharing Ceet - Conduit  | 4 Inch   | \$ 0.83  | \$ 2.22  | ¥ 0.73   |   |  |
| Post Sharing Cost - Manholas - Mat. &  | Ind Hole: 3*E or   | \$ 1,008.00  |  | \$ 1,008.00  |   |  |
| A REAL PROPERTY AND A REAL | Marchola: 4*8*0 /  | \$ 3,404.53  | \$ 6,404.01  | 1 10120  | a phil bit  |  |
|  |  |  |  | \$ 3,404.93  | \$ 9,038 43   | \$ 2,670.00  |
|  | fambole 6*12*7/  | 4,512.00   |  | \$ 4,512.00  |   | \$ 2,422.20  |
|  | Adder 6*12*7   |  | \$ .   | \$ 2,640.00  | \$ 3,208.94   | N/A  |
| ole Specing  | 00000 - 00005  |  | 250<br>250   | 250  | 175   | 250  |
|  | 00005 - 00100  | 250  | KEN.   | 250  | 175   |  |
|  |  | 630  | 600  | 250  |   | 250  |
|  | 00100 - 00200  | 250  | 250  | 250  | 175   | 200  |
|  | 00200 - 00850  | 250  | 250  | 250  | 175   | 200  |
|  | 00850 - 00850  | 150  | 150  | 150  | 175   | 17   |
|  | 00850 - 02850  | 150  | 150  | 150  |   |  |
|  |  |  |  |  | 175   | 170  |
|  | 02550 - 05000  | 150  | 150  | 150  | 175   | 160  |
|  | 05000 - 10000  | 150  | 150  | 150  | 175   | 160  |
|  | 10000 +  | 150  | 150  | 150  | 175   |  |
|  | 10000 4  | 1.30   | 190  | 130  | 1/0   | 150  |
|  |  |  | 8 53.25  | 1 1000   | \$ 70.43  |  |
| Cabla - Conner - Anisi - 54 Auro-  | 4956   | 8 24 94  |  |  | P 70.431  | N/A  |
| Ceble - Copper - Aerial - 24 Geupe   | 4200   | \$ 52.79   | \$ 23,03   | \$ 45.14   |   |  |
| Ceble - Copper - Aarial - 24 Gaupa<br>(Material Cost)  | 3000   | \$ 47,89   | \$ 15.74   | \$ 56.61   | \$ 60.63  |  |
|  |  |  | \$ 15.74   |  | \$ 60.63  | N/A  |
|  | 3000   | \$ 47,89<br>\$ 46,45   | \$ 15.74<br>\$ 16.45   | 5 56.81<br>5 32.03   | \$ 60.63<br>\$ 50.82  | N/A<br>N/A   |
|  | 3000<br>3000<br>2400   | 47,89<br>46,45<br>35,99  | \$ 15.74<br>\$ 16.45<br>\$ 13.16   | \$ 56.81<br>\$ 32.03<br>\$ 22.82   | \$ 60.63<br>\$ 50.82<br>\$ 41.02  | N/A<br>N/A   |
|  | 3000<br>3000<br>2400<br>2100   | 47,89<br>46,45<br>35,99<br>26,30   | \$ 15.74<br>\$ 16.45<br>\$ 13.16<br>\$ 11.51   | 546.51<br>52.03<br>522.82<br>522.82<br>520.47  | \$ 60.63<br>\$ 50.82<br>\$ 41.02<br>\$ 56.23  | N/A<br>N/A<br>N/A<br>N/A   |
|  | 3000<br>3000<br>2400<br>2100<br>1800   | 47,89<br>46,45<br>535,99<br>526,30<br>526,30   | \$ 15.74<br>\$ 16.45<br>\$ 13.16   | 5 36.81<br>5 32.03<br>5 22.82<br>5 20.47<br>5 17.68  | \$ 60.63<br>\$ 50.82<br>\$ 41.02<br>\$ 58.23<br>\$ 51.05  | N/A<br>N/A   |
|  | 3000<br>3000<br>2400<br>2100<br>1800   | 47,89<br>46,45<br>35,99<br>26,30   | \$ 15.74<br>\$ 16.45<br>\$ 13.16<br>\$ 11.51   | 546.51<br>52.03<br>522.82<br>522.82<br>520.47  | \$ 60.63<br>\$ 50.82<br>\$ 41.02<br>\$ 58.23<br>\$ 51.05  | N/A<br>N/A<br>N/A<br>N/A   |
|  | 3000<br>3000<br>2400<br>2100<br>1800<br>1200   | 47,89<br>46,45<br>35,99<br>26,50<br>26,54<br>16,83   | \$ 18,74<br>\$ 16,45<br>\$ 13,16<br>\$ 11,51<br>\$ 9,87<br>\$ 6,46   | \$ 36.81<br>\$ 32.03<br>\$ 22.82<br>\$ 20.47<br>\$ 17.68<br>\$ 10.89   | \$ 60.63<br>\$ 50.82<br>\$ 41.02<br>\$ 58.23<br>\$ 51.05  | N/A<br>N/A<br>N/A<br>N/A<br>N/A  |
|  | 3000<br>3000<br>2400<br>2100<br>1800   | 47,89<br>46,45<br>535,99<br>526,30<br>526,30   | \$ 18,74<br>\$ 16,45<br>\$ 13,16<br>\$ 11,51<br>\$ 9,87  | 5 36.81<br>5 32.03<br>5 22.82<br>5 20.47<br>5 17.68  | \$ 60.63<br>\$ 50.82<br>\$ 41.02<br>\$ 58.23<br>\$ 51.08<br>\$ 20.47  | N/A<br>N/A<br>N/A<br>N/A   |

348101\_32.6

#### Docket No. 980696-TP J. W. Wells Exhibit No. \_\_\_\_ (MW-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Deneity Zuna | BCPM 3.1<br>BaltSouth -<br>Defeult<br>[1/16/95] | BCPM 3.1<br>Beldauth-FL<br>(s/3/98) | BCPM 3.1<br>Sprint-FL<br>(8/3/98) | BCPM 2.1<br>GTE - FL<br>(8/3/98) | Hiti 8.0a<br>Flarida<br>(8/3/98) |
|--|--------------|---|-------------------------------------|-----------------------------------|----------------------------------|----------------------------------|
|  | 300          | \$ 5.85   | \$ 1.77                             | \$ 4.60                           | \$ 5.93                          | N/                               |
|  | 200          | \$ 4.55   | \$ 1.37                             | \$ 4,23                           | \$ 4.51                          | 4 4.2                            |
|  | 100          | \$ 3.37   | \$ 0.75                             | \$ 2.97                           | \$ 2.66                          | 8 2.6                            |
|  | 60           | \$ 2.77   | \$ 0.47                             | \$ 2.51                           | \$ 1.85                          | 4 1,6                            |
|  | 25           | \$ 2.62   | \$ 0.30                             | \$ 2.28                           | \$ 1.39                          | 9 1.1                            |
|  | 18           | \$ 2.50   | \$ 0.50                             | \$ 1.90                           | \$ 1.38                          | 4 0.7                            |
|  | 12           | \$ 2.54   | \$ 0.30                             |                                   |                                  | \$ 0.6                           |
| Cable - Copper - Asriel - 24 Gauge   | 4200         | 18 .  | \$ 22.64                            | 5 .                               | 1 .                              | N/                               |
| (Supply Coet)  | 3600         | 1 .   | \$ 19.40                            | \$ .                              | 1 .                              | N/                               |
|  | 3000         | \$ .  | \$ 10.17                            | \$ .                              | 1 .                              | 94/                              |
|  | 2400         | 1 .   | \$ 12.94                            | \$ .                              | \$ .                             | N/                               |
|  | 2100         | 1 .   | \$ 11.32<br>\$ 9.70                 | \$ .                              | \$ .                             | N/                               |
|  | 1800         | 1 .   | \$ 9.70                             | \$ .                              | \$ .                             | N/                               |
|  | 1200         | \$ -  | \$ 6,35                             | \$ .                              | \$ .                             | NU                               |
|  | 800          | 1 .   | \$ 4.87                             | \$ .                              | 1                                | N/                               |
|  | 600          | 5 .   | \$ 3.33                             | \$ .                              | \$ .                             | N/                               |
|  | 400          | 5 .   | \$ 2.26                             | 5 .                               | 1 .                              | N/                               |
|  | 300          | 1 .   | \$ 1.74                             | 5 .                               | 1 .                              | N/                               |
|  | 200          | 5 -   | \$ 1.35                             | 1 .                               | 5 .                              | N/                               |
|  | 100          | 1 .   | \$ 0.74                             | 1 . 1                             | \$ .                             | N/                               |
|  | 60           | 1 .   | \$ 0.48                             | 1 .                               | 1                                | N/                               |
|  | 25           | 15 .  | \$ 0.30                             | 1                                 | 1                                | N/                               |
|  | 18           | 1 .   | 1 0.30                              | 1                                 | 1                                | N/                               |
|  | 12           | 1 .   | \$ 0.30                             |                                   | 1 .                              | N/                               |
| able - Copper - Aerial - 24 Gauge  | 4200         | 1   | 1 138                               | 1                                 | 1 .                              |                                  |
| (Tax)  | 3800         |   | \$ 1.18                             | 1                                 | 1                                |                                  |
|  | 2000         | 1 .   | 8 0.99                              |                                   |                                  | N                                |
|  | 2400         | 1   | \$ 0.79                             | 1 .                               | <u>.</u>                         | N/                               |
|  | 2100         | 1   | \$ 0.69                             | 1 .                               | 1 .                              | N                                |
|  | 1800         | 1   | \$ 0.59                             | 1 .                               | 1                                |                                  |
|  |              |   | \$ 0.59                             | 2 .                               |                                  | N/                               |
|  | 1200         | 1   |                                     |                                   | <u> </u>                         | N                                |
|  | 800          | · · · ·   | 8 0.50                              |                                   | <u>.</u>                         | N                                |
|  | 600          | · ·   |                                     |                                   |                                  | N/                               |
|  | 400          | 1 .   | \$ 0.14                             | 3 .                               | 1 .                              | N/                               |
| and the second sec | 300          | 1   | \$ 0.11                             | ş .                               | \$ .                             | N/                               |
|  | 200          |   | \$ 0.08                             | 1                                 | \$ .                             | M/                               |
|  | 100          | 3 .   | \$ 0.05                             |                                   | \$ .                             | N/                               |
|  | 60           | \$ ·  | \$ 0.03                             | \$ .                              | \$ .                             | N/                               |
|  | 25           | 1 .   | \$ 0.02                             | \$ .                              | \$ .                             |                                  |
|  | 18           | \$ ·  | \$ 0.02                             |                                   | \$ .                             | N/                               |
|  | 12           | 1 .   | \$ 0.02                             |                                   | \$ .                             | P6/                              |
| ehile - Copper - Aeriel - 24 Gauge   | 4200         | 1 .   | \$ 57.20                            | 1 .                               | \$ .                             | N/                               |
| (Plesing)  | 3600         | 1 .   | \$ 49.10                            | 1 .                               | \$ .                             | N/                               |
|  | 3000         |   | \$ 40.91                            | 1 .                               | \$                               | N/                               |
|  | 2400         | 1 .   | \$ 32.73                            | 1 .                               | \$ .                             | N/                               |
|  | 2100         | 1 .   | \$ 20.64                            | 4 -                               | 5 .                              | N/                               |
|  | 1800         | 1 .   | \$ 24.55                            | 1 .                               | \$ .                             | N/                               |
|  | 1,200        | 1 .   | \$ 16.07                            | 5 .                               | \$ .                             | N/                               |
|  | 900          | \$ .  | \$ 12.33                            | \$ .                              | \$ .                             | P4/                              |
|  | 600          | 1 .   | \$ 8.43                             | \$ .                              | \$ .                             | N/                               |
|  | 400          | 1 .   | \$ 5,72                             | \$ .                              | \$ .                             | N/                               |
| the second se  | 300          | 1 .   | \$ 4.59                             | \$ -                              | \$ .                             | 14/                              |
|  | 200          | \$ .  | \$ 3.41                             | \$ .                              | \$ .                             | P4/                              |
|  | 100          | 1 .   | \$ 1.67                             | 1 .                               | \$ .                             | N/                               |
|  | 60           | 1 .   | \$ 1.17                             | 5                                 | 1 .                              | N/                               |
|  | 25           | 4 -   | \$ 0.75                             | \$ .                              | \$ .                             | N/                               |
|  | 1.6          | 1 .   | \$ 0.75                             | \$ .                              | \$ .                             | N/                               |
|  | 12           | 4 .   | \$ 0.75                             | \$ .                              | \$ .                             | N/                               |
| sble - Copper - Aerial - 24 Gauge  | 4200         | 1 .   | \$ 10.47                            |                                   | 5 .                              | H.                               |
| Tipling!   | 3600         | 8 .   | \$ 8.97                             |                                   | \$ .                             | N/                               |
|  | 3000         | \$ .  | \$ 7,48                             | 1 .                               | \$ .                             | N/                               |
|  | 2400         | \$  | \$ 5.98                             |                                   | \$ .                             | N/                               |
|  | 2100         | \$ .  | \$ 5.23                             |                                   |                                  | NL/                              |
|  | 1800         | \$ .  | \$ 4.40                             |                                   | 3 .                              | N/                               |
|  | 1,200        | 3 .   | 5 2.94                              | 1 .                               | 5 .                              | N/                               |
|  | 800          | \$ .  | \$ 2.25                             |                                   |                                  | N//                              |
|  | 600          | \$ .  | 2.28                                | \$ .                              | 1 .                              | N/                               |
|  | 400          | \$ .  | \$ 1.05                             | 5 .                               | 5 .                              | N/                               |
|  | 200          | \$ .  | \$ 0.80                             |                                   | \$ .                             |                                  |
|  | 200          | 5 .   | \$ 0.62                             | 5                                 | 1                                | N/I                              |
|  | 100          | 1 .   | \$ 0.34                             | 5 .                               | 5 .                              | NU                               |
|  | 60           | 8 .   | \$ 0.21                             |                                   |                                  |                                  |
|  | 26           | 1   | \$ 0.14                             |                                   |                                  | N//                              |
|  | 10           | 1   | 0.14                                |                                   |                                  |                                  |
|  | 12           |   | \$ 0.14                             |                                   |                                  |                                  |
| dile - Copper - Aprial - 24 Gauge  | 12 4200      | 1   | 8 9.15                              |                                   |                                  |                                  |
| Engineering  | 3600         | 1   | 7.64                                |                                   |                                  | N//                              |
|  | 3000         | 1   | 0.54                                |                                   |                                  | N//                              |
|  |              |   |                                     |                                   |                                  |                                  |

448101,328

Page 4 of 22

#### Docket No. 6800806-TP J. W. Wells Exhibit: No. \_\_\_\_ (JWW-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION   | Density Zana | BCPM 3.1<br>BallSouth -<br>Default<br>(1/16/98) | BCPM 3.Y<br>Beldouth-FL<br>(8/3/96) | BCPM 3.1<br>Sprint FL<br>[8/3/99] | BCPM 3.1<br>GTE - FL<br>(8/3/96) | HM 8.0+<br>Florida<br>(8/3/98) |
|---|--------------|---|-------------------------------------|-----------------------------------|----------------------------------|--------------------------------|
|   | 2100         | \$  | \$ 4.57                             | \$ -                              | 1 .                              | NU                             |
|   | 1800         | 3 .   | \$ 3.92                             | 1 .                               | \$ -                             | 84/4                           |
|   | 1200         | 15 -  | \$ 2.57                             | \$ . ]                            | \$ .                             | P6//                           |
|   | 900          | 5 .   | \$ 1.97                             | \$ .                              | 1 .                              | P6//                           |
|   | 600          | \$ .  | \$ 1.35                             | \$ .                              | \$ .                             | N//                            |
|   | 400          | 1 .   | \$ 0.91                             | \$ .                              | 1 .                              | N/r                            |
|   | 300          | 15 .  | \$ 0.70                             | 1 .                               | 1 .                              | N//                            |
|   | 200          | 1 .   | \$ 0.54                             | 1 .                               | 5 .                              | N//                            |
|   | 100          | 1 .   | \$ 0.50                             | 1 .                               | 5 .                              | N//                            |
|   | 60           | 5 .   | 3 0.19                              |                                   | 1                                | N/                             |
|   | 25           | 15 .  | \$ 0.12                             | \$ .                              | 1 .                              | N/-                            |
|   | 18           | 5 -   | \$ 0.12                             | 1 .                               | 1 .                              | N/                             |
|   | 12           | 1 .   | \$ 0.12                             |                                   | 1 .                              | N/                             |
| 11 A  | 4200         | \$ 52.79  | 1 123.05                            | \$ 45.14                          | \$ 70.43                         | \$ 29.0                        |
| able - Copper - Aarial - 24 Gauge   |              | \$ 47.89  | \$ 106.24                           |                                   | \$ 60.63                         |                                |
| TOTAL   | 3600         | \$ 46.45  | \$ 68.53                            | \$ 32.03                          | \$ 50.82                         |                                |
| -   | 3000         |   |                                     | 1 22.82                           | \$ 41.02                         |                                |
|   | 2400         | \$ 35.99  | \$ 70.83                            |                                   |                                  | \$ 20.0                        |
|   | 2100         | \$ 28.50  | \$ 61.97                            |                                   | 1 38.25                          | 18.0                           |
|   | 1800         | \$ 26.54  | \$ 53.12                            |                                   | \$ 31.05                         | 10,0                           |
|   | 1200         | \$ 16.83  | \$ 34.76                            | 10.60                             | \$ 20.47                         | 12.0                           |
|   | 800          | \$ 12.93  | \$ 26.67                            | \$ 0.79                           | \$ 15.77                         | 10.0                           |
|   | 600          | \$ 68.8   | \$ 18,23                            | \$ 7.63                           | \$ 10.93                         | \$ 7.7                         |
|   | 400          | \$ 0.82   | \$ 12.38                            |                                   | \$ 7.08                          | 0.0                            |
|   | 300          | \$ 5.85   | \$ 9.51                             | \$ 4.80                           | \$ 5.93                          | \$ 5.1                         |
|   | 200          | \$ 4.55   | \$ 7.37                             | \$ 4.23                           | \$ 4.31                          | 4. 4.2                         |
|   | 100          | \$ 3.37   | \$ 4.05                             | \$ 2.97                           | \$ 2.66                          | 4 2.6                          |
|   | 50           | \$ 2.77   | \$ 2.53                             | \$ 2.51                           | \$ 1.85                          | 4 1.0                          |
|   | 28           | \$ 2.62   | \$ 1.63                             |                                   | \$ 1,30                          | 4 1.1                          |
|   | 18           | 8 2.50  | \$ 1.63                             | \$ 1.90                           | 8 1.58                           | 4 0,7                          |
|   | 12           | \$ 2.54   | \$ 1.63                             | \$ 1.64                           | \$ 1.35                          |                                |
| sbis - Copper - Aarial - 26 Geuge   | 4200         | \$ 37.18  | \$ 15.82                            |                                   | 3 58.04                          | N                              |
| Material)   | 3800         | \$ 34.01  | \$ 13.56                            | \$ 36.61                          | \$ 48.27                         | N/                             |
| and a set   | 3000         |   | \$ 11.30                            |                                   | \$ 40,49                         | N/                             |
| and the second se | 2400         | \$ 33.36  | 8 8.60                              | 1 18.54                           | \$ 32.71                         | N/                             |
|   | 2100         | \$ 20.88  | 1 7.53                              |                                   | \$ 30.48                         | N                              |
|   |              | \$ 19.28  | 1 6.93                              | \$ 14.47                          | \$ 24.60                         |                                |
|   | 1800         | \$ 12.78  | \$ 4.68                             | \$ 8.75                           | \$ 16.32                         | N/                             |
|   | 1200         |   | \$ 2.61                             | \$ 8.18                           | 1 12.49                          | N/                             |
|   | 900          | \$ 0.66   | \$ 2.55                             | \$ 0.55                           | \$ 0.67                          | <u>N/</u>                      |
|   | 600          | \$ 721  |                                     | \$ 5.07                           | \$ 5.05                          | N/                             |
|   | 400          | \$ 5.58   | \$ 1.77                             |                                   |                                  | N                              |
|   | 300          | \$ 4.88   | \$ 1.50                             | \$ 4.27                           | \$ 4.78                          | N/                             |
|   | 200          | \$ 3.84   | \$ 0.99                             | \$ 3,87                           | \$ 3.45                          | N/                             |
|   | 100          | \$ 2.99   | \$ 0.58                             | \$ 2.79                           | \$ 2.24                          | N/                             |
|   | 60           | \$ 2.50   | \$ 0.38                             | \$ 2.42                           | \$ 1.62                          | N                              |
|   | 25           | \$ 2.50   | \$ 0.27                             | \$ 2.23                           | \$ 1.29                          | N/                             |
|   | .10          | \$ 2.50   | \$ 0.27                             | \$ 1.88                           | \$ 1.29                          | N/                             |
|   | 12           | \$ 2.50   | \$ 0.27                             | \$ 1.82                           | \$ 1.29                          | PL/                            |
| able - Copper - Aariel - 28 Gauge   | 4200         | 1 .   | 3 19.72                             | \$ .                              | \$ .                             | N/                             |
| (Supply Cost)   | 3000         | \$ .  | \$ 16.91                            | \$ .                              | \$ ·                             | N/                             |
|   | 3000         | 1 .   | \$ 14.09                            | 1 .                               | \$                               | N/                             |
|   | 2400         | 1 .   | \$ 10.72                            | 1 .                               | \$                               | N/                             |
|   | 2100         | \$ .  | \$ 9,58                             | 8 .                               | 1 -                              | N/                             |
|   | 1800         | \$ .  | \$ 0.64                             | \$ .                              | \$ .                             | N,                             |
|   | 1200         | \$ .  | \$ 5.84                             | 1 .                               | 8 .                              | N/                             |
|   | 800          | \$ .  | \$ 4.50                             | 1 .                               | \$ -                             | N/                             |
|   | 600          | 1 .   | \$ 5,22                             | \$ .                              | \$ .                             | N/                             |
|   | 400          | 1 .   | \$ 2,20<br>\$ 1,73                  | \$ ·                              | \$ .                             | H/                             |
|   | 300          | 1   | \$ 1.73                             | 1 .                               | 1 .                              | N/                             |
|   | 200          | 1 .   | \$ 1.24                             |                                   | \$ .                             | N/                             |
|   | 100          | 1 .   | \$ 0.72                             | 1 .                               | 5 .                              | Pul.                           |
|   |              | 18 .  | \$ 0.47                             | 1 .                               | 1                                | 84/                            |
|   | 80<br>25     | 18 .  | \$ 0.34                             | 1 .                               | 1 .                              | N/                             |
|   | 10           | 1.  | \$ 0.34                             |                                   | 1 .                              | N/                             |
|   | 12           | 1   | \$ 0.34                             |                                   | 3 .                              | N/                             |
| able - Copper - Aarial - 26 Gauge   | 4200         | 1   | \$ 0.95                             |                                   | 1                                | N/                             |
| (Tex)   | 3600         | 1   | 1 0.81                              |                                   |                                  | N/                             |
|   | 3000         | 1   | 1 0.68                              |                                   | 1                                | N                              |
|   | 2400         | 1 .   | 1 0.52                              |                                   | 1                                | N                              |
|   | 2100         | 1   | \$ 0.45                             | 1                                 |                                  | N/                             |
| the second se   | 1800         | 1   | \$ 0.42                             |                                   | 1                                | N/                             |
|   | 1200         |   | \$ 0.28                             |                                   |                                  | N/                             |
|   |              | 1   | \$ 0.22                             |                                   |                                  |                                |
|   | 900          | 1   | \$ 0.15                             |                                   | 1                                | N/                             |
|   | 600          | 1   |                                     |                                   | 1                                | N/                             |
|   | 400          |   | 5 0.11                              |                                   | 1                                | N/                             |
|   | 200          | 18 .  | 1 0.08                              |                                   |                                  | N/                             |
|   | 200          | 1 .   | \$ 0.08<br>\$ 0.03                  |                                   | · · ·                            | N/                             |
|   |              |   |                                     | 5 *                               |                                  | N/                             |
|   | 10           | 1   | \$ 0.02                             |                                   |                                  | N/                             |

346501\_318

#### Docket No. 980690-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zone | BCPM 3.1<br>BallSouth -<br>Default<br>(1/16/95) | BCPM 3.1<br>BellBouth-FL<br>[8/3/94] | 80PM 3.1<br>Sprint-FL<br>[1/3/98] | 8CPM 3.1<br>OTE - FL<br>(6/2/98) | HM 8.0+<br>Florida<br>(8/3/95)   |
|--|--------------|---|--------------------------------------|-----------------------------------|----------------------------------|--|
|  | 10           | \$ .  | \$ 0.02                              |                                   | 1 .                              | N  |
|  | 12           | \$ .  | \$ 0.02                              | \$ .                              | 1 .                              | N  |
| Cable - Copper - Aarial - 26 Gauge   | 4,200        |   | \$ 47.75                             | s                                 |                                  | N. N.  |
| (Pleoing)  | 3600         | \$ .  | \$ 40,03                             | \$                                |                                  | N  |
|  | 3000         | 15 .  | \$ 34.10                             | · ·                               | · ·                              | N  |
|  | 2400         | 13 -  | \$ 25.96                             |                                   | 1 .                              | N  |
|  | 2100         | 1 .   | \$ 22.71                             | 1 .                               | 13 .                             | N  |
|  | 1800         | 1 .   | \$ 20.91                             | 1 .                               | 1 ·                              | N  |
|  | 1200         | 13 .  | \$ 14.13                             | <u> </u>                          | 1 .                              | N  |
|  | 000          | 1   | \$ 10.88                             |                                   | 1                                | N  |
|  | 600          | 1   | \$ 7.70                              | 1 .                               | 1                                | N  |
|  | 400          |   |                                      |                                   | · ·                              | M  |
|  | 300          |   | \$ 4.20                              | · ·                               |                                  | N  |
|  | 200          | 1.  | \$ 3.00                              | <u>.</u>                          | 12 .                             | N  |
|  | 100          |   | \$ 1.74                              | 1 .                               | 1                                | N  |
|  | 60           |   | \$ 1.14                              | · · ·                             |                                  | N  |
|  | 26           | 12  | \$ 0.82                              |                                   |                                  | N  |
|  | 18           | 15 .  | \$ 0.82                              |                                   |                                  | N  |
|  | 12           | 18 .  | \$ 0.62                              | · ·                               | 3 .                              | N  |
| able - Couper - Aarial - 28 Gauge  | 4200         | 1 .   | 5 7.10                               | 1 .                               | 1                                | N  |
| (Sphping)  | 3600         | 11 .  | \$ 6.08                              | 1 .                               | 1 .                              | N  |
|  | 3000         | 1 .   | \$ 5.07                              | \$ .                              | 1 .                              | N  |
|  | 2400         | 1 .   | \$ 3.86                              | 1 .                               | 1 .                              | N  |
|  | 2100         | 1 .   | \$ 3.38                              | · ·                               | 1                                | N  |
|  | 1800         | 5 .   | \$ 3.11                              | 1 .                               | 1 .                              | H  |
|  | 1200         | 1 .   | \$ 2.10                              | 1 .                               | 1 .                              | N  |
|  | 800          | 1 .   | \$ 1.62                              | 1 .                               | 1 .                              | N  |
|  | 000          | 1   | \$ 1.16                              | 1 .                               | 3 .                              | N  |
|  | 400          | 1 .   | \$ 0.79                              | 1 .                               | 1                                | N  |
| and the second sec | 300          | \$ .  | \$ 0.62                              |                                   | 1 .                              | N  |
|  | 200          | 1 .   | \$ 0.45                              | 1 .                               | 1 .                              | N  |
|  | 100          | 1 .   | \$ 0.26                              | 1 .                               | 1 .                              | N  |
|  | 60           | 1 .   | \$ 0.17                              | \$                                | 1 .                              | N  |
|  | 26           | 1 .   | \$ 0.12                              | \$ .                              | 1                                | N  |
|  | 1.0          | 1 .   | \$ 0.12                              | 1 .                               | 1 .                              | N  |
|  | 12           | 1 .   | \$ 0.12                              | \$ .                              | 1 .                              | N  |
| abls - Copper - Aarial - 28 Gauge  | 4200         | 15 .  | \$ 6.29                              | \$ .                              | 18 .                             | N  |
| (Engineering)  | 3000         | 1 .   | \$ 5.39                              | 1 .                               | 1 .                              | N  |
|  | 3000         | 1 .   | \$ 4.10                              | \$ .                              | 1 .                              | N  |
|  | 2400         | 1 .   | \$ 3.42                              | 1 .                               | 1 .                              | N  |
|  | 2100         | 1 .   | \$ 2.90                              | \$ .                              | 1 .                              | N  |
|  | 1800         | 15 -  | \$ 2.75                              | 1 .                               | 1 .                              | N  |
|  | 1200         | 1 .   | \$ 1.06                              | \$ .                              | 1 .                              | N  |
|  | 800          | 15 -  | \$ 1,43                              | \$ .                              | 1 .                              | N  |
|  | 000          | 1.5 .   | \$ 1,03                              | 1 .                               |                                  | N 1  |
|  | 400          | 1 .   | \$ 0.70                              | · ·                               | 1 .                              | N  |
|  | 300          | 1 .   | \$ 0.55                              | 1 .                               | 1 .                              | N  |
|  | 200          | 1 .   | \$ 0.59                              | 1 .                               | 1 .                              |  |
| and the second sec | 190          | 1 .   | \$ 0,23                              | 1 .                               | 15 .                             | N  |
|  | \$6          | 1 .   | \$ 0.15                              | 1 .                               |                                  | N  |
|  | 25           | 18  | 1 0.11                               | 1 .                               | 1 .                              | N  |
|  | 18           | 1 .   | \$ 0,11                              | ş .                               | 1 .                              | N 1  |
|  | 12           | 18 .  | \$ 0.11                              | 3 .                               | 1 .                              | N  |
| eble - Copper - Aerial - 28 Gauge  | 4200         | \$ 37.18  | \$ 67.63                             |                                   | \$ 55.04                         |  |
| LATOT  | 2600         | \$ 34.01  | 53.65                                | \$ 56.61                          | 48.27                            |  |
|  |              | 1 33.36   | \$ 69.74                             | \$ 32.03                          | \$ 40.49                         |  |
|  | 2400         | \$ 26.26  | \$ 53.00                             | 10.54                             | \$ 32.71<br>\$ 30.48             | 9 20/  |
|  | 2100         | \$ 20.88  |                                      | 1 16.72                           | 30.48                            | 9 18/  |
|  | 1800         | \$ 10.28  | 8 42.77                              | 14.47                             | 1 24.80                          | 4 16.  |
|  | 1200         | \$ 12.78  |                                      | 5 8.75                            | 16.52                            | 4 12/  |
|  | 900          | \$ 9.86<br>\$ 7.21                              | \$ 15.93                             | B 6.55                            | \$ 8.67                          |  |
|  | 600          |   |                                      | \$ 5.07                           | 5 5.95                           |  |
|  | 400          | \$ 5.58   |                                      | 8 4.27                            |                                  | and the second sec |
|  | 300          | 5 3.64  |                                      | 3 3.67                            | 3.45                             | • 6,<br>• 4,   |
|  | 200          | 8 2.00  | 1 3.65                               | 2.70                              | 224                              | 9 2  |
|  | 80           | 1 2.50  |                                      | 2.42                              | 1 1.62                           | 4 14   |
|  | 1 11         | \$ 2.50   | 1 1.68                               | 1 2.23                            | 3 129                            | 1 1/   |
|  | 25           | 2.50  | 1.68                                 | 1 1.50                            | 1 120                            | 0.   |
|  | 10           | 8 2.50  | 1 1.63                               |                                   |                                  | 0.0  |
| the Course Budget Manage   | 4200         | \$ 30.37  | 1.00                                 | \$53.50                           | 8 65.04                          | 4 0.<br>N  |
| ebie - Copper - Buried - 24 Gauge  | 100          | \$ 36.54  | \$ 23.26<br>\$ 10.03                 | 4321                              |                                  | N  |
| (Meteriel Cost)  | 3600         | 3478  | \$ 16.61                             | \$ 37.45                          | \$ 73.18                         | N  |
|  | 2400         | \$ 32.36  | \$ 13,29                             | 54.14                             | \$ 49.45                         | N  |
|  | 2100         | 1 97.00   | \$ 11.63                             | 23.18                             | 1 46                             | N  |
|  | 1800         | 1 - 56.64                                       | \$ 9.97                              | \$ 19.83                          | 1 35 24                          | N  |
|  | 1200         | 8 27.92<br>8 25.57<br>8 17.21                   | 3 0.64                               | \$ 11.45                          | 3 21.62                          | N  |
|  |              | 13.60   | \$ 4.90                              | 1024                              | 10.64                            | N  |
|  | 800          | 1.        | 1.5                                  |                                   |                                  |  |

20001\_318

#### Dockat No. 960896-TP J. W. Wells Esthbit No. \_\_\_\_ (WWV-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION   | Density Zona | BOPM 3.1<br>BellSouth -<br>Default<br>[1/16/98] | BCPM 3.1<br>Bellbouth-FL<br>(8/3/94) | 8CPM 3.1<br>Epiter-FL<br>[8/3/98] | 8CPM 8.1<br>0TE - FL<br>(8/3/94) | HM 5.0+<br>Flarida<br>(8/3/98) |
|---|--------------|---|--------------------------------------|-----------------------------------|----------------------------------|--------------------------------|
|   | 400          | 1 7,20  | \$ 2.32                              | \$ 0.30                           | \$ 7,67                          | N//                            |
|   | 300          | \$ 5.20   | \$ 1.86                              | \$ 8,27                           | \$ 6.95                          | N//                            |
|   | 200          | \$ 4.45   | \$ 1.22                              | \$ 4.51                           | \$ 4.35                          | 94/4                           |
|   | 100          | \$ 3.04   | \$ 0.65                              | \$ 3.07                           | \$ 2.71                          | N/-                            |
|   | 60           | \$ 2,50   | \$ 0.56                              | \$ 2.55                           | \$ 1,89                          | N//                            |
|   | 28           | \$ 2.08   | \$ 0.22                              | 8 2.27                            | \$ 1.41                          | N//                            |
|   | 10           | \$ 2.05   | \$ 0.22                              | \$ 1,98                           | \$ 1.50                          | N/                             |
|   | 12           | \$ 1.97   | \$ 0.22                              | \$ 1,73                           | \$ 1.34                          | 10                             |
| sble - Copper - Buried - 24 Gauge   | 4200         | 18 .  | \$ 13.32                             | 3 .                               | 1 .                              | N/                             |
| (Bupply Cost)   | 3600         | 18 -  | \$ 11.42                             | 5 .                               | \$ .                             | N/                             |
| instrum and   | 3000         | 15 .  | \$ 9.52                              | \$ .                              | \$ .                             | N/.                            |
|   | 2400         | 8 .   | \$ 7.61                              | \$ .                              | \$ .                             | 14/                            |
|   | 2100         | 5 .   | \$ 6.66                              | 1 .                               | \$ .                             | N                              |
|   | 1800         | 18 .  | \$ 5.71                              | \$ .                              | \$ .                             | N/                             |
|   | 1200         | 15 -  | \$ 3.60                              | \$ .                              | \$ .                             | N/                             |
|   | 900          | 15 .  | \$ 2,86                              | \$ .                              | 1 .                              | . 14/                          |
|   | 600          | 3 .   | \$ 1.92                              | \$ .                              | \$ .                             | N/                             |
|   | 400          | 8 .   | \$ 1,33                              | \$ .                              | \$ .                             | N/                             |
|   | 300          | 1 .   | \$ 1.07                              | \$ .                              | \$ .                             | NJ                             |
|   | 200          |   | \$ 0.70                              | 1                                 | \$ .                             | N/                             |
|   | 100          | 1   | 0.37                                 | 1                                 | 1                                | N                              |
|   | 60           | 1 .   | \$ 0.21                              | -                                 | 1                                | N                              |
|   |              | 1   | \$ 0.13                              |                                   | 1                                |                                |
|   | 25           | 1 .   | 1 0.13                               | 1                                 | 1                                | N                              |
|   | 18           |   | \$ 0.13                              |                                   | 1                                |                                |
|   | 12           | 1 .   | 1,40                                 | 2                                 |                                  | N                              |
| able - Copper - Buried - 24 Gauge   | 4,200        | 1   | 1.40                                 | 1 .                               | 3 .                              | N/                             |
| (Tex)   | 3600         | 1 .   | \$ 1.20                              | · ·                               | · ·                              | N                              |
|   | 3000         | 1 .   | \$ 1,00                              | 1 .                               | 5 .                              | N/                             |
|   | 2400         | 1 .   | \$ 0.60                              |                                   | 1 .                              | PU/                            |
|   | 2100         | 1 .   | \$ 0.70                              | 1 .                               | \$ .                             | N/                             |
|   | 1800         | 1 .   | \$ 0.60                              | 1 .                               | \$ .                             | N                              |
|   | 1200         | 1 .   | \$ 0.40                              | · ·                               | \$ ·                             | N/                             |
|   | \$90         | 1 .   | \$ 0.50                              | 5 .                               | 5 .                              | N                              |
|   | 600          | 1 .   | \$ 0.20                              | 1 .                               | \$ •                             | N                              |
|   | 400          | 1 .   | \$ 014                               | 1 .                               | 5 -                              | N.                             |
|   | 300          | 1 .   | \$ 0.11                              | 1 ·                               | \$ .                             | N/                             |
|   | 200          | 1 .   | \$ 0.07                              | s .                               | \$ .                             | N/                             |
|   | 100          | 4 .   | \$ 0.04                              | \$ -                              | 1 .                              | N/                             |
|   | 60           | \$ .  | \$ 0.02                              | 5 .                               | \$ .                             | N/                             |
|   | 25           | 15 .  | \$ 0.01                              | 1 .                               | 3 .                              | N,                             |
|   | 16           | 1 .   | \$ 0.01                              | \$ .                              | \$ .                             | N/                             |
|   | 12           | 1 .   | \$ 0.01                              | \$ .                              | 8 .                              | N/                             |
| able - Copper - Buried - 24 Gauge   | 4200         |   | \$ 34.64                             | 1 .                               | 3 .                              | N/                             |
| (Plesing)   | 2000         | 18 .  | \$ 29.69                             |                                   | 1 .                              | N                              |
|   | 3000         | 1 .   | \$ 24.74                             |                                   | 1 .                              | N                              |
|   | 2400         | 1 .   | \$ 19.79                             |                                   | \$ .                             | N                              |
| and the second se | 2100         | 1   | \$ 17.32                             |                                   | 3                                | N/                             |
|   | 1900         | 1   | \$ 14.84                             | 5 .                               | 1 .                              | N                              |
|   | 1200         | 1   | \$ 9,89                              | \$ .                              |                                  | N                              |
|   | 900          | 1   | 8 7.44                               | 1                                 | 1 .                              | N                              |
|   | 600          |   | 1 6.00                               |                                   | 1                                | N                              |
|   | 400          | 1   | \$ 3.40                              | 1                                 | 1                                | N                              |
|   | - 20         | 1   | \$ 2.77                              |                                   |                                  | N                              |
|   | 200          |   | \$ 1.01                              |                                   | 1                                | N                              |
|   | 100          | 1   | \$ 0.96                              | 1                                 | 1                                | N                              |
|   |              | 1   | \$ 0.54                              | 1                                 | 1                                | N                              |
|   | 50<br>28     | 1   | \$ 0.33                              | 1                                 | 13 .                             | N                              |
| and the second se | 1            |   | 1 100                                | 1                                 | 1                                |                                |
|   | 10           | 1 .   | \$ 0.33<br>\$ 0.33                   |                                   |                                  | N                              |
| the Course Ball I Have  | 12           |   |                                      |                                   |                                  | N                              |
| able - Copper - Buried - 24 Gauge   | 4200         | 1   |                                      | 1 .                               | 3 .                              | \$4.<br>N                      |
| (Splining)  | 3000         | 11  | 1                                    | 1                                 | 1 .                              | N                              |
| and the second se | 3000         |   | · · ·                                | 1                                 |                                  | N                              |
|   | 2400         | 1.  | 3 .                                  |                                   | 3 .                              | N                              |
|   | 2100         | · ·   |                                      | · ·                               | 1 .                              | N                              |
|   | 1800         |   | · ·                                  | 1                                 | 18 .                             | N                              |
|   | 1200         |   | 1                                    | 1 .                               | 1                                | M.                             |
|   | 000          | 1 .   |                                      | 1 .                               | 1 .                              | N                              |
|   | 000          | 1 .   |                                      | 1 .                               | 1                                | N                              |
|   | 400          |   | 1 .                                  | 5 .                               | \$ .                             | N                              |
|   | \$00         |   | 1 .                                  | 9 .                               | \$ -                             | N.                             |
|   | 200          | 1.  | 1 .                                  | 5 -                               | \$ .                             | N                              |
|   | 100          |   | 1 .                                  | \$ .                              | \$ .                             | N.                             |
|   | 80           | 1 .   | 1 .                                  | 1 .                               | \$ .                             | N                              |
|   | 26           |   | 1 .                                  | 6 .                               | 5 .                              | N                              |
|   | 10           | 1 .   | \$ .                                 | 1 .                               | \$ -                             | N                              |
|   | 17           | 1 .   | \$ .                                 | 1 .                               | \$ .                             | 84                             |
| able - Copper - Burled - 24 Geuge   | 4200         | 18 .  | \$ 10.55                             | 15 .                              | \$ .                             | N,                             |
| (Engineering)   | 5000         | 5 .   | 8 0.04                               | 5 .                               | \$ .                             | N                              |
|   |              |   | \$ 7.53                              |                                   |                                  |                                |

#### Dicket No. 800095-TP J. W. Wells Exhibit No. \_\_\_\_(J.WV-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zana | BCPM 3.1<br>Bellieuth -<br>Default<br>(1/16/98)  | BCPM 3.1<br>BellBouth-FL<br>[8/3/98] | BCPM 2.1<br>Sprint-FL<br>[8/2/96] | BCPM 3.1<br>GTE - FL<br>(5/3/96) | HM 5.0+<br>Florida<br>(8/2/96) |
|--|--------------|--|--------------------------------------|-----------------------------------|----------------------------------|--------------------------------|
|  | 2400         | 5 .  | 5 6.03                               | 5 .                               | 3 .                              | N/                             |
|  | 2100         | 18 .   | \$ 5.27                              | 5 .                               | \$ .                             | N/                             |
|  | 1800         | 1 .  | \$ 4.52                              | \$ -                              | \$ .                             | P4/                            |
|  | 1200         | 1 .  | \$ 3.01                              | \$ .                              | 1 .                              | N/                             |
|  | 900          | 15 .   | 3 2.26                               | 1                                 | 5 .                              | N/                             |
|  | 600          | 8  | \$ 1.52                              |                                   | 1 .                              | N/                             |
|  | 400          | 1 .  | \$ 1.05                              | 1 .                               | 1                                | N/                             |
| and the state of t | 300          | 18 . 1   | 3 0.84                               | 1 .                               | 1 .                              | N/                             |
|  | 200          |  | \$ 0.55                              | 1                                 | 1                                |                                |
|  |              |  | 5 0.26                               |                                   |                                  | N/1                            |
|  | 100          | 12   | 0.17                                 | <u>.</u>                          |                                  | - NO                           |
|  | 60           | 1 .  | 5 0.10                               | · · ·                             |                                  | N/                             |
|  | 28           | 1 .  |                                      |                                   |                                  | N/                             |
|  | 10           | 19 .   | \$ 0.10                              |                                   | · ·                              | N/                             |
|  | 12           | 5 .  | \$ 0.10                              |                                   | \$                               | NJ                             |
| able - Copper - Buried - 24 Gauge  | 4200         | \$ 36.37   | \$ 83.16                             |                                   | \$ 85.04                         | 4 30,1                         |
| LATOT  | 3800         | \$ 35.58   | \$ 71.28                             | \$ 43.21                          | \$ 73.13                         | 4 27.0                         |
| 0.1.M.19   | 3000         | \$ 34.79   | \$ 59.40                             | \$ 37.45                          | \$ 61.31                         | 4 23.0                         |
|  | 2400         | \$ 32.56   | 47.82                                | 3 20.10                           | \$ 40.45                         | 4 20.0                         |
|  | 2100         | 8 5765   | \$ 41.58                             |                                   | \$ 43.60                         | 4 18.7                         |
|  | 1800         | \$ 25.57   | 35.64                                | 1 1844                            | \$ 35,24                         | 6 10.0                         |
| the second beauty and the second seco |              | 1 1721   | 1 23.73                              | \$ 11.45                          | 1 21.62                          |                                |
|  | 1200         | 1 1/41   | 17.80                                | 11/10                             | \$ 16.56                         | 1 124                          |
|  | 800          | 13.66  | 1/.60                                | \$ 10.24<br>\$ 7.55               | 10.00                            | 4 10,4                         |
|  | 600          | \$ 9.05  | \$ 12.02                             | 7.55                              | \$ 11.33                         | 8 8.0                          |
|  | 400          | \$ 7.20  | \$ 8.30                              |                                   | \$ 7,67                          | 4 8.2                          |
|  | 300          | \$ 5.29  | 5 6.60                               | \$ 5,27                           | \$ 5.95                          | 4 6,3                          |
|  | 200          | \$ 4.45  | \$ 4.55                              | \$ 4,01                           | \$ 4.55                          | 4 4,4                          |
|  | 100          | \$ 3.04  | \$ 2.51                              | \$ 3.07                           | \$ 2.71                          | 4 2.6                          |
|  | 50           | \$ 2.50  | \$ 1,30                              | \$ 2,55<br>\$ 2,27<br>\$ 1,06     | \$ 1.69                          | 0 1.7                          |
|  | 28           | \$ 2.08  | 1 0.76                               | \$ 2.97                           | \$ 1.41                          | 0 1.2                          |
|  | 12           | 3 2.05   | \$ 0.78                              | \$ 1.05                           | 1 130                            | 0.7                            |
|  | 6            | \$ 1.97  |                                      | \$ 1.73                           | \$ 134                           | 4 0.6                          |
|  |              | 3 33.16  | \$ 16.73                             |                                   |                                  |                                |
| eble - Copper - Buried - 20 Gauge  | 4200         |  |                                      |                                   |                                  | N/                             |
| (Material)   | 3600         | \$ 30.20   | 5 14.34                              |                                   | 41.45                            | N                              |
|  | 3000         | 8 29.10  | \$ 11.95                             |                                   | \$ 40.64                         | N                              |
|  | 2400         | \$ 28.79   | \$ 9.58                              |                                   | \$ 32.82                         | N/                             |
|  | 2100         | \$ 22.60   | \$ 8,49                              |                                   | \$ 29.03                         | N/                             |
|  | 1800         | \$ 20.46   | \$ 7,45                              | \$ 15.63                          | \$ 23.49                         | N/                             |
|  | 1200         | \$ 13.20   | \$ 5.55                              | \$ 8,80                           | \$ 15.88                         | N                              |
|  | 800          | \$ 10.70   | \$ 3.70                              | \$ 8.24                           | \$ 12.22                         | N                              |
|  | 800          | \$ 7.27  | \$ 2.87                              |                                   | \$ 0.59                          | N                              |
|  | 400          | \$ 5.67  | \$ 1.82                              | \$ 5.42                           | \$ 6.05                          | N                              |
| and the second se  | 300          | \$ 4.38  | \$ 1.37                              |                                   | 8 4.76                           | N/                             |
|  | 200          | \$ 3.40  | \$ 0.99                              | \$ 4.07                           | \$ 3.51                          | N                              |
|  |              | \$ 2.52  | \$ 0.54                              | \$ 2.85                           | \$ 2.26                          |                                |
| and the second sec   | 100          | 5 2.10   | \$ 0.33                              |                                   | 1 1.65                           | N/                             |
|  | 60           |  |                                      |                                   |                                  | N/                             |
|  | 25           | \$ 1,93  | \$ 0.25                              | \$ 2.22                           | \$ 1.30                          | N                              |
|  | 10           | \$ 1.93  | \$ 0.23                              | \$ 1,84                           | \$ 1.30                          | P4/                            |
|  | 12           | \$ 1,03  | \$ 0.23                              |                                   | \$ 1,30                          | N                              |
| eble - Copper - Buried - 29 Geoge  | 4200         | 18 .   | \$ 12.70                             | 5 .                               | 1 .                              | N.                             |
| (Supply Cost)  | 3800         | 15 .   | \$ 10.88                             |                                   | \$ .                             | N                              |
|  | 3000         | 18 .   | \$ 9.07                              |                                   | 1 .                              | N                              |
| and the second sec   | 2400         | 1  | \$ 7,26                              |                                   |                                  | N                              |
|  | 2100         | 18 .   | \$ 6.44                              |                                   | 1                                | N                              |
|  |              |  |                                      |                                   |                                  |                                |
|  | 1800         | 1 .  | \$ 5.65<br>\$ 4.20<br>\$ 2.81        |                                   | · · · ·                          | N                              |
|  | 1200         |  | 5.40                                 |                                   | · · ·                            | N                              |
|  | 900          | 1 .  | 2.01                                 |                                   |                                  | N                              |
|  | 600          | 1 .  | 3 2.10 j                             | a .                               |                                  | N                              |
|  | 400          | 15 .   | \$ 1.56                              |                                   |                                  | N                              |
| which have been also   | 300          | 8 .  | \$ 1.04                              |                                   | 1 .                              |                                |
|  | 200          |  | \$ 0.75                              | • •                               | 1 .                              | N                              |
|  | 100          | 3 .  | 5 0.41<br>5 0.25<br>5 0.17           | \$                                | 1 .                              | N.                             |
|  | 50           | 5 .  | \$ 0.25                              | \$ .                              |                                  | N                              |
|  | 20           | 5 .  | \$ 0.17                              | 5 .                               | 5 .                              | PL.                            |
|  | 10           | 8 -  | \$ 0.17                              | 1 .                               | 5 .                              | N                              |
|  | 12           | \$ .   | \$ 0.17                              |                                   | 1                                | N                              |
| abla - Copper - Burled - 25 Gauge  | 4200         | and and present out of the local division of | 1.00                                 |                                   | -                                |                                |
|  | 2450         |  | 1.00                                 |                                   | 1 .                              | N                              |
| (Tex)  | 3600         | 1 .  | \$ 0.86<br>\$ 0.72                   | 1 .                               |                                  | N                              |
|  | 3000         | 1 .  | B 0.72                               | 1 .                               | · ·                              | N                              |
|  | 2400         | 1 .  | \$ 0.57                              | 1 .                               | · ·                              | N                              |
|  | 2100         | 5 -  | \$ 0.51                              | \$ .                              | 5 .                              | N.                             |
|  | 1800         | 5 .  | \$ 0.45                              | 1 .                               | \$ .                             | N                              |
|  | 1200         | 3 .  | \$ 0.33                              | 1 .                               | \$ .                             | N                              |
|  | 800          | 5 .  | 8 0.33<br>8 0.22<br>8 0.17           | 1 .                               | 1 .                              | N                              |
|  |              |  | 1 017                                | 1                                 | 1                                | N.                             |
|  | 600          |  |                                      |                                   | -                                |                                |
|  | 600          |  | 1 011                                |                                   |                                  |                                |
|  | 400          | 5 -  | \$ 0.11                              | 1 .                               |                                  | N                              |
|  | 400          | 5 -  | \$ 0.11                              |                                   |                                  | N                              |
|  | 400          | 5 -  | \$ 0.11                              | 1 .                               |                                  |                                |

# Docket No. 980096-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Denalty Zone | BCPM 3.1<br>BellSouth -<br>Default<br>(1/16/98) | BCPM 3.1<br>Beldouth-FL<br>(8/3/98) | BCPM 3.1<br>Sprint FL<br>(6/2/94) | BCPM 3.1<br>GTE - FL<br>(8/5/98) | HM 8.0a<br>Flatida<br>(8/2/98) |
|--|--------------|---|-------------------------------------|-----------------------------------|----------------------------------|--------------------------------|
| and the second sec | 25           | 1 S   | \$ 0.01                             | 1 .                               | 1 .                              | N/A                            |
|  | 18           | 1 .   | \$ 0.01                             | 1 .                               | 1                                | NJA                            |
|  | 12           | 3 .   | \$ 0.01                             | \$ .                              | 1 .                              | N/A                            |
| Cable - Copper - Buried - 26 Gauge   | 4200         | 3 .   | \$ 31.15                            | \$ .                              | 5 .                              | N/A                            |
| (Placing)  | 3000         | 1 .   | \$ 28,70                            | 1 .                               | 1 .                              | N/A                            |
|  | 1000         | 1 .   | \$ 22.25                            | \$                                | 1 .                              | N/A                            |
|  | 2400         | 1 .   | \$ 17.80                            | 1 .                               | 1 .                              | N/A                            |
|  | 2100         | 13 .  | \$ 15.81                            | 1                                 | 1                                | N/A                            |
|  | 1800         | 1   | 5 13.87                             |                                   | 1                                | NIA                            |
|  | 900          | 1   | \$ 10.30                            | 1 .                               |                                  | N/A                            |
|  | 800          | 1   | \$ 5.36                             | 1 .                               | 1.                               | N/A                            |
| and the second se  | 400          | 1   | \$ 3.59                             | 1                                 |                                  | N/A                            |
|  | 300          | 1   | 3 2.55                              | 1 .                               | 1                                | N/A                            |
|  | 200          | 1   | \$ 2.56<br>\$ 1.84                  | 1 .                               | 1                                | N/A                            |
|  | 100          | 18 .  | \$ 1.01                             | 1                                 | 1                                | N/A                            |
|  | 80           | 1 .   | 8 0.02                              | 1 .                               | 1                                | N/A                            |
|  | 25           | 18 .  | \$ 0.43                             | 1 .                               | 1                                | N/A                            |
|  | 10           | 1 .   | \$ 0.43                             | \$ .                              | 1 .                              | N/A                            |
|  | 12           | 18 .  | \$ 0.43                             | \$ .                              | 1 .                              | N/A                            |
| Cable - Copper - Burled - 26 Gauge   | 4200         | 3 .   | \$ .                                | \$ .                              | 1 .                              | N/A                            |
| (Splicing)   | 3600         | 1 .   | 1 .                                 | \$ .                              | 18 .                             | N/A                            |
|  | 3000         | 1 .   | 5 .                                 | \$ .                              | 1 .                              | N/A                            |
|  | 2400         | 1 .   | 1 .                                 | \$ .                              | 4 .                              | N/A                            |
|  | 2100         | 1 .   | \$ .                                | 1 .                               | 1 .                              | N/A                            |
|  | 1800         |   | 1 .                                 | \$                                | 1 .                              | N/A                            |
| and the second second  | 1200         | 1 .   | \$ .                                | 1 .                               | 1 .                              | N/A                            |
|  | 800          | 1 .   | \$ .                                | 1 .                               | \$ .                             | N/A                            |
|  | 600          | 1   | 1 .                                 | 1 .                               | 1 .                              | N/A                            |
| and the second sec | 400          | 18 .  | 3 .                                 | ş                                 | \$                               | N/A                            |
|  | 300          | 1.  |                                     |                                   | 1 .                              | N/A                            |
|  | 200          | 1   | 1 .                                 |                                   | 1 .                              | N(A                            |
|  | 100          | 12 .  |                                     |                                   | 1                                | N/A                            |
|  | 60           | 19 .  | 3 .                                 | · ·                               |                                  | N/A                            |
|  | 25           | 1   | 3 .                                 |                                   | 13 .                             | N/A                            |
|  | 12           | 1   | 3 .                                 | 1 :                               | 1                                | N/A                            |
| Cable - Cepper - Buried - 28 Gauge   | 4200         | 13 .  | \$ 7.50                             |                                   | 1                                | N/A                            |
| (Engineering)  | 3800         | 1   | \$ 6.50                             | 1 .                               | 1                                | N/A                            |
|  | 3000         | 18 .  | \$ 5.42                             | 1 .                               | 18 .                             | N/A                            |
|  | 2400         | \$ .  | \$ 4.34                             | 1 .                               | 1.                               | N/A                            |
|  | 2100         | 1 .   | \$ 3.85                             | 1 .                               | 1 .                              | PL/A                           |
|  | 1800         | 1 .   | \$ 3.38                             | 1 .                               | 1 .                              | N/A                            |
|  | 1200         | 1 .   | \$ 2.51                             | \$ .                              | 1 .                              | N/A                            |
|  | 800          | 15 .  | \$ 1.68                             | 1 .                               | 1 .                              | N/A                            |
|  | 600          | 1 .   | \$ 1.30                             | 1 .                               | 1 .                              | N/A                            |
|  | 400          | 1.  | \$ 0.83                             | 1 .                               | \$ .                             | N/A                            |
|  | 300          | 3 .   | \$ 0.62                             | · ·                               | 1.                               | N/A                            |
|  | 200          | 12 .  | 1 0.45                              |                                   |                                  |                                |
|  | 100          | 1   | \$ 0.25                             |                                   | 1                                | N/A                            |
| the second s   | 15           | 1   | \$ 0.10                             | 1 :                               | 1                                | N/A                            |
| and the second se  | 18           | 1 .   | \$ 0.10                             |                                   | 1                                | N/A                            |
|  | 12           | 1   | \$ 0.10                             | 1                                 | 1                                | N/A                            |
| Cable - Copper - Buried - 26 Gauge   | 4200         | \$ 33.16  | \$ 69.17                            |                                   |                                  | \$ \$0,18                      |
| (LATOT)  | 3600         | 30.20   | \$ 60.50                            | \$ 43.21                          | \$ 48.45                         | 8 27.04                        |
|  | 3000         | \$ 29.10  | \$ 40.41                            | \$ 37.45                          | \$ 40.64                         | 4 23.92                        |
|  | 2400         | \$ 26.70  | 1 39.53                             | \$ 20.66                          | \$ 32.82                         | \$ 20,80                       |
|  | 2100         | \$ 22.60  | 3 35.101                            | \$ 16.53                          | \$ 29.03                         | 4 18.72                        |
|  | 1800         | \$ 20.48  |                                     | 15,83                             | \$ 25.49                         | \$ 10.04                       |
|  | 1200         | \$ 13.20  | \$ 22.68                            | \$ 8,00                           | \$ 15.68                         | 4 12,48                        |
|  | 800          | 10.70   | \$ 15.51                            | 8.24                              |                                  |                                |
|  | 600          | \$ 7,27   | \$ 11.87                            | 8 6.21                            | \$ 8.50                          | 4 8.00                         |
|  | 400          | \$ 4.38   | \$ 7.53                             | 5 6.42                            | \$ 6.05                          | 6 0.24                         |
|  | 200          | \$ 3.49   | \$ 4.09                             | 4.07                              | \$ 3.51                          |                                |
| the second se  | 100          | \$ 2.52   | \$ 224                              | 2.65                              | \$ 2.20                          |                                |
|  | \$0          | \$ 2.16   | \$ 1.30                             | 1 244                             | \$ 1.65                          |                                |
|  | 28           | 1 1.93  | \$ 0.95                             | 1 2.22                            | \$ 1.50                          | 4 1.24                         |
|  | 18           | 1 1.93  |                                     | \$ 1.04                           | 1 15                             | 0.70                           |
|  | 12           | \$ 1.93   | \$ 0.95                             | \$ 1.70                           | s 130<br>s 130                   | 8 0.88                         |
| Cable - Copper - Underground - 24 Clau   | 4200         | \$ 48.48  | \$ 21.09                            | \$ 61.60                          | \$ 73.67                         | N/A                            |
| (Material)   | 3000         | \$ 42.91  | \$ 18.08                            | \$ 50.61                          | \$ 63.40                         | N/A                            |
|  | \$000        | 1 39.53   | \$ 15.08                            | \$ 43.65                          | \$ 53,12                         | N/A                            |
|  | 2400         | 3 29.07   | \$ 12.05                            | 1 31.51                           | 5 42.84                          | N/A                            |
|  | 2100         | \$ 27.00  | \$ 10.61                            | \$ 27.68                          | 5 57.60                          | N/A                            |
|  | 1800         | \$ 24.27  | \$ 0.50                             | \$ 23.60                          | 12.40                            | N/A                            |
|  | 1200         | \$ 16.72  | \$ 6.24                             | \$ 14,21                          | 22.40                            | N/A                            |
|  | 1290         | 5 10.72<br>5 13.82                              | 3 6.24<br>8 6.52                    | s 14.21<br>s 12.30                | 17.79 D                          |                                |

3,8101,328

#### Docket No. 950896-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zona          | BCPM 3.1<br>BallSouth -<br>Default<br>(1/16/98) | BCPM 3.1<br>Ballbeuth-FL<br>(B/3/86)  | BOPM 3.1<br>Revint-FL<br>(8/3/98)  | BOPM 3.1<br>GTE - FL<br>[8/3/98]  | Hint 8.0+<br>Florida<br>(8/3/98) |
|--|-----------------------|---|---|--|---|----------------------------------|
|  | 600                   | \$ 9.54   | \$ 3,25   | \$ 8.85  | \$ 12.10  | PG/                              |
|  | 400                   | \$ 7.89   | \$ 2.17   | \$ 3.51  |   | N                                |
|  | 300                   | \$ 5.26   |   | \$ 7.10  | \$ 5.77   | N,                               |
|  | 200                   | \$ 4.22   | \$ 1.08   | \$ 5.47  |   | N                                |
|  | 100                   | \$ 2.92   | \$ 0.54   | \$ 4.03  | \$ 2.58   | N                                |
|  | 50                    | \$ 2.16   | \$ 0.27   | \$ 3.51  | \$ 1.01   | N                                |
|  | 25                    | \$ 1.39   | \$ 0.14   |  | 1 1.33  | N                                |
|  | 18                    | \$ 1.39   | \$ 0.14   |  |   | N                                |
|  | 12                    | \$ 1.50   |   | \$ 2.54  | \$ 1.33   |                                  |
| able - Copper - Underground - 24 Gau   | 4200                  | 1   | \$ 18.21  | 1  | the second se | N                                |
| (Supply Cost)  | 3600                  | 1   | \$ 15.60  |  |   | N                                |
| logger sort  | 3000                  | 1   | \$ 13.00  |  | 1 .   | N                                |
|  | 2400                  | 1   | \$ 10.40  |  | 1   | N                                |
|  | 2100                  |   | \$ 9.16   |  | 1 1   | N                                |
|  | 1800                  | 1   | \$ 8.10   |  |   | N                                |
|  | 1200                  |   | \$ 5.39   |  |   | <u>N</u>                         |
|  | 900                   |   | \$ 5.63   |  |   | N                                |
|  |                       |   |   |  |   | N                                |
|  | 600                   |   | \$ 2.81   | 2 .  | 1   | N                                |
| and the second sec | 400                   | 1 .   | \$ 1.87   | 5 .  | 3 .   | N                                |
|  | 300                   | ş .   | \$ 1.40   | \$ ·   | 1 .   | N                                |
|  | 200                   | 1 .   | \$ 0.94   | ŧ .  | \$ .  | N                                |
|  | 100                   | · ·   | \$ 0.47   | 5 .  | \$ -  | N                                |
| the second se  | 50                    |   | \$ 0.23   | \$ .   | \$ .  | N                                |
|  | 25                    | \$ -  | \$ 0.12   | \$ •   | \$ .  | N                                |
|  | 18                    | \$ .  | \$ 0,12   | \$ .   | \$ .  | N                                |
|  | 12                    | \$ .  | \$ 0.12   | 5 .  | \$ .  | N                                |
| able - Copper - U. derground - 24 Gau  | 4200                  | 3 .   | \$ 1.27   |  | 1   | N                                |
| (Tex)  | 2600                  | 1 .   | \$ 1.08   | 1  | 1   | N                                |
|  | 3000                  | 1 .   | \$ 0.90   | 1  | 1   |                                  |
|  | 2400                  | 1   | \$ 0.72   | 1 .  |   | N                                |
|  | 2100                  |   | \$ 0.64   |  |   | N                                |
|  | 1800                  |   | the second se | Contraction of the local division of the loc | 1 1   | N                                |
|  | 1200                  |   | \$ 0.37   |  |   | N                                |
|  |                       | · ·   |   |  |   | N                                |
|  | 000                   | 3 · ·   |   |  |   | N                                |
|  | 600                   | 3 ·   | \$ 0.20   | 2 .  |   | N                                |
|  | 400                   | 3 .   | \$ 0.13   | 5 .  | \$ .  | N                                |
|  | 300                   | · ·   | \$ 0,10   | \$ .   | \$ .  | N                                |
|  | 200                   | 1 .   | \$ 0.07   | \$ .   | 1   | N                                |
|  | 100                   | \$ .  | \$ 0.03   | 5 .  | \$  | N                                |
|  | 50                    | 1 .   | \$ 0.02   | ş  | \$ -  | N                                |
|  | 25                    | \$ .  | \$ 0.01   | \$ .   | 8 .   | N                                |
|  | .10                   | \$ .  | \$ 0.01   | \$   | \$ .  | N                                |
|  | 12                    | \$ -  | \$ 0.01   | \$ .   | \$  | N                                |
| ebie - Copper - Underground - 24 Geu   | 4200                  | \$ .  | \$ 40.18  | \$ .   | 1   | N                                |
| Placing)   | 3600                  | 5 .   | \$ 34.44  |  |   | N                                |
|  | 3000                  | 3 .   | \$ 28.70  |  | 1   | N                                |
|  | 2400                  | 1 .   | \$ 22.96  |  | 1   | N                                |
|  | 2100                  | 1 .   | \$ 20,22  | 5 .  | 1 . 1   |                                  |
|  | 1800                  | 1 .   | 17.87   |  |   | N                                |
|  | 1200                  | 1   | \$ 11.60  |  |   | H                                |
|  | 800                   | 1   | \$ 12.43  |  |   | N                                |
|  | 600                   | 1   | 5 6.10  |  |   | N                                |
|  |                       |   |   |  |   | N                                |
|  | 400                   | 3 .   | \$ 415  |  | 3 · · ·   | N                                |
|  | 300                   | 3 .   | \$ 3.10   | · ·  |   | N                                |
|  | 200                   |   | \$ 2.00   |  | 1 .   | N                                |
|  | 100                   | 5 .   | \$ 1,05   |  |   | N                                |
|  | 50                    | 8 .   | \$ 0.62   |  |   | N                                |
|  | 25                    |   | \$ 0.26   |  |   | N                                |
|  | 18                    | \$ .  | \$ 0.26   |  | \$ .  | N.                               |
|  | 12                    | 5 .   | \$ 0.26   | s · ·  | 1 .   | N.                               |
| eble - Copper - Underground - 24 Gau   | 4200                  | \$ .  | \$ 8,58   | 5  | 1 .   | N.                               |
| (lploing)  | 3600                  | 1 .   | \$ 7,55<br>\$ 6,13  | 5 -  | \$ .  | N                                |
|  | 3000                  | \$ .  | \$ 8,13   | 5 .  | \$ .  | N/                               |
|  | 2400                  | 5 .   | \$ 4.00   | 5 .  |   | N                                |
|  | 2100                  | 1 .   | 4 4 92  |  | \$ .  | N                                |
| and the second se  | 1800                  | \$ .  | \$ 182  |  |   | N/                               |
|  | 1200                  | \$ .  | 1 J.82<br>5 2.84<br>1 2.65  |  | 5 .   | N                                |
|  | 900                   | 5 .   | \$ 2.65   |  | 5   | N                                |
|  | 000                   | 5 .   | \$ 1.32   |  | 1   | N/                               |
| the second se  | 400                   | \$ .  | \$ 0.88   |  | 1   | N                                |
|  | \$00                  | 1 .   | \$ 0.66   |  |   |                                  |
|  |                       | 1   | \$ 0.44   |  |   | - No                             |
|  | 200                   |   |   |  |   | N/                               |
|  | 200                   |   | £ 0.551   |  |   |                                  |
|  | 100                   | \$ .  | \$ 0.22   |  |   |                                  |
|  | 100                   | 1 .   | \$ 0.11   |  |   | N/                               |
|  | 100<br>50<br>25       | · ·   | \$ 0.08   |  |   | N/                               |
|  | 100<br>60<br>28<br>19 | · ·   | \$ 0.08<br>\$ 0.08<br>\$ 0.06   |  |   | N/<br>N/                         |
| sbie - Copper - Underground - 24 Geu   | 100<br>50<br>25       | · ·   | \$ 0.08   |  |   | N/                               |

### Docket No. 980696-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-6) Input Virlue Comperisons

| INPUT VALUE DESCRIPTION   | Density Zone | BCPM 3.1<br>BellBouth -<br>Default<br>(1/16/00)   | BCPM 3.1<br>Betdeuth-FL<br>[8/3/98] | BCPM 3.1<br>8ptnt-FL<br>(8/3/98) | BCPM 3.1<br>GTE - FL<br>(8/3/98) | Pitel B.C.<br>Florida<br>(8/3/90) |
|---|--------------|---|-------------------------------------|----------------------------------|----------------------------------|-----------------------------------|
|   | 3000         | 5 -   | 8 4.21                              | 1 .                              | \$ .                             | N/                                |
|   | 2400         | 5 .   | \$ 3.37                             | \$ .                             | 1 .                              | N.                                |
|   | 2100         | \$ .  | \$ 2.97                             | \$ .                             | \$ .                             | N                                 |
|   | 1800         | 5 .   | 1 2.62                              | 1 .                              | 1 .                              | N.                                |
|   | 1200         | 1   | \$ 1.74<br>\$ 1.82                  |                                  |                                  | N                                 |
|   | 800          | 1 .   | 5 0.91                              |                                  | · ·                              | N                                 |
|   | 400          | 1   | 1 0.61                              |                                  |                                  | N                                 |
|   | 300          | 1   | \$ 0.45                             | 1                                | 3 .                              | PA/                               |
| the second s  | 200          | \$ .  | 1 0.50                              | 1                                | 1 .                              | N/                                |
|   | 100          | 1   | 8 0.15                              | \$                               | 1                                | N                                 |
|   | 80           | \$ .  | \$ 0.08                             | 1 .                              | \$ .                             | N                                 |
|   | 28           | 5 -   | \$ 0.04                             | \$ .                             | \$ .                             | N/                                |
|   | 18           | \$ .  | \$ 0.04                             | \$ .                             | \$ .                             | N.                                |
|   | 12           | \$ .  | \$ 0.04                             | 1 .                              | 1 .                              | 14                                |
| able - Copper - L'-Jerground - 24 Gau   | 4200         | \$ 46.48  | \$ 05.21                            | \$ 61.69                         | \$ 73.67                         | 4 28.0                            |
| (LATOT)   | 3600         | \$ 42.91  | \$ 81,61                            | \$ 50.61                         | \$ 63.40                         | \$ 26.0                           |
|   | 3000         | \$ 39.33  | \$ 68.01                            | \$ 43.65                         |                                  |                                   |
|   | 2400         | \$ 29.97  | \$ 54.41                            | \$ 31,51                         | \$ 42.84                         | \$ 20.0                           |
|   | 2100         | \$ 27.00  | 47.01                               | \$ 27.68                         | \$ 37.66                         | 4 10.0                            |
|   | 1800         | \$ 2427   | \$ 42.35                            | \$ 23.80                         | \$ 52.72                         | 4 10.0                            |
|   | 1200         | \$ 16.72  | \$ 28.19                            | 5 1421                           | \$ 22.40                         | 120                               |
|   | 900          | \$ 13.82  | \$ 29.45<br>\$ 14.68                | \$ 12.39<br>\$ 8.95              | \$ 17.79                         | 1 10.0                            |
|   | 400          | 5 7.50  | 9 14.00<br>9 9.78                   | 3 0.00                           | 5 12.10                          | 4 7.                              |
|   | 300          | \$ 6,26   | 1 7.34                              | 5 7.10                           | \$ 5.77                          | 1 6.0<br>1 6.1                    |
|   | 200          | 5 4.22  | 4.59                                | 5 8.47                           | \$ 4.20                          | 4 6.<br>4 4.                      |
|   | 100          | 8 2.92  | 1 2.45                              | 4.03                             | 1 2.58                           | 1 2                               |
|   | 50           | \$ 2.10   | 1 1.22                              | \$ 3.51                          | 1 1.01                           | 5 1/                              |
|   | 25           | \$ 1.39   | 1 0.61                              | \$ 3.23                          | 1 1.55                           | 4 1.                              |
|   | 18           | \$ 1.39   | \$ 0.61                             | \$ 2.63                          | \$ 1.33                          | 0.                                |
|   | 12           | \$ 1.39   | \$ 0.61                             | \$ 2.54                          | \$ 1.33                          | \$ 0.                             |
| able - Copper - Underground - 26 Gau  | 4200         | \$ 35.60  | \$ 14.55                            | \$ 61.69                         | \$ 58.03                         | N                                 |
| (Motorial)  | 3600         | \$ 33.30  | \$ 12.56                            | \$ 50.61                         | \$ 50.73                         | N                                 |
|   | 3000         | \$ 28.21  | \$ 10.59                            | \$ 43.65                         | \$ 42.53                         | N                                 |
|   | 2400         | \$ 21.50  | \$ 8.57                             | \$ 20.53                         | \$ 34.52                         | 24                                |
|   | 2100         | \$ 19.40  | \$ 7.57                             | \$ 23.32                         | \$ 50.34                         | N                                 |
|   | 1800         | \$ 17.38  | \$ 6.55                             | \$ 20.05                         | \$ 24.54                         | N                                 |
|   | 1200         | \$ 11.95  | \$ 4.57                             | \$ 11.71                         | \$ 17.28                         | N                                 |
| the second se | 800          | \$ 9.96   | \$ 3.51                             | \$ 10.51                         | \$ 12.82                         | N                                 |
|   | 600          | \$ 7.52   | \$ 2.35                             | \$ 7.70                          | \$ 9,01                          |                                   |
|   | 400          | 3 6.55  | \$ 1.57                             | \$ 7,69                          | \$ 5.78                          | N                                 |
|   | 300          | 3 4.42  | 5 1.18                              | 5 6.45<br>5 5.05                 | \$ 4.65                          | N                                 |
|   | 200          | \$ 3.60   | \$ 0.78                             | 5 3.82                           | \$ 3.40<br>\$ 2.16               | N                                 |
|   | 100          | \$ 1.19   | \$ 0.30<br>\$ 0.20                  | 5 3.40                           | 5 1.54                           | N                                 |
|   |              | \$ 1.00   | \$ 0,10                             | \$ 3.18                          | 1 122                            | N                                 |
|   | 25           | \$ 1.00   | \$ 0.10                             | \$ 2.78                          | 1 122                            | N                                 |
|   | 0            | \$ 1.00   | \$ 0.10                             | \$ 2.51                          | 1 122                            | N                                 |
| able - Copper - Underground - 26 Gau  | 4200         | 3   | 3 16.65                             | -                                | 144                              | N                                 |
| (Supply Ceet)   | 3000         | 3 .   | \$ 14.40                            | 1                                | 1                                | N                                 |
|   | 3000         | \$ .  | \$ 12.14                            | 1 .                              | 1 .                              | N                                 |
|   | 2400         | \$ .  | £8.9 £                              |                                  | 1 .                              | N                                 |
|   | 2100         | 5 -   | \$ 0.68                             | \$ .                             | \$ .                             | N                                 |
|   | 1800         | 3 .   | \$ 7.51                             | 1 .                              | 1 .                              | N                                 |
|   | 1200         | 3 .   | \$ 5,23                             |                                  | 1 .                              | N                                 |
|   | 800          | 1 .   | 4.02                                |                                  | 1 .                              | N                                 |
|   | 600          | 1 .   | \$ 2.69                             |                                  | \$                               | N                                 |
|   | 400          | 1 .   | 1 1.60                              |                                  | 1 .                              | N                                 |
|   | 300          | 1 .   | \$ 1.35<br>0.90                     |                                  |                                  | N                                 |
|   | 100          | 1 .   | 0.43                                |                                  | 1                                | N                                 |
|   | 50           | 1 .   | 3 0.22                              |                                  | 1 .                              | N                                 |
|   | 25           | 1   | 0.11                                |                                  | 1 .                              | N                                 |
|   | 10           | 1   | 0.11                                |                                  | 1                                | N                                 |
|   | 12           | and the second se | 1 0.11                              |                                  | 1                                | N. N.                             |
| able - Copper - Underground - 28 Geu  | 4200         | 3 .   | \$ 0.87                             |                                  | 1                                | N                                 |
| Text  | 3000         | \$ .  | \$ 0.75                             |                                  | 1                                | N                                 |
|   | 3000         | \$ .  | \$ 0.64                             |                                  | 1 .                              | N/                                |
|   | 2400         | \$ .  | \$ 0.51                             |                                  | 1 .                              | N                                 |
|   | 2100         | \$ .  | \$ 0.45                             |                                  |                                  | N                                 |
|   | 1800         | 1 .   | 1 0.59                              | s - 1                            |                                  | N                                 |
|   | 1,200        | \$ .  | 0.27                                |                                  | \$ · ·                           | 84                                |
|   | 800          |   | 0.21                                | 5 ·                              | 1 .                              | N/                                |
|   | 600          | 5 .   | 1 0.14                              |                                  |                                  | N                                 |
|   | 400          | 5 -   | \$ 0.0¥                             |                                  | 1 .                              | N                                 |
|   | 300          | \$ .  | 1 0.07                              | ş .                              | ş .                              | N                                 |
|   | 200          | 1 .   | \$ 0.05                             | 5 - 1                            | 5                                |                                   |

#### Docket No. 980698-TP J. W. Wells Exhibit No. \_\_\_\_ (AWW-r) Input Value Compensions

| INPUT VALUE DEBORPTION                | Density Zone | BCPM 3.1<br>Balifouth -<br>Default<br>(1/16/96) | BCPM 3.1<br>Beldeuth-FL<br>[8/3/98] | BCPM 3.1<br>Sprint-FL<br>[8/0.98] | 8CPM 3.1<br>GTE - FL<br>(8/3/98) | HM 5.0+<br>Floride<br>(8/5/98) |
|---------------------------------------|--------------|---|-------------------------------------|-----------------------------------|----------------------------------|--------------------------------|
|                                       | 50           | 3 .   | \$ 0.01                             | 1 .                               | 1 .                              | N//                            |
|                                       | 25           | 5 .   | \$ 0.01                             | 1 .                               | 3 .                              | N/                             |
|                                       | 10           | \$ .  | \$ 0.01                             | 1 .                               | 1 .                              | N/.                            |
|                                       | 12           | 1 .   |                                     | 1 .                               | \$ .                             | N/-                            |
| Cable - Copper - Underground - 20 Geu | 4200         | 1 .   | \$ 56.31                            | \$ .                              | \$ .                             | N/                             |
| (Placing)                             | 3000         | 1 .   | \$ 31.35                            | · ·                               | 1                                | N/                             |
|                                       | 3000         |   | \$ 26.44                            | 1 .                               | \$ .                             | N/-                            |
|                                       | 2400         |   | \$ 21.40                            | 1 .                               | \$ .                             | N/-                            |
|                                       | 2100         | 1   | \$ 18.89<br>\$ 16.38                | · ·                               |                                  | N/                             |
|                                       | 1200         | 1   | 3 11.40                             |                                   | 2 .                              | P4/                            |
|                                       | 800          | 1 .   | \$ 8.76                             | 1                                 | 1 .                              | - <u>N</u>                     |
|                                       | 600          | 1 .   | \$ 5.87                             | 1 .                               | 3                                | N/<br>N/                       |
|                                       | 400          | \$ .  | \$ 3.91                             | \$ .                              | \$ .                             | N/                             |
|                                       | 300          | 1 .   | \$ 2.03                             |                                   | \$ .                             | N/                             |
|                                       | 200          | 1 .   | \$ 1.64                             | \$ .                              | \$ .                             | N/                             |
|                                       | 100          | 1 .   | \$ 0.98                             | \$ .                              | \$ .                             | N/                             |
|                                       | 60           | 1 .   | \$ 0.49                             | 1 .                               | \$ .                             | N/-                            |
|                                       | 25           | 1 .   | \$ 0.24                             |                                   | \$ .                             | N/.                            |
|                                       | 18           | 3 .   | \$ 0.24                             |                                   | 1 .                              | N/.                            |
| Cable Commen Hard                     | 12           | 1 .   | \$ 0.24                             | 1 .                               | 3 .                              | N/                             |
| Cebie - Copper - Und ground - 28 Geu  | 4200         | · ·   | \$ 8.02                             |                                   | 1 .                              | N/                             |
| (lighting)                            | 3600         | 1 .   | 1 5.11                              |                                   | 1 .                              | N/                             |
|                                       | 2400         | 1   | \$ 431                              |                                   | 1 .                              | NI/                            |
|                                       | 2100         | 1 :   | \$ 3.08                             |                                   |                                  | N/                             |
|                                       | 1800         | 1 .   | \$ 2.67                             |                                   | 1 .                              | N/                             |
|                                       | 1200         | 1 .   | \$ 1.66                             |                                   | 1 .                              | N/                             |
|                                       | 800          | 1 .   | \$ 1.43                             | 1 .                               | \$ .                             | PL/<br>PL/                     |
|                                       | 300          | 5 .   | \$ 0.08                             |                                   | 1                                | N/                             |
|                                       | 400          | 1 .   | \$ 0.64                             | \$ .                              | 5 .                              | 14/1                           |
|                                       | 300          | \$ .  | \$ 0.45                             | \$ .                              | \$ .                             | P4//                           |
|                                       | 200          | 5 .   | \$ 0.32                             |                                   | \$ .                             | N//                            |
|                                       | 100          |   | \$ 0.16                             | s .                               | \$ .                             | N/;                            |
|                                       | 50           | 1 .   | \$ 0.08                             |                                   | 3 .                              | NU                             |
|                                       | 25           |   | 5 0.04                              |                                   | 1 .                              | N//                            |
|                                       | 12           | 1 .   | \$ 0.04                             |                                   | 1                                | N//                            |
| Cable - Criper - Underground - 26 Gau | 4200         | 1   | \$ 4.07                             |                                   | 1 .                              | NU                             |
| (Engineering)                         | 3800         | 1   | \$ 3.51                             |                                   | 1                                | N//                            |
|                                       | 3000         | 5 .   | \$ 2.06                             | 5 .                               | \$ .                             | 14/1                           |
|                                       | 2400         | 1 .   | \$ 2.40                             | 5 .                               | \$ .                             | N//                            |
|                                       | 2100         | 1 .   | \$ 2.12                             | 5 .                               | 3                                | PL/4                           |
|                                       | 1800         | \$ .  | \$ 1.83                             | 5 .                               | \$ .                             | N//                            |
|                                       | 1200         | 1 .   | \$ 1.28                             | 5 -                               | \$                               | N//                            |
|                                       | 909          |   | \$ 0.98                             | s .                               | 1 .                              | N//                            |
|                                       | 600          |   | \$ 0.66                             |                                   | 1 1                              | N//                            |
|                                       | 400          |   | \$ 0.44<br>\$ 0.33                  |                                   | 2 .                              | N//                            |
|                                       | 200          |   | \$ 0.22                             |                                   | 1 :                              | N//                            |
|                                       | 100          | 1   | \$ 0.11                             |                                   | 1 .                              | N//                            |
|                                       | 60           | 8 .   | \$ 0.05                             |                                   | 1                                | N//                            |
|                                       | 25           | 5 -   | \$ 0.03                             | 5 .                               | 1 .                              | N//                            |
|                                       | 19           | \$ .  | \$ 0.03                             | s .                               | \$ .                             | N//                            |
|                                       | 12           | 1 .   | \$ 0.03                             |                                   | \$ .                             | N/J                            |
| Cable - Copper - Underground - 28 Gau | 4200         | \$ 35.60  |                                     | \$ 61.60                          | \$ 58,93                         |                                |
| (LATOT)                               | 3400         | \$ 33.30  | \$ 67.68<br>\$ 57.08                | \$ 50.61                          | \$ 50,73                         | \$ 20,00                       |
|                                       | 3000         | 8 28.21<br>8 21.50                              | \$ 46.20                            | 43.65                             |                                  | 0 23.00                        |
|                                       | 2400         | \$ 10.40  | 40.70                               | 23.52                             | \$ 20.34                         | \$ 20.0                        |
|                                       | 1800         | \$ 17.58  |                                     |                                   | 2454                             | 9 18.00                        |
|                                       | 1200         | \$ 11.65  |                                     | 20,08                             | \$ 17.28                         | 10.0                           |
|                                       | 800          | \$ 0.08   |                                     | \$ 10.51                          | \$ 12.82                         | 12.00<br>4 10.00               |
|                                       | 800          | \$ 7.52   | \$ 12.67                            | \$ 7,70                           | \$ 9.01                          | 4 7.7                          |
|                                       | 400          | \$ 9.55   | \$ 8.44                             | 5 7.69                            | \$ 5.78                          | 0.00                           |
|                                       | 300          | \$ 4.42   |                                     |                                   | \$ 4.05                          | 6 6.13                         |
|                                       | 200          | \$ 3.60   |                                     | \$ 5.08                           | \$ 3,40                          | \$ 4.21                        |
|                                       | 100          | \$ 2,65   | 1 2.11                              | \$ 3.82                           | \$ 2.10                          | 4 2.80                         |
|                                       | 25           | \$ 1.10<br>\$ 1.00                              | \$ 1.08<br>\$ 0.53                  | 3.40                              | \$ 1.58                          | + 1.4                          |
|                                       | 10           | 1.00  | 0.53                                |                                   | 1.22                             | 1.11                           |
|                                       | 12           | \$ 1.00   | \$ 0.53                             |                                   |                                  | \$ 0.83                        |
| ALL PROVIDENT                         | 200          | \$ 12.02  | \$ 8.38                             |                                   | 12.60                            | 9 0,83<br>N/A                  |
| able - Fiber - Aeriel                 | 210          | N/A   | NA                                  | N/A                               | N/A<br>10.53                     | N/A                            |
| (Material)                            | A19          |   |                                     | 181.4                             |                                  |                                |
| able - Fiber - Aeriel<br>(Meteriel)   | 144          | \$ 9.65   | \$ 4.24                             | \$ 7,82                           | 10.33                            | N/A                            |
| dos - Fiber - Aeriel<br>(Material)    | 144          | 5 7,19  |                                     | 5.96 !                            | 10.33<br>7.12                    | N/A                            |
| stor - Fiber - Annel<br>(Material)    | 144          |   | 2.93                                | 6.96                              | 5 7.12                           | N/A<br>N/A<br>N/A              |

#### Docket No. 600696-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-f) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zona  | BCP94 3.1<br>BellBouch -<br>Default<br>[1/16/90]  | BCPM 3.1<br>BellSouth-FL<br>(8/5/98)    | BOPM 3.1<br>Eprint-FL<br>(8/3/94)  | 80PM 3.1<br>GTE - FL<br>(8/3/96) | HM 8.0a<br>Florida<br>(1/3/98) |
|--|---|---|---|--|----------------------------------|--------------------------------|
|  | 36  | 1 4.67  | \$ 1.10                                 | \$ 3.70  | \$ 3.63                          | N/                             |
|  | 24  | 3 3.45  | \$ 0.68                                 | 3 3.70<br>3.22<br>3.03   | \$ 2.65                          | N/                             |
|  | 18  | \$ 5,45   | \$ 0.66                                 | \$ 3.03  | \$ 2.48                          | N/                             |
|  | 12  | \$ 3.04   | \$ 0.58                                 | \$ 2.83  | \$ 1.90                          | N/                             |
| able - Fiber - Aarial  | 280   | 3 .   | \$ 2.69                                 | 1 .  | 1 . 1                            | N/                             |
| (Supply Cost)  | 210   | N/A   | N/A                                     | N/A  | N/A                              | N/                             |
| Product Sector   | 144   | 1 .   | \$ 1.46                                 | 1 .  | \$ .                             | N                              |
|  | 00  | 1 .   | \$ 1.01                                 | \$ .   | 1 .                              | N/                             |
|  | 72  | 15 .  | \$ 0.78                                 | 1 .  | 1 .                              | N                              |
|  | 60  | 15 .  | \$ 0.65                                 | 1 .  | \$ .                             | Pd.                            |
|  | 48  | 5 .   | 3 0.54                                  | 1 .  | 1 .                              | PL/                            |
|  | 20  | 5 .   | \$ 0.58                                 | \$ .   | 5 .                              | N                              |
|  | 24  | 18 .  | \$ 0.30                                 | 1 .  |                                  | N                              |
|  | 18  | 1 .   | \$ 0.23                                 | 1 .  | 8 .                              | 24                             |
|  | 12  | \$ .  | \$ 0.20                                 |  | \$ .                             | PN/                            |
| abla - Filtrar - # arial   | 288   | 18 .  | \$ 0.50                                 |  | 1                                | N                              |
|  | 210   | NA  | NA I                                    |  | N/A                              | N.                             |
| (Tax)  | 144   | 1 .   | \$ 0.25                                 | \$   | 3 .                              | N                              |
|  | and a summer of a local strength of the second s | 11  | \$ 0.18                                 | and the second s | 1                                | N                              |
|  | 00  |   | 1 0.14                                  |  | 1                                |                                |
|  | 72  | 1   | 0.14                                    | 1 :  | 1                                | N                              |
|  | 0   | 1   | \$ 0.09                                 |  | 1                                | P6                             |
|  | 40  | 1   | 0.07                                    |  |                                  |                                |
|  | 20  | 19  |   |  |                                  | N                              |
|  | 24  | 1 .   | \$ 0.05                                 | 1 .  |                                  | N                              |
|  | 18  | 1 .   | \$ 0.04                                 | 1 .  | 1                                | N                              |
|  | 12  | 1 .   | \$ 0.03                                 | 1 .  | 1 .                              | N                              |
| oble - Fiber - Anriel  | 288   | 1   | \$ 6.12                                 |  | 1                                | N                              |
| Pleoing  | 216   | NA  | NA                                      | NA.  | NA                               | N                              |
|  | 144   | 1 .   | \$ 3.00                                 | 1 .  |                                  | N                              |
|  |   | 1 .   | \$ 2.14                                 | 1 .  | \$                               | N                              |
|  | 72  | 1 .   | \$ 1.66                                 | 1 .  | 1 .                              | N                              |
|  | 60  | 5 .   | \$ 1,58                                 | \$   | \$ · · ·                         | . N                            |
|  | 48  | 5 .   | \$ 1.15                                 | \$   | 5 .                              | N                              |
|  | 3.0   | 1 .   | \$ 0.81                                 | \$ .   | \$ .                             | N                              |
|  | 24  | 8 -   | \$ 0.64                                 | 1 .  | \$ .                             | N                              |
|  | 18  | 1 .   | \$ 0.48                                 | 5 .  | \$ .                             | N.                             |
|  | 12  | 1 .   | \$ 0.42                                 | \$ .   | \$ .                             | P4                             |
| abla - Fiber - Aarial  | 288   | 15 -  | \$ 1,09                                 | 3 .  | 1 .                              | 14                             |
| (Spiloing)   | 216   | N/A   | NA                                      | N/A  | N/A                              | N                              |
| CARLESS BO   | 144   | 5 .   | \$ 0.55                                 | \$ .   | \$ .                             | N                              |
|  | 86  |   | \$ 0.38                                 | 1 .  | \$ .                             | N                              |
|  | 72  | 15 .  | \$ 0,29                                 | \$ .   | 5 .                              | N                              |
|  | 60  | 1   | \$ 0,25                                 | \$ .   | 5 .                              | N                              |
|  | 48  | 15 .  | \$ 0.20                                 | \$ .   | \$ .                             | N                              |
|  | 30  | 8 .   | \$ 0.14                                 | 3 .  | \$ .                             | N                              |
|  | 24  | 18 .  | \$ 0.11                                 | \$ .   | \$ .                             |                                |
|  | 18  | 18 .  | \$ 0.09                                 | 3 .  | \$ .                             | N                              |
|  | 12  | 1 .   | \$ 0.08                                 | 1 .  | \$ .                             | N                              |
| abla - Fiber - Asriel  | 28-8  | 15 .  | \$ 0.73                                 | 1 .  | 3 .                              | N                              |
| Engineering  | 216   | N/A   | N/A                                     | N/A  | N/A                              | N                              |
|  | 144   | \$ .  | \$ 0.37                                 | \$ .   | 5 .                              | N                              |
|  | 00  | 1 .   | 1 0.25                                  | 1 .  | 1 .                              | N                              |
|  | 72  | 1 .   | \$ 0,20                                 | \$ .   | \$ .                             | N                              |
|  | 00  | 1 .   | \$ 0,20<br>\$ 0,16                      | 1 .  | 1 .                              | N                              |
|  | 4.0   | 18 .  | \$ 0.14                                 |  | 1 .                              | N                              |
|  | 36  | 15 .  | \$ 0.10                                 |  | \$ .                             | N                              |
|  | 24  | \$ .  | \$ 0.06                                 |  | 8 .                              | N                              |
| the second s   | 10  |   | \$ 0.06                                 | \$ .   | \$ .                             | N                              |
|  | 12  | 1 .   | \$ 0.05                                 | 1 .  | 1 .                              | N                              |
| able - Fiber - Aerial  | 280   | and the second se | \$ 18.70                                | \$ 13.00   | \$ 12.60                         | P.                             |
| LATOT  | 210   | NA  | NA                                      | NA   | NA                               | 4 13.                          |
|  | 144   |   | \$ 0.00                                 | \$ 7,62  | \$ 10.33                         | 6 0.                           |
|  | 00  | \$ 1,85   |   | \$ 5.00  | \$ 7,12                          | \$ 7.                          |
|  | 72  | \$ 6.75   |   | \$ 5.33  | \$ 5.60                          | 4 8.                           |
|  | 60  | \$ 6.02   | \$ 4.44                                 | \$ 4.68  |                                  | 4 8.                           |
|  | 48  | \$ 6.27   | 5 9.71                                  | \$ 4.15  | \$ 437                           | 9 4.                           |
|  | 38  | \$ 4.67   | 1 2.50                                  | 1 3.70   | 1 2.63                           | 4 4.                           |
|  | 24  | \$ 3.45   | \$ 2.06                                 | \$ 3.22  | \$ 2.63                          | 4 3.                           |
|  | 10  | \$ 3.26   | 1.58                                    | \$ 3.03  | \$ 2.48                          | 1 3                            |
|  | 12  | \$ 3.04   |   |  |                                  | 1 2.1                          |
| able - Fiber - Buried  | 288   | 1 12.79   |   |  | \$ 12.24                         | N                              |
| Material)  | 216   | NA  | NA                                      | NA   | NA                               | 4 13.                          |
| LINE LITER.  | 144   | 1 0.96  |   |  | \$ 9.53                          | \$ 9.                          |
|  | 80  | 1 7.43  |   | \$ 6.23  | \$ 9.53<br>\$ 5.60               | 4 7.                           |
|  | 72  | 6.00  | 1 2.52                                  | \$ 5.16  | 8 4.45                           | 1 6.                           |
| and its section of the section of th | 00  | 8 5.17  | 1 1.84                                  | \$ 4.64  | \$ 4.08                          |                                |
|  |   |   | 1.04                                    | 4.04   | 9,69                             | 4 6.1                          |
|  |   | 1 700   | 1 | 8 1 AT   | 5 5.74                           |                                |
|  | 40  | 8 4.95  | 1 H2<br>1 13                            | \$ 4.07<br>\$ 3.42   | 5 3.76<br>5 3.06<br>5 2.51       | 1 1                            |

.

Decket No. 960696-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION   | Density Zone  | BCPM 3.1<br>Balideuth -<br>Default<br>(1/16/06)  | BCPM 3.1<br>BellSouth-FL<br>JB/3/96]  | BCPM 3.1<br>Bpdet-FL<br>(8/3/98)   | BCPM 3.1<br>GTE - FL<br>(5/3/94)  | HM 8.0#<br>Florida<br>[8/3/98]  |
|---|---|--|---|--|---|---|
|   | 18  | \$ 3.25  | \$ 0.67   |  |   | 4 3.4   |
|   | 12  | \$ 2.75  | \$ 0.60   | \$ 2.66  | \$ 1.92   | 8 3,1   |
| Cable - Fiber - Buried  | 298   | 1 .  | \$ 2.71   |  | 1 .   | NJ  |
| (Supply Cost)   | 210   | N/A  | NA  | N/A  | N/A   |   |
|   | 144   | 3 .  | \$ 1.37   | 1 .  |   | N//   |
|   | 80  |  | 1 0.95  |  |   |   |
|   | 72  | 1  | \$ 0.73<br>\$ 0.61  |  |   | N6/   |
|   | 60  | 1  | 1 0.51  | 1  | 1 .   | N//   |
|   | 48  | 1 .  | 1 0.36  | 1  | 1   | N/  |
|   | 24  | 1  | \$ 0.28   | -  | 1 .   | P4//  |
|   | 10  | 1  | \$ 0.21   | 1 .  | 1 .   | NU  |
|   | 12  | 5  | \$ 0.19   | 1 .  | 1 .   | N//   |
| at Fiber - Buried   | 228   | 3 .  | \$ 0.52   | 1 .  | 13 .  | N/.   |
| (Tex)   | 210   | N/A  | NA  | N/A  | NA  | N/.   |
| 11,852  | 144   | 5 .  | \$ 0.28   | 1 .  | 5 .   | N/  |
|   | 96  | \$ .   | \$ 0.18   | \$ .   | \$ .  | N/  |
|   | 72  | 5 .  | \$ 0.14   | 1 .  | \$ .  | N/  |
| and the second second second second   | 60  | \$ .   | \$ 0.12   | 1 .  | \$ -  | N/  |
|   | 48  | \$ .   | \$ 0.10   | 1 .  | 5 -   | N/  |
|   | 36  | \$ -   | \$ 0.07   | 1 .  | 1 .   | N   |
|   | 24  | \$ .   | \$ 0.05   | 1 .  | \$ -  | N/  |
|   | 10  | \$ .   | \$ 0.04   | s .  | 1 .   | PK/   |
|   | 12  | 5 .  | \$ 0.04   | 1 .  | 1 .   | . NI  |
| able - Fiber - Buried   | 280   | 1 .  | \$ 5.96   |  | \$  | N/  |
| (Plaoing)   | 218   | NA   | N/A.  | IVA.   | N/A   | N/  |
|   | 144   | 3 .  | \$ 3.01   | 1 .  | 4 .   | NI  |
|   | 86  | \$ .   | \$ 2.08   | 1  | 1 .   | N.  |
|   | 72  | \$ .   | \$ 1.61   | 1 .  | 1 .   | N/  |
|   | 60  | \$ -   | \$ 1.34   | 1 .  | 15 .  | N/  |
|   | 48  | 1 .  | 5 1.12  | 5 -  | 15 -  | N/  |
|   | 36  | 1 .  | \$ 0.78   | 1 .  | 1 .   | N.  |
|   | 24  | \$ .   | \$ 0.62   | 1  | 1 .   | . M   |
|   | 10  | \$ -   | \$ 0.47   | ş -  | 1 .   | N   |
|   | 12  | \$ .   | \$ 0.41   | 1 .  | 1 .   | N. N.   |
| Cable - Fiber - Burled  | 268   | 1 .  | 1 .   | 1 .  | 1 .   | N   |
| (Splicing)  | 216   | NIA  | NA  | N/A  | N/A   | N   |
|   | 144   | 5 .  | 1 .   | 1 .  | 1 .   | N.  |
|   | 90  | 1 .  | 1 .   | 1 .  | 18 -  | N   |
|   | 72  | 1 .  | 1 .   | 1 .  | 1 .   | N   |
|   | 02  | 1 .  | 1 .   | 1 .  | 1   | 1 N   |
|   | 48  | 1 .  | 1 .   | 1 .  | 1 .   | N   |
|   | 3.6   | \$ .   | \$ .  | 1 .  | 1 .   | N   |
|   | 24  | 1 .  | 1 .   |  | 11 .  | N   |
|   | 18  | 5 -  | \$ .  | 1 .  | 1 .   | N   |
|   | 12  | 15 -   | 1 .   | 1 .  | 1 .   | N   |
| able - Fiber - Buried   | 283   | 15 -   | 1 1.28  | \$ .   | 1   | 14  |
| (Engineering)   | 216   | N/A  | N/A   | N/A  | N/A   | N. N.   |
|   | 144   |  | \$ 0.65   | 1 .  | 1   | N   |
|   | 90  | 1 .  | 1 0.45  | · ·  | 1 .   | N.  |
|   | 7:  | 1 .  | 3 0.35  |  | 1 .   | N.  |
|   | 60  | 11 .   | \$ 0.20   |  | 1   | N. N.   |
|   | 48  | 1  | 5 0.17  |  | 1   | N   |
|   | 30  | 1  | \$ 0.13   |  |   | N   |
|   | 24  | 1  | \$ 0.10   |  | 1   | N   |
|   | 12  | 1  | 5 0.09  |  | 1   | N   |
| Cable - Fiber - Buried  | 298   | and the second se  | \$ 19.08  |  | 18 12.24  | Pi Pi   |
| (TOTAL)   | 210   | N/A  | NA  | NA   | N/A   | 4 13.3  |
| 1.9.10M   | 144   | 5 9.98   |   | \$ 8.25  | 1 0.53  | 4 0.  |
|   | 90  | 1 7.45   | \$ 6.65   | \$ 6.23  | \$ 5.60   | 4 7.  |
| and the second se | 72  | \$ 6.00  | \$ 5.15   | \$ 5,16  | \$ 4.45   | 4 6.  |
|   | 80  | 15 6.17  | \$ 4.29   | \$ 4.64  | 18 4.06   | 6 5,1   |
|   | 4.0   | \$ 4.95  | 5 358   | \$ 4.07  | \$ 3.76   | 6 4.1   |
|   | 38  | 5 4.01   | \$ 2.51   | \$ 3.42  | 11 3.08   | 4 4   |
|   | 24  | \$ 3.93  | \$ 1.99   | \$ 3.06  | \$ 2.51   | 4 3.  |
|   | 10  | \$ 3.25  | \$ 1,50   | \$ 2.90  | \$ 2.51   | 6 3.  |
|   |   | \$ 2.75  | \$ 1.32   | \$ 2.68  | \$ 1.92   | 4 3.1   |
|   | 12  |  | 3 8.25  | \$ 15.01   | 13 11.88  | I N   |
| Cable - Fiber - Underground   | 12 288  | \$ 11.50   |   |  |   |   |
| able - Fiber - Underground  | 12 288  | 11.50<br>N/A   | N/A   | NA   |   | 9 13.   |
| Cable - Fiber - Underground   | 12  | 11.50<br>N/A   | 1 417   | N/A<br>8 0.41  | 5 10.84   | 4 13.1  |
| Cable - Fiber - Underground   | 12<br>288<br>210<br>144<br>00                               | \$ 11.50<br>N/A<br>\$ 10.50<br>\$ 7.40   | 1 417   | N/A<br>8 0.41  | 5 10.64   | 0 13.<br>0 9.<br>0 7.   |
| Cable - Fiber - Underground   | 12<br>289<br>216<br>144                                     | 1120<br>NAA<br>1050<br>740   | N/A<br>1 4.17<br>5 2.68<br>1 2.23   | N/A<br>0.41<br>7.51<br>6.55  | 5 10.64   | 6 13.<br>6 9.<br>6 7.<br>6 7.<br>6 5.   |
| Cable - Fiber - Underground   | 12<br>288<br>210<br>144<br>06<br>72<br>50                   | 8 11.50<br>NA<br>8 10.30<br>8 7.40<br>8 6.25<br>8 5.50   | N/A<br>1 4.17<br>2.68<br>1 2.23<br>1 46   | NA<br>0.41<br>7.51<br>6.55<br>6.55   | 5 10.64<br>5 6.59<br>5 4.84<br>8 4.45   | 6 13.<br>6 9.1<br>6 9.1<br>6 7.<br>6 7.<br>6 5.1<br>6 5.1<br>8 6.1  |
| Cable - Fiber - Underground   | 12<br>288<br>216<br>144<br>06<br>72<br>50<br>48             | 8 11.50<br>N/A<br>8 10.30<br>8 7.40<br>8 6.25<br>8 5.50<br>8 4.76  | N/A<br>1 4.17<br>5 2.88<br>5 2.23<br>5 1.88<br>5 1.55   | NIA<br>0.411<br>7.511<br>6.555<br>6.077<br>6.551   | 5 10.64<br>5 6.59<br>5 4.84<br>5 4.45   | 9 13.1<br>9 9.1<br>9 7.1<br>9 7.1<br>9 5.1<br>9 6.2<br>9 6.2  |
| Cable - Fiber - Underground   | 12<br>288<br>216<br>144<br>06<br>72<br>50<br>48<br>25       | 5 11.50<br>N/A<br>5 10.30<br>5 7.40<br>5 6.25<br>5 6.25<br>5 4.76<br>5 4.76<br>5 4.76  | NA<br>1 4.17<br>2.88<br>2.23<br>1.88<br>1.88<br>1.55<br>1.00  | NiA<br>0.411<br>7.511<br>6.555<br>6.607<br>6.551<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.511<br>6.5111<br>6.5111<br>6.511 6.5111<br>6.511 6.5111<br>6.511 6.511 6.51                         | 5 10.64<br>5 6.59<br>5 4.84<br>5 4.45   | 9 13.1<br>9 9.1<br>9 7.1<br>9 7.1<br>9 5.1<br>9 6.2<br>9 6.2  |
| Cable - Fiber - Underground   | 12<br>288<br>218<br>144<br>00<br>72<br>50<br>48<br>26<br>24 | 8 11.50<br>N/A<br>9 10.300<br>8 0.215<br>8 | NUA<br>\$ 4.17<br>\$ 2.68<br>\$ 2.23<br>\$ 1.66<br>\$ 1.55<br>\$ 1.00<br>\$ 0.68  | NiA<br>0,41<br>7,51<br>6,55<br>8,6,55<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,51<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,6,55<br>8,75<br>8,75<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,55<br>8,5 | 5 10.64<br>5 6.59<br>5 4.84<br>5 4.45   | 9 13.1<br>9 9.1<br>9 7.1<br>9 7.1<br>9 5.1<br>9 6.2<br>9 6.2  |
| Cable - Fiber - Underground   | 12<br>288<br>216<br>144<br>06<br>72<br>50<br>48<br>25       | 5 11.50<br>N/A<br>5 10.30<br>5 7.40<br>5 6.25<br>5 6.25<br>5 4.76<br>5 4.76<br>5 4.76  | NUA           \$         4.17           \$         2.63           \$         2.23           \$         1.55           \$         1.55           \$         1.55           \$         0.58 | HiA<br>9,41<br>9,51<br>8,55<br>8,67<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,61<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,65<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,67<br>8,7<br>8,7<br>8,7<br>8,7<br>8,7<br>8,7<br>8,7<br>8,   | 5 10.84<br>5 6.39<br>5 4.84<br>5 4.45<br>5 3.42<br>5 2.84<br>5 2.37<br>8 2.01 | 0         13.           0         7.           0         7.           0         7.           0         8.           0         4.           0         4.           0         4.           0         3. |

3,4101\_X1.8

Deckat No. 960696-TP J. W. Wells Eshibit No. \_\_\_\_(JWW-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION   | Density Zone | BCPM 3.1<br>BallSouth -<br>Default | BCPM 3.1<br>Baltouth-FL    | BCPM 3.1<br>Bprint-FL | BCPM 2.1<br>GTE + FL<br>(\$/3/98] | HM 5.0+<br>Florida |
|---|--------------|------------------------------------|----------------------------|-----------------------|-----------------------------------|--------------------|
|   |              | [1/16/98]                          | (8/3/94)                   | (8/3/94)              |                                   | [8/5/99]           |
| ervice Area Interface (SAI) - Outdoor   | 26           | \$ 407.00                          |                            | 3 405.13              | 1 738.88<br>1.011.25              | N/                 |
| (Material)  |              | \$ 407.00                          | 1 mint                     | \$ 875.40             |                                   | N//                |
|   | 100          | \$ 1,685.00                        | \$ 214.81                  | \$ 1,107.67           | \$ 1,549.28                       | N/J                |
|   | 200          | \$ 2,120.00                        | \$ 429.62                  | \$ 1,371.50           | \$ 1,742.42                       | N//                |
|   | 300          | 1 2,355.00                         | \$ 644.43                  | \$ 1,590.54           | \$ 1,035.57<br>\$ 2,874.18        | N//                |
|   | 400          | \$ 2,590.00                        | \$ 859.24                  | 5 1,794,06            |                                   | N/4                |
|   | 000          | \$ 5,509.00                        | \$ 1,264.11                | \$ 2,447.66           | \$ 3,812.00                       |                    |
|   | 600          | \$ 6,848.00                        | \$ 1,552,14                | \$ 3,361,55           | \$ 4,802.78<br>\$ 8,420.07        | N/                 |
|   | 1200         | § 7,588.00                         | \$ 1,851.65                | \$ 4,059.73           |                                   | N/                 |
|   | 1800         | \$ 8,717.00                        | \$ 2,580.35                |                       | \$ 7,739.70                       | - NO               |
|   | 2100         | \$ 11,490.00                       | \$ 3,002.55                | \$ 6,684.45           |                                   | P4/                |
|   | 2400         | \$ 11,400.00                       | \$ 3,240.26                | \$ 7,110.22           | \$ 10,057.68                      | P4/                |
|   | 3000         | \$ 11,713.00                       | \$ 4,405.95                | \$ 8,623.59           | \$ 10,056,65                      | P4/                |
|   | 3600         | \$ 14,055.60                       | \$ 5,464.75                | \$ 10,348.31          | \$ 12,043.98                      | P4/                |
|   | 4200         | \$ 18,398.20                       | \$ 6,033.10                |                       | \$ 14,051,31                      | M/                 |
|   | 8400         | NA                                 | NEA                        | NA                    | NA                                | P4/                |
|   | 7200         | NA                                 | NA                         | N/A                   | N/A                               | N/                 |
| ervice Area Into face (BAB - Outdoor  | 26           |                                    |                            |                       |                                   | N/                 |
| (Supply Cost)   | 50           |                                    |                            |                       |                                   | P6/                |
|   | 100          | \$ .                               | \$ 184.63                  | \$ .                  | 1 .                               | P6/                |
|   | 200          | 1 .                                | \$ 369.26                  | \$ .                  | · ·                               | N/                 |
|   | 300          | 1 .                                | \$ 653.69                  | \$ .                  | 1 .                               | N/                 |
|   | 400          | 1 .                                | \$ 738.52                  | 1 .                   | \$ .                              | PH/                |
|   | 600          | \$ .                               | \$ 1,103.60                | 1 .                   | 1 .                               | N/                 |
|   | 800          | 1 .                                | \$ 1,334.08                | \$ .                  | 1 .                               | N/                 |
|   | 1200         | 1 .                                | 6 4 601 40                 | \$ .                  |                                   | N                  |
|   | 1800         | 1 .                                | \$ 2,217.41                | \$ .                  |                                   | N/                 |
|   | 2100         | 1 .                                | \$ 2,217,81<br>\$ 2,580,69 | 1 .                   | 1 .                               | N                  |
| and the second se | 2400         | 1                                  | \$ 2,785.00                |                       | 1                                 | N/                 |
|   | 3000         | 1 .                                | \$ 3,786.92                | 1 .                   | 1                                 | N/                 |
|   | 3600         | 1                                  | \$ 4,600.00                | 1                     | 1 .                               | N                  |
|   | 4200         | 1 .                                | \$ 5,185.45                |                       | 1                                 | H4/                |
|   |              |                                    | . PUIDAGE                  |                       |                                   | N/                 |
|   | 5400         |                                    |                            |                       |                                   | N/                 |
| the second se   | 7200         |                                    |                            |                       |                                   | N/                 |
| ervice Area Interface (SAI) - Outdoor   | 26           |                                    |                            |                       |                                   |                    |
| (Tex)   | 60           |                                    | 4 45 80                    | -                     |                                   | N/                 |
|   | 100          | 19                                 | \$ 12.60                   | ş .                   |                                   | P4/                |
|   | 200          | 13 .                               | \$ 25.78                   | 3 .                   | 1 .                               | N/                 |
|   | 300          | 1 .                                | \$ 38.67                   | 3 ·                   | 1 .                               | P4/                |
|   | 400          | 1 .                                | \$ 61,55                   | 1 .                   |                                   | N                  |
|   | 600          | 5 -                                | \$ 7.05                    | \$ .                  | 1 .                               | N                  |
|   | 800          | 1 .                                | \$ \$3,13                  | 1 .                   | 1 .                               | N                  |
|   | 1200         | \$ .                               | \$ 111.10                  | \$ ·                  | 1 .                               | N/                 |
|   | 1800         | 1 .                                | \$ 154.82                  | 1 .                   | 5 .                               | N/                 |
|   | 2100         | 1 .                                | \$ 180.15                  | 1                     | 1 .                               |                    |
|   | 2400         | \$ .                               | \$ 194.42                  | \$ -                  | \$ .                              | P4/                |
|   | 3000         | 3 .                                | \$ 264.56                  | 5 -                   | \$ .                              | N/                 |
|   | 3000         | \$ .                               | \$ 327.80                  | 3 . "                 | \$ .                              | N                  |
|   | 4200         | 5 .                                | \$ 561.99                  | 5 -                   | \$ .                              | N.                 |
|   | 5400         |                                    |                            |                       |                                   | N                  |
|   | 7200         |                                    |                            |                       |                                   | N                  |
| ervice Area Interface (SA) - Outdoor  | 26           |                                    |                            |                       |                                   | N                  |
| (Pleong)  | 50           |                                    |                            |                       |                                   | PL.                |
| I I I I I I I I I I I I I I I I I I I   | 100          | 5 .                                | \$ 451.10                  | 1 .                   | 8 .                               | PL.                |
|   | 200          | 18 .                               | \$ 902.21                  | 1 .                   | \$ .                              | N                  |
|   | 200          | 1 .                                | \$ 1,353.31                | 1 .                   |                                   | N                  |
| the second s  | 400          | 1                                  | 1 1004.41                  | 1                     | 1 .                               | N                  |
|   | 600          | 1                                  | \$ 2,696.63                |                       |                                   | N                  |
|   |              |                                    | \$ 3,250.40                |                       | 1                                 | N                  |
|   | 800          | 1                                  | \$ 5,888.46                | 1                     |                                   | N                  |
|   | 1200         | 1                                  | \$ 5,418,73                |                       | 1                                 |                    |
|   | 1600         | 13 .                               | \$ 6,505.36                |                       |                                   | N                  |
|   | 2100         | 1 .                                |                            | · ·                   | 1 .                               | N                  |
|   | 2400         | 1                                  | \$ 6,804.54                | 1                     | 1 .                               | N                  |
| and the second  | 3000         | 1 .                                | \$ 9,252.50                |                       | 1 .                               | N                  |
|   | 3800         | 1 .                                | \$ 11,476,97               | 1 .                   | 1 .                               |                    |
|   | 4200         | 5 .                                | \$ 12,669,50               | \$ .                  | 1 .                               |                    |
|   | 6400         |                                    |                            |                       |                                   | N                  |
|   | 7200         |                                    |                            |                       |                                   |                    |
| ervice Area Interface (BAI) - Outdoor   | 26           |                                    |                            |                       |                                   | N.                 |
| (Spioing)   | 60           |                                    |                            |                       |                                   | N                  |
|   | 100          | \$ .                               | \$ 657,32                  | \$ .                  | 3 .                               | 14                 |
|   | 200          | 1 .                                | \$ 1,214.65                | 1 .                   | 1 .                               | N.                 |
|   | 300          | 1 .                                | \$ 1,071.07                | 1 .                   | \$ .                              | PA,                |
|   | 400          | 1 .                                | \$ 2,629.29                | 1 .                   | 1 .                               | N/                 |
|   | 000          | 1                                  | \$ 3,929.58                | 1 .                   | 1 .                               | N                  |
|   | 800          | 1                                  | \$ 4,749.54                | 1 .                   | 1 .                               | N/                 |
|   | 1200         | 1 .                                | \$ 5,668,04                | 1 .                   | \$ .                              | N                  |
|   |              |                                    |                            |                       | 1                                 |                    |
|   | 17.00        | 15 -                               | \$ 7,505.57                | 1.5                   |                                   | N                  |

3,0101\_328

Frage 16 of 22

Docket No. 980996-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zone | BGPM 3.1<br>BellSouth -<br>Defeult<br>{1/16/98] | BCPM 3.1<br>Belliouth FL<br>(3/2/98)   | 8CPM 3.1<br>Sprint-FL<br>(8/3/98)  | BCPM 3.1<br>GTE - FL<br>[5/3/96] | HM 8.0+<br>Florida<br>(5/2/98) |
|--|--------------|---|--|--|----------------------------------|--------------------------------|
|  | 2400         | 1 .   | \$ 9,915.19  | \$ .   | 1 .                              | N//                            |
|  | 3000         |   | \$ 13,482.22   | \$ .   | 1                                | -N//                           |
|  | 3600         | 1 .   | \$ 16,722,13   | 1 .  | \$ .                             | N.C                            |
|  | 4200         | 13 - 1  | \$ 18,461.28   | 5 .  | \$ .                             | N/                             |
|  | 5400         |   |  |  |                                  | N//                            |
| Service Area Interface (SAI) - Outdoor   | 7200         |   |  |  |                                  | N//                            |
| (Engineering)  | 80           |   |  |  |                                  | N/                             |
| 197.961117.194   | 100          | 3 .   | \$ 94.93   | 1 .  | 1 .                              | N/<br>N/                       |
|  | 200          | 15 .  | \$ 159.65  | \$ .   |                                  | N/                             |
|  | 300          | 1 .   | \$ 284.78  |  | 1                                | N4/                            |
|  | 400          | 18 - 1  | \$ 379.70  |  | 1 .                              | N/                             |
|  | 600          | 1 .   | \$ 567,45  | \$ .   | 1 .                              | N/                             |
|  | 009          | 1 .   | \$ 685.89  | \$ -   | 1 .                              | N/                             |
|  | 1200         | \$ .  | \$ 618.24  | 5 .  | 1 .                              | N/                             |
|  | 1800         | 13 . 1  | \$ 1,140.26  | \$ .   | 1 .                              | H/                             |
|  | 2100         | 13 .  | \$ 1,326.83  | 5 ·  | 1 .                              | N(                             |
|  | 2400         | 1   | 1,431,87   | <u>.</u>   |                                  |                                |
|  | 3000         | 1   | \$ 1,040.90<br>\$ 2,414.87   |  | 1 .                              | N/                             |
|  | 4200         | 1   | \$ 2,666.03  |  | 1 .                              | N/4                            |
|  | 5400         | 3 .   | 1,000,03   | s .  | ş .                              | N/                             |
|  | 7200         |   |  |  |                                  | N/                             |
| Service Area Interface (SAII - Outdoor   | 28           |   |  |  |                                  | N/                             |
| (TOTAL)  | 80           |   |  |  |                                  | 4 250.0                        |
|  | 100          | \$ 1,885.00                                     | \$ 1,615.60  | \$ 1,197.67  | \$ 1,549.28                      | 4 350.0                        |
|  | 200          | \$ 2,120.00                                     | \$ 3,231.36  | \$ 1,371.50  | 1 1,742.42                       | 4 600.0                        |
|  | 300          | \$ 2,355.00                                     | \$ 4,647.05  | \$ 1,590.54  | \$ 1,935.57                      | N/                             |
|  | 400          | \$ 2,590.00                                     | \$ 6,402.72  | \$ 1,794.00  | \$ 2,674.16                      | \$ 1,000,0                     |
|  | 600          | \$ 5,509.00                                     | \$ .0,658.30   |  | \$ 3,812.00                      | \$ 1,400.0                     |
|  | 800          | \$ 6,648.00                                     | \$ 11,674.24   | 3,361.55   | \$ 4,892.78                      | \$ 1,900.0                     |
|  | 1200         | \$ 7,586.00                                     | \$ 13,026.00   |  | \$ 5,420.07                      | \$ 2,400.0                     |
| and the second s | 1800         | \$ 8,717.00                                     | \$ 19,407,84   |  | \$ 7,739.70                      | \$ 3,400.0                     |
|  | 2100         | 11,490.00                                       | 22,583.50  | \$ 6,684.45  | \$ 10,057.68                     | N/1                            |
|  | 2400         | 11,490.00                                       | \$ 24,371,28   | \$ 7,110.22  | 3 10,057,68                      | \$ 4,300.0                     |
|  | 3000         | \$ 11,713.00                                    | 33,138,93  | \$ 8,623.50  | \$ 10,036.65                     | N                              |
|  | 3600         | \$ 10,398,20                                    | 41,102.57  | 10,348,31<br>12,073,03   | \$ 12,043.08                     | \$ 6,000.0                     |
|  | 6400         | 10,300.20                                       | 9 45,311,34  | \$ 12,073.03   | \$ 14,051.31                     | N/                             |
|  | 7200         |   |  |  |                                  | 6 8,200.0                      |
| Service Area Interface (SAI) - Indoor  | 26           | \$ 340.00                                       |  | \$ 509,53  | \$ 340.00                        | \$ 10,000,0<br>N/              |
| (Meterial)   | 50           | 3 509.43  |  | \$ 751.63  | \$ 509.43                        | N//                            |
| Includes oper of protection)   | 100          | \$ 811.60                                       | \$ 325.92  | \$ 1,102.64  | \$ 611.60                        | N/4                            |
|  | 200          | \$ 1,293.00                                     | 651.85   | 1 1 979 68   | \$ 1,293.00                      | N//                            |
|  | 300          | 3 1,965.71                                      | \$ 977.77  | \$ 2,781.51  | \$ 1,065.71                      | N/I                            |
|  | 400          | \$ 2,324.03                                     | \$ 1,303.70  | \$ 3,733,75  | \$ 2,324.03                      | N//                            |
|  | 600          | \$ 3,757.00                                     | 1,955.55   | \$ 5,412.6*  |                                  | 34/                            |
|  | 800          | \$ 4,901.56                                     | 2,033.32   | \$ 8,043,74  | \$ 4,901,36                      | N//                            |
|  | 1200         | \$ 6,867,06                                     | \$ 3,911,00  | \$ 10,825.25   | \$ 6,667.08                      | N//                            |
|  | 1800         | \$ 8,658.56                                     | 5 5,505.84   | \$ 13,456.37   | \$ 8,658.36                      | N//                            |
|  | 2100         | \$ 11,005.80<br>\$ 13,559.71                    | 6,644,41   | \$ 18,087,16   | \$ 11,095.80                     | N/-                            |
|  | 2400         | \$ 16,669,77                                    | 0.777.73   |  |                                  | NA                             |
|  | 3800         | \$ 19,605.42                                    |  |  | \$ 19,505.42                     |                                |
|  | 4200         | \$ 23,582.42                                    | 13,668,82  | \$ 37,587.59   | 23,362.42                        | N/                             |
|  | 5400         | 1 ATTORNE                                       | 19,000.04  | ar per an  | A ARADE AL                       | N/                             |
|  | 7200         |   | A REAL PROPERTY OF A REAL PROPER |  | 1                                | N/                             |
| Service Area Interface (CAl) - Indoor  | 28           |   |  |  |                                  | N/                             |
| (Supply Cost)  | 50           |   |  |  |                                  | N/r                            |
|  | 100          | 5 - 1   | \$ 400.50  | \$ .   | 1 .                              | N/                             |
|  | 200          | 18 . 1  | \$ 800.89  | 5 .  | 1 .                              | N//                            |
|  | 300          | 1 . 1   | \$ 1,201.43  | \$ .   | 1 .                              | No                             |
|  | 400          | s   | 1,601.98   | \$ .   | 1 .                              | N/                             |
|  | 600          | 1 .   | 2,402.97   |  | 1 .                              |                                |
|  | 800          | 1   | 3,604,46   | the state of the s | · ·                              | N//                            |
|  | 1200         |   | 4,805.95   |  |                                  | N//                            |
| the second s   | 1800         |   | 8,410,41   |  |                                  | N//                            |
|  | 2400         |   | 9,611,80   |  |                                  | N//                            |
|  | 3000         | 1   | 12,014.87  |  | 1                                | N//                            |
|  | 3000         | 1   | 14,417,84  |  |                                  | N/I                            |
|  | 4200         | 1   | 16,620,62  |  | 1 .                              | N//                            |
|  | \$400        |   | Constant and a second  |  |                                  | N/                             |
|  | 7200         |   |  |  |                                  | N//                            |
| Service Area Interface (SAB - Indoor   | 25           |   |  |  |                                  | N//                            |
| (Tes)  | 60           |   |  |  |                                  | N/J                            |
|  | 100          | 18 - 1  | 10.58  | 5 -  | 1 .                              | N//                            |
|  | 200          | 1 . 1   | 539.11<br>53.87  | s .  | \$                               |                                |
|  | 300          | 1   |  | 5  | 1 .                              | N//                            |

Dockst No. 900653-TP J. W. Wells Exhibit No. \_\_\_\_ (XWW-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zone         | BCPM 3.1<br>Belliouth -<br>Default<br>(1/16/98) | BCPM 3.1<br>BallSouth FL<br>(8/3/88) | BCPM 3.1<br>Byrins FL<br>(8/3/96) | 6CPM 3.1<br>GTE - FL<br>[8/3/98] | HM 0.0+<br>Fioride<br>(8/2/90) |
|--|----------------------|---|--------------------------------------|-----------------------------------|----------------------------------|--------------------------------|
|  | 7200                 | (interest)                                      |                                      |                                   |                                  | 4 9,656.0                      |
| Drop Terminal Cost - Aerial  | per Line             | NA  | NA                                   | NA                                | N/A                              | 4 32.0                         |
| (Material)   | 6                    | \$ 05.98  | 5 .                                  | \$ 150.32                         | \$ 95.68                         | N                              |
|  | 12                   | \$ 131.81                                       | 1 . 1                                | \$ 180.16                         | \$ 131.01                        | N                              |
|  | 25                   | \$ 216.00                                       | 1 .                                  | \$ 282.99                         |                                  |                                |
| Drop Terminal Cost - Aerial  | per Line             |   |                                      | 1 AV8.00                          | 10.00                            | N                              |
| (Supply Cost)  | 0                    | 3 .   | 1                                    | 1                                 | 1                                |                                |
| Toobday coard  | 12                   | 1 .   | 1                                    |                                   | 3 .                              | N                              |
|  |                      |   | 1 .                                  | 5 · ·                             |                                  | N                              |
| Prop Terminel Cost - Aerial  | 25                   | 3 .   | \$ .                                 | 1 .                               | \$ .                             | N                              |
|  | per Line             | 5 .   |                                      |                                   |                                  | N/                             |
| (Tex)  | 0                    |   | 3 .                                  | 2                                 |                                  | N                              |
|  | 12                   | \$ .  | 3 ·                                  | 1                                 |                                  | N/                             |
|  | 25                   | 1 .   | 3 · · ·                              | ş .                               | 1 .                              | N.                             |
| Prop Terminal Cost - Aerial  | per Line             |   |                                      |                                   |                                  | N. N.                          |
| Placing  | 0                    | 3 .   | 3                                    |                                   | \$ .                             | N.                             |
|  | 12                   | 3 .   | 1 .                                  | 1 .                               | 1 .                              | PK.                            |
|  | 25                   | \$ .  | 1 .                                  | 1 .                               | \$ .                             | N.                             |
| Prop Terminal Cort - Aerial  | per Line             |   |                                      |                                   |                                  | N                              |
| (Spiloty)  |                      | 3 .   | \$ .                                 | 1 .                               | \$                               | N.                             |
|  | 12                   | \$ .  | \$ .                                 | \$ .                              | \$ .                             | N                              |
|  | 25                   | 1 .   | \$ .                                 | 3 .                               | \$ .                             | N.                             |
| Prop Terminal Cost - Aerial  | per Line             |   |                                      |                                   |                                  | N,                             |
| Ingineering  | 0                    | 5 .   | \$ .                                 | 1 .                               | \$ .                             | N                              |
|  | 12                   | \$ .  | \$ .                                 | 1 .                               | 1 .                              | N                              |
|  | 25                   | \$ .  | \$ .+                                | 1 .                               | \$ .                             | N                              |
| Prop Terminal Cost - Aeriel  | per Line             |   |                                      |                                   |                                  | 0 32.0                         |
| LATOT  | 0                    | \$ 95.96  | 1 .                                  | \$ 150.32                         | \$ 95.98                         | N N                            |
| A1.5.1.58.   | 12                   | \$ 131.81                                       | 1                                    | \$ 180.18                         | \$ 131.61                        | N                              |
|  | 18                   | \$ 216.00                                       | 1                                    | \$ 282.00                         |                                  |                                |
| Drop Terminal Cost - Buriad  | in the second second | # 619.99  |                                      | * 202.0V                          | 8 210.00                         |                                |
| (Matarial)   | per Line             | \$ 157.05                                       |                                      | 1 117.15                          | A 189.00                         | N                              |
| (Matar)al)   | 0                    | \$ 440.87                                       |                                      | \$ 117.10                         | \$ 157.05                        | N/                             |
| and the second statement of th | 12                   |   | 1 .                                  | \$ 145.29                         |                                  | N                              |
|  | 25                   | \$ 451.00                                       | 1 .                                  | \$ 210.76                         | \$ 451.00                        | N/                             |
| Prop Terminal Cost - Buried  | per Line             |   |                                      |                                   |                                  | N.                             |
| (Supply Cost)  | 0                    | \$ .  | 1 .                                  | 5 · · ·                           | 1 .                              | N                              |
|  | 12                   | \$ .  | \$ .                                 | 1 .                               | 1 .                              | N                              |
| the second se  | 25                   | 1 .   | \$ .                                 | 1 .                               | 1 -                              | N.                             |
| Drop Terminal Cost - Buried  | per Line             |   |                                      |                                   |                                  | N.                             |
| (T ex)   | 0                    | \$ .  | 1 .                                  | 1 .                               | \$ .                             | N.                             |
|  | 12                   | \$ .  | \$ .                                 | 1 .                               | \$ .                             | NU.                            |
|  | 25                   | 5 -   | \$ .                                 | 1 .                               | \$ .                             | N                              |
| Prop Terminal Cost - Buried  | per Line             |   |                                      |                                   |                                  | N.                             |
| (Placing)  | 6                    | 1 .   | 5 .                                  | 1 .                               | \$ .                             | N                              |
|  | 12                   | \$ .  | 1 .                                  | 1 .                               | 1 .                              | N                              |
|  | 25                   | \$ .  | \$ .                                 | 1 .                               | 1 .                              | N                              |
| Drop Terminal Cost - Burlad  | per Line             |   |                                      |                                   |                                  | N                              |
| (Spling)   | 0                    | 1 .   | 1 .                                  | 1 .                               | 3 .                              | N                              |
| 10000000   | 12                   | \$ .  | 1 .                                  | 1                                 | 1                                | N                              |
|  | 25                   | \$ .  |                                      | -                                 |                                  |                                |
| Prop Terminal Cost - Buried  | perline              |   |                                      |                                   | 3 .                              | N                              |
| (Engineering   | Per Liver            | 4   |                                      |                                   |                                  | N                              |
| The Party of the second s   | 12                   | 1   | 1                                    |                                   | 1 .                              | N.                             |
|  | 14                   |   |                                      |                                   | 1 .                              | N/                             |
| Prop Terminal Cost - Burley  | and the              |   |                                      |                                   | 1                                | N                              |
| (TOTAL)  | per Line             | \$ 157.05                                       |                                      | 1 11V 12                          | 1 199.00                         | 4 42.8                         |
| 11511764   | 0                    | \$ 440.87                                       |                                      | \$ 117,10                         |                                  | Pl/                            |
|  | 12                   |   |                                      | \$ 145.29                         |                                  | N                              |
|  | 25                   | \$ 451.00                                       | ş .                                  | \$ 219,76                         | \$ 451.00                        | \$ 170.0                       |
| Cont. And down Front Ball  | -                    |   |                                      |                                   |                                  |                                |
| Prop Cost - Asriel per Foot (2 Pair)   | 00000 - 00005        |   |                                      | \$ 0.50                           |                                  | 0,1                            |
| Material   | 00005 - 00100        |   | 1 0.07                               | 64.0                              |                                  | 0.1                            |
|  | 00100 . 00200        |   | \$ 0.07                              | 5 0.60                            |                                  | # 0,1                          |
|  | 00200 - 00650        |   | \$ 0.07                              | \$ 0.80                           |                                  | 0.1                            |
|  | 00850 - 00850        |   |                                      |                                   |                                  | ¢ 0,1                          |
|  | 00850 - 02550        |   | \$ 0.07                              | 0.60                              |                                  | \$ 0,1                         |
|  | 02550 - 05000        |   | \$ 0.07                              | \$ 0.60                           |                                  | ¢ 0,1                          |
|  | 01000 - 10000        |   | \$ 0.07                              | \$ 0.60                           |                                  | 0,1                            |
|  | 10000 +              | \$ 0.77   | \$ 0.07                              | \$ 0,50                           | \$ 0.62                          | 4 0,1                          |
| rop Cost - Aerial per Foot (2 Pair)  | 00000 - 00005        |   | \$ ·                                 |                                   | 5 .                              | N/                             |
| (Supply Cost)  | 00005 - 00100        |   | 1 .                                  | \$ .                              | \$ .                             | N/                             |
|  | 00100 - 00200        |   | 1 .                                  | \$ .                              | \$ .                             | N/                             |
|  | 00200 - 00850        |   | 1 .                                  | \$ .                              | \$ .                             | 14/                            |
|  | 00650 - 00850        |   | 1 .                                  | 1 .                               | \$ .                             | N                              |
| and the second sec   | 00850 - 02550        |   | \$ .                                 | 1 .                               | \$ .                             | N/                             |
|  | 02550 - 08000        | 1 .   | \$ .                                 | \$ .                              |                                  |                                |
|  | 0\$600 - 10000       | \$ .  | \$ .                                 | 1 .                               | \$ .                             | N                              |
|  | 10000 +              | 1 .   | 8 .                                  | \$ .                              | \$ .                             | NI                             |
| rop Cost - Aarial per Foot (2 Pair)  | 00000 - 00005        | \$ .  | 1 .                                  |                                   | \$                               | N/                             |
| (Tex)  | 00005 - 00100        |   |                                      |                                   |                                  |                                |

3,0101,328

#### Docket No. 950696-TP J. W. Wells Exhibit No. \_\_\_\_ (AWW-6) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zona                   | BCPM 3.1<br>BellSouth -<br>Defedt<br>(1/16/98)   | BCPM 3.1<br>BeliSouth-FL<br>[8/3/96] | BCPM 3.1<br>Sprint-FL<br>(8/3/98)  | 8CPM 2.1<br>GTE - FL<br>[8/3/98] | HM 6.0+<br>Florida<br>(8/3/96) |
|--|--------------------------------|--|--------------------------------------|--|----------------------------------|--------------------------------|
|  | 00100 - 00200                  | 5 -  | 1 .                                  | 5 .  | \$ .                             | PL/.                           |
|  | 00200 - 00650                  | 1 .  | s .                                  | \$ .   | 1 .                              | N//                            |
|  | 00850 - 00850                  | \$ .   |                                      | \$ .   | 1 · · ·                          | 967                            |
|  | 00850 - 02550                  | 1 .  |                                      | 1 .  | ş .                              | N//                            |
|  | 02550 - 05000                  | 1 .  |                                      | 1  | 1                                | P4//                           |
|  | 06000 - 10000                  | 1 · · ·  |                                      |  |                                  | N//                            |
| Drop Cost - Aerial per Foot 12 Pairl   | 10000 +                        | 1 1  | 5 0.19                               | 1 1  | 1 .                              | N/-                            |
| (Placing)  | 00005 - 00100                  | 1  | 0.19                                 | 1  | 1 .                              | 0.1                            |
| 1. Monda   | 00100 - 00200                  | 1 .  | 1010                                 |  | 1 .                              | . 0.1                          |
|  | 00200 - 00650                  | 1 .  | \$ 0.19                              | 1 . 1  | 1 .                              | 6 C 1                          |
|  | 00850 - 00850                  | 1 .  | \$ 0.19                              | \$ .   | \$ .                             | . 0.2                          |
|  | 00850 - 02550                  | \$ .   | \$ 0.19                              | \$ .   | \$ .                             | 4 0.2                          |
|  | 02550 - 05000                  | 1 .  | \$ 0.19                              | 1 .  | 1 .                              | 0.2                            |
|  | 05000 - 10000                  | 1 .  | \$ 0.19                              | 1 .  | \$ .                             | 4 0.2                          |
|  | 10000 +                        | 1 .  | \$ 0.19                              | 1  | 1 .                              | 0.2                            |
| Drop Cost - Aerial per Fout (2 Pair)   | 00000 - 00005                  | 5 .  | \$ · ·                               |  | 1                                | N//                            |
| (Bplining)   | 00005 - 00100                  | 1 .  | s                                    | ş .  | 1 .                              | N/-                            |
|  | 00100 - 00200                  | \$ .   | \$ .                                 | 1 .  | \$ .                             | P4//                           |
|  | 00200 - 00650                  | 1 .  | · ·                                  |  | 1                                | N//                            |
|  | 00850 - 00850                  |  |                                      |  | 1 .                              | N//                            |
|  | 02550 - 02550                  |  |                                      |  | 1 :                              | N//                            |
|  | 05000 - 10000                  | 1 .  |                                      | 1 .  | 1                                | N/                             |
|  | 10000 +                        | 1 .  | 1                                    |  | 1                                | N/                             |
| Drop Cost - Aerial per Foot (2 Pair)   | 00000 - 00005                  | 1 .  | 1                                    | 1  | 1                                | N/                             |
| (Engineering)  | 10005 - 00100                  | 1 .  | \$ .                                 |  | 1                                | N/                             |
| the second se  | 00100 - 00200                  | 1 .  | 5 .                                  | 1 .  | \$ .                             | N//                            |
|  | 00200 - 00650                  | 1 .  | \$ .                                 | \$ .   | 1 .                              | N/                             |
|  | 00850 - 00850                  | 1 .  | 5 .                                  | 1 .  | \$                               | NU                             |
|  | 00850 - 02550                  | 1 .  | \$ -                                 | 1 .  | \$ ·                             | N/                             |
|  | 02550 - 05000                  | \$ .   | 1 ·                                  | \$ .   | ¥                                | N/                             |
|  | 05000 - 10000                  | 1 .  | s .                                  |  | 1 .                              |                                |
|  | 10000 +                        |  |                                      | 1  |                                  | N/.                            |
| Dron Coet - Aerial par Foot (2 Pair)   | 00000 - 00005                  |  | 1 0.26                               | 5 0.80   | 0.62                             | 0.2                            |
| LIATUT)  | 00005 - 00100                  | \$ 0.77  | \$ 0.26                              | 0.60   | 0.82                             | 0.2                            |
|  | 00200 - 00650                  | 8 0.77   | \$ 0.26                              | 0.50   | \$ 0.62                          | 0.2                            |
|  | 00650 - 00850                  | 8 0.77   | 1 026                                | 5 0.80   | 1 0.62                           | 4 0.3                          |
|  | 00850 - 02550                  | \$ 0.77  | \$ 0.26                              | \$ 0.60  | \$ 0.62                          | 4 0.3                          |
|  | 02550 - 05000                  | \$ 0.77  | \$ 0.26                              | \$ 0.80  | \$ 0.82                          | 0.3                            |
|  | 05000 - 10000                  | \$ 0.77  | \$ 0.26                              | \$ 0.80  | \$ 0.62                          | \$ 0.3                         |
|  | 10000 +                        | \$ 0.77  | \$ 0.28                              | \$ 0.80  | \$ 0.62                          | \$ 0.3                         |
| Drop Cost - Buried per Foot (3 / 8 Pair)   | 00000 - 00005                  |  | \$ 0.12                              |  |                                  | 4 0.1                          |
| (Metarial)   | 00005 - 00100                  | \$ 0.77  | \$ 0.12                              | \$ 0.74  |                                  | 1 0,1                          |
|  | 00100 - 00200                  | \$ 0.77  | \$ 0.12                              | \$ 0.74  |                                  | 0.1                            |
|  | 00200 - 00650                  | \$ 0.77  | \$ 0.12                              | \$ 0.74  | \$ 0.62                          | 0,1                            |
|  | 00850 - 00850                  | 1 0.77<br>5 0.77   | 1 0,12<br>5 0,12                     | \$ 0.74  |                                  | 0,1                            |
|  | 02550 - 02550                  | \$ 0.77  | 0.12                                 | \$ 0.74  |                                  | 0,1                            |
|  | 05000 - 10000                  | 0.77   | 8 0.12                               | 0.74   |                                  | 0.1                            |
| a second s  | 10000 +                        | \$ 0.77  | \$ 0.12                              | 8 0.74   |                                  |                                |
| Drop Cost - Buried per Foot (3 / 6 Pair)   |                                | and a summer of the local division of the lo | 1 .                                  | 1 .  | 1                                | NU                             |
| (Supply Covt)  | 00008 - 00100                  |  | 1 .                                  | 1 .  | 1 .                              | NJ.                            |
|  | 00100 - 00200                  | \$ .   | \$ .                                 | \$ ·   | \$ .                             | N/                             |
|  | 00200 - 00650                  |  | 1 .                                  | 1 .  | \$ ·                             | N/                             |
|  | 00850 - 00850                  |  |                                      | 1 .  | 1 .                              | N/                             |
|  | 00850 - 02550                  |  |                                      |  |                                  | N/                             |
|  | 02550 - 05000                  |  |                                      | 1 .  | · ·                              | N/                             |
|  | 05000 - 10000                  |  | · · ·                                |  |                                  | N/                             |
| Drop Cost - Buried par Foot (3 / 8 Pair)   | 10000 +<br>00000 · 00005       |  |                                      |  |                                  | N/<br>N/                       |
| (Text)   | 00005 - 00100                  |  |                                      |  |                                  | P6/<br>P1/                     |
|  | 00100 - 00200                  |  | 1 .                                  | -  | 1                                | N/                             |
|  | 00200 - 00650                  |  | 1                                    |  |                                  | N/                             |
|  | 00850 - 00850                  |  | 1 .                                  | \$ .   | \$ .                             | N/                             |
|  | 00850 - 02550                  |  | 1 .                                  | \$ .   | \$ .                             | M/                             |
|  | 02550 - 05000                  | and a summary of the second  | 1 .                                  | ş .  | ş .                              | N/                             |
|  | 05000 - 10000                  | 1 .  | ş .                                  | \$ ·   |                                  | .N/                            |
|  | 10000 +                        | \$ .   | 1                                    | 1 .  | 1 .                              | N/                             |
| Drop Cost - Buried per Foot (3 / 6 Pair)   |                                |  | \$ 0.58                              |  | · ·                              | 0.0                            |
| (Plecing)  | 00005 - 00100                  |  | \$ 0.58                              | 1 .  |                                  | 0.0                            |
|  | 00100 - 00200                  |  | \$ 0.58                              |  | 1                                | 4 0,0                          |
|  | 00200 - 00550<br>00650 - 00850 |  | 0.56                                 |  |                                  | 4 0.0                          |
| and the second sec | 00850 - 02550                  |  | 0.58                                 |  | 1                                | 0.0                            |
|  | 02550 - / 5000                 |  | 8 0.58                               | -  | 1                                | 4 0.7                          |
|  | 05000 - 10000                  |  | \$ 0.58                              | - Arrest and a second sec |                                  | 4 1.6                          |
|  |                                |  |                                      |  |                                  |                                |

Docket No. 980696-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comperisons

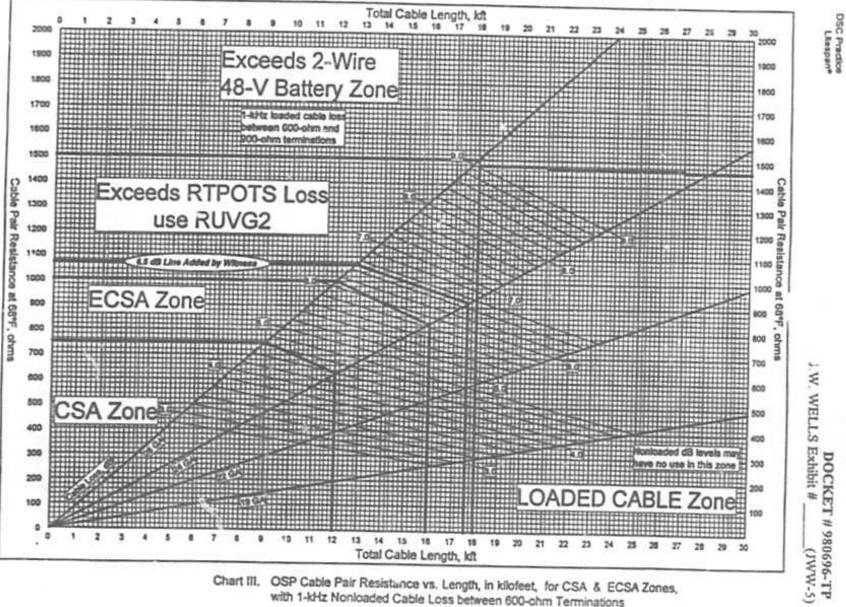
|  | 1                              | BCPM 3.1   | BOPM 3.1   | RCPM 2.1   | BCPM 2.1               | HM S.C.     |
|--|--------------------------------|--|--|--|------------------------|-------------|
| INPUT VALUE DESCRIPTION  | Density Zeese                  | BallSouth -<br>Default   | Bellieuth-FL   | Spolet FL  | GTE . FL               | Fiorida     |
|  |                                | [1/16/98]  | (a/3/94)   | 18/2/941   | [8/3/98]               | [8/3/96]    |
| Drop Cost - Buried per Foot (3 / 6 Pair)   | 00000 - 00005                  | \$ .   | 3 . ]  | 1 . ]  | 1 .                    | N           |
| (Splining)   | 00005 - 00100                  | \$ .   | \$   | \$   | 5 .                    | N.          |
|  | 00100 - 00200                  | 3 .  | 3 .  | 5 .  | 1 .                    | N           |
|  | 00200-00#50                    |  | s .  | 3 .  | 1 .                    | N           |
| the second se  | 00650 - 00850                  | 2  |  |  |                        | N.          |
|  | 00850 - 02550<br>02550 - 05000 | 2  |  |  |                        | N           |
|  | 05000 - 10000                  | 1 :  | :  | 3 .  | 1 .                    |             |
|  | 10000 +                        | 1  |  | 1  | 1                      | N           |
| Drop Cost · Buried per Foot 13 / 6 Pairl   | 00000 - 00006                  | 1  |  | 1  | 1                      | N           |
| (Engineering)  | 00005 - 00100                  | 1 .  |  |  |                        | N           |
| The second se  | 00100 - 00200                  |  | 1  | 1  | 1                      | N           |
|  | 00200 - 00680                  | 5 .  | 5 .  | 8 . 1  | 1 .                    | N           |
|  | 00650 - 00850                  | \$ .   | \$ .   | \$ .   | 1 .                    | N.          |
|  | 00850 - 02550                  | \$ .   | 5 .  | \$ .   | \$ .                   | N           |
|  | 02550 - 05000                  | \$ .   | 5 .  | \$ .   | 1 .                    | N           |
|  | 05000 - 10000                  | \$ .   | \$ .   | \$ · ·   | \$ .                   | N           |
| and the second se  | 10000 +                        | \$ .   | 1 .  | 1 .  | 1 .                    | N           |
| Drop Cent - Buried per Foot (3 / 6 Pair)   |                                | \$ 0.77  | \$ 0.70  | \$ 0.74  | \$ 0.62                | 4 0.3       |
| (ATOT)   | 00005-00100                    | 1 0.77   | \$ 0.70  | \$ 0.74  | \$ 0.62                | \$ 0.7      |
| and the second se  | 00100 - 00200                  | 5 0.77   | \$ 0.70  | \$ 0.74  | \$ 0.62                | \$ 0.3      |
|  | 00200 - 00850                  | \$ 0.77  | \$ 0.70  | 3 074  | \$ 0.62                | 0.          |
|  | 00650 - 00850                  | \$ 0.77  | \$ 0.70  | \$ 0.74  | \$ 0.62                | 0,          |
|  | 00850 - 02550                  | \$ 0.77<br>\$ 0.77   | \$ 0.70  | 0.74   | 1 0.62                 | . 0,1       |
|  | 02550 - 05000                  | 3 0.77   | \$ 0.70  | 0.74   | \$ 0.82                | 0.          |
|  | 05000 - 10000                  | 1 0.77   | 0.70   | and the second s | 5 0.62                 | 1 14        |
| Harman Landoux Frankes (Miller)  | 10000 +                        | the second s | Concession of the local division of the loca | and the second se  | \$ 0.62                | 4 6.1       |
| Network Interface Device (NID)<br>(Material  | Residential                    | 5 50.75  | \$ 7.80  | \$ 58.95   | \$ 29.40               | 4 10.0      |
| The loss states and the second s | Dusinese                       | \$ 30.73   | and the second se  | \$ 99.55   | \$ 29.45               | 4 25.0      |
| Protectar  | Residential                    | 3  | \$ 3.56  |  | · · · ·                | 4 4.0       |
| (Material  | Buelvese                       | \$ ·   |  | 5 .  | 1 .                    | \$ 4.5      |
| Interface  | Residential                    | \$ .   | \$ 4.89  | 5 ·  |                        | N           |
| C laterial   | Bueinees                       |  | 1 4.89   | 1 .  |                        | N           |
| Network Interface Device (NID)   | Residential                    | \$ .   |  | \$ .   | 1 .                    | N           |
| (Supply Cest)  | Business                       | \$ .   | 1 .  | 5 .  | 1 .                    | N           |
| Protector  | Residential                    | \$ .   | s  | \$ -   | \$ .                   | N           |
| (Bupply Cent)  | Business                       | 3 -  | 1 .  | 5 .  | 1 .                    | N           |
| Interface  | Residential                    | \$ .   | \$ .   | ş .  | 1 .                    | N.          |
| (Bupply Cost)  | Business                       |  | 1 .  |  | 1 .                    | N           |
| Network Interface Device (NID)   | Residential                    | \$   | 1 .  | • •  | 1 .                    | N           |
| (Tax   | Business                       | \$   | 1 .  | \$ .   | 1 .                    | N           |
| Protector  | Residential                    | \$   | 1 · ·  | 1 .  | 1 .                    | N.          |
| (Tex   | Bueinees                       | \$ .   | 1 .  | 1 .  | 1 .                    |             |
| interface  | Residential                    | 5 .  | 5 .  | 5 -  | 1 .                    | N           |
| (Tex   | Bueiness                       | 1 .  | 1 .  | 1 .  | 1 .                    | N           |
| Network Interface Device (NID)   | Residential                    | \$   | \$ 24.26   | 5 .  | 1 .                    | 6 15.0      |
| (Pleoing)  | Business                       | 1 .  | \$ 24.26   | 1 .  | 1 .                    | 1 15.0      |
| Protector  | Residential                    | 1 .  | \$ 8.15  | \$   | 1 .                    | N           |
| (Placing)  | Business                       | \$ .   | \$ 8.15  | \$ .   | \$ .                   | 14          |
| interfeos  | Providential                   | \$ .   | \$ 8.15  | 5 · ·  | 1 .                    |             |
| Plesiogl   | Business                       | 1 .  | \$ 0.15  | 1 .  | 1 .                    | N           |
| Network Interlace Device (NID)   | Residential                    | \$ -   | 1 .  | 1 .  | \$ ·                   | N.          |
| (Seleina)  | Businese                       | \$ .   | 1 .  | 1 -  | 1 .                    | N           |
| Protector  | Residential                    | 1 .  | \$ .   | \$ .   | \$ .                   | N/          |
| (Belieing)   | Business                       | 1 .  | \$ .   | 1 .  | 1 .                    | N           |
| nterfese   | Revidential                    |  |  | 5 -  | \$ .                   | N           |
| (Seleina)  | Bureinzen                      | 1 .  | 1 ·  | 1 .  | 1 .                    | N           |
| Network Interfese Device (NID)   | Residential                    | 1 .  | 1 .  | \$ .   | 1 .                    | N.          |
| (Ingineering)  | Businees                       | 1 .  | 1 .  | 1 .  | 1 .                    | N           |
| Protector  | Residential                    | 1  | ۱ ·  | 1 .  | ۱ ·                    | N           |
| (Engineering   | Business                       | \$ .   | 1 .  | 1 .  | 1 .                    | N           |
| nterfece   | Residential                    | \$ .   | \$ .   | 1 .  | \$ ·                   | N.          |
| Engineering  | Buninese                       | 1 .  | 1 .  | 1 .  | 1 .                    | N.          |
| Network Interface Davice (NID)   | Residential                    | 1 .  | \$ 32.06   | 1 .  | \$ ·                   | 4 25.0      |
| Total)   | Businese                       | \$ .   | \$ 32.08   | 1 .  | \$ -                   | 40.0        |
| Protector  | Residential                    | 1 .  | \$ 11.D1   |  | \$ .                   | 4 4.0       |
| (र ल म)  | Bueinees                       | 1 .  | \$ 11.51   |  | 1 .                    | 4.0         |
| nterface   | Residential                    | 1 .  | \$ 13.04   |  | 1 .                    | 4 18.0      |
| (Total)  | Business                       | 1 .  | 13.04  | 1 .  |                        | 1 15.0      |
| NID, Protector & Interface   | Residential                    | 1 .  | \$ 56.61   |  | ¥ •                    | 1 18.0      |
| (Orand Total) - Installed  | Bueinese                       | 1 .  | \$ 56.61   | 1 .  | 1 .                    | \$ .44.0    |
| Digital Loop Carrier (DLC) Fixed Cost  | 0                              | \$ 19,120.17   | \$ 19,120.17   | \$ 23,158.57   | \$ 23,753.40           | 118,300,0   |
|  | 28                             | 18 203.56<br>23,788.75   | 19,203.58<br>23,769.75   | \$ 23,158,57   | 23,763.40<br>23,763.40 | 4 18,300.0  |
|  | 4.9                            | \$ 23,768.75<br>\$ 23,866.56   | 23,769.75  | \$ 26,928.10<br>\$ 26,920.10   |                        |             |
|  | 97                             |  |  |  | \$ 30,299.78           | \$ 27,700.0 |

Decket No. 980696-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

|  | 1                 | BCPM 3.1  |                               |                       |                      |  |
|--|-------------------|---|-------------------------------|-----------------------|----------------------|--|
| NAMES OF A DESCRIPTION   | August August     | Bellowth -  | BCPM 3.1<br>Belifeuth-FL      | BOPM 3.1<br>Eprint-FL | BCPM 3.1<br>GTE - FL | Hild B.Co<br>Florida   |
| INPUT VALUE DESCRIPTION  | Density Zone      | Defeult   | [8/5/94]                      | (8/3/991              | (8/3/94)             | (8/3/94)   |
|  |                   | [1/16/96]   |                               |                       |                      |  |
|  | 103               | \$ 37,873.22<br>\$ 64,291.00  | \$ 37,873.22<br>\$ 64,291,00  | \$ 36,675,90          |                      | 0 37,100.00  |
| and the second se  | 241<br>385        | 1 68,377.00   | 68,377.00                     | \$ 130,818.01         | \$ 80,196.60         | \$ 37,100.00<br>\$ 70,000.00   |
|  | 673               | 1 96,659,00   | \$ 96,659.00                  | \$ 128,568.72         | \$ 113,125,29        | \$ 23,500.00   |
|  | 1345              | \$ 105,230.00   | Annual Cold States and States |                       | \$ 132,112.15        | *******  |
| Digital Loop Carrier (DLC) per Line Cost   | VG: 0 - 192       | \$ 84.00  | \$ \$4.00                     | 4 88.59               |                      | 6 100.00   |
| COLUMN CONFERENCE (COLUMN COLUMN | VG: 182 - 2018    | and the second se | 4 89,11                       | 68.02                 | 8 72.30              | 4 77.84  |
|  | ISDN              | 1   | \$ .                          | 1 .                   | 3                    | N//  |
|  | D61               | 1 .   | \$ .                          | \$ .                  | \$ .                 | PL/J   |
|  | DOS               | 1 .   | 1 .                           | 1 .                   | \$ .                 | \$6/1  |
|  | 4W                | 1 .   | 1 .                           | 1 .                   | \$ .                 | 96/7   |
|  | (85               | 1 .   | 1 .                           | \$ .                  | \$                   | N//  |
|  | COIN (High Dens.) | 1 .   | 1 .                           |                       | \$ .                 | 8 125.00   |
|  | ADGL              | 1 . 1   |                               |                       | \$ .                 | N//  |
|  | HOS               | 3   | 1                             | 1 1111                | 1                    | N//  |
| Factors · Electronice  |                   | 85.00%  | 65.00%                        | 85.00%                | 85.00%               | 90.08  |
| Ascimum Copper Distribution Cable Len  | rth .             | 12,000  | 12,000                        | 12,000                | 12,000               | the second s |
| itier / Copper Break Joint   |                   | 12,000  | 12,000                        | 12,000                | 12,000               | 9,00   |
| aire per Housing Unit  |                   | 2   |                               | 2                     | 2                    | NU   |
| Aaximum Fibry Faeder   |                   | 288   | 298                           | 216                   | 268                  | 21   |
| Assimum Copper Distribution Size   | ANALA ANALA       | 3600  | 3600                          | 11,70%                | 3800                 | 2,40   |
| Sant Mix - Distribution - % Aerial   | 00000 - 00005     | 40.00%  | 40.00%                        | 11,70%                | 21,62%               | 26.00  |
|  | 00005-00100       | 37.00%  | 37.00%                        | 12 20%                | 25.72%               | 25,00  |
|  | 00100-00200       | 30.00%  | 33.00%                        | 12.40%                | 21,77%               | 25.00  |
|  | 00200-00850       | 20.00%  | 20.00%                        | 12,70%                | 10.61%               | 30,00  |
|  | 00850 - 02550     | 10.00%  | 10.00%                        | 12.80%                | 29.65%               | 30.00  |
| the second  | 02550 - 05000     | 5.00%   | 5.00%                         | 13.00%                | 34.59%               | 10.00  |
|  | 05000 · 10000     | 5.00%   | 5.00%                         | 13.10%                | 73.90%               | 60.00  |
|  | 10000 +           | 0.00%   | 0.00%                         | 13,20%                | 73.60%               | 85.00  |
| Sant Mix · Distribution · % Buried   | 00000 - 00005     | 60.00%  | 60.00%                        | 87.50%                | 78.11%               | 78.00  |
| IEO. INS. CONTRACTOR INCOMENTS   | 00005 - 00100     | e1.00%  | 61,00%                        | 67.10%                | 78.11%               | 78.00  |
|  | 00100 - 00200     | 62.00%  | 62.00%                        | 66.70%                | 73.01%               | 78.00  |
|  | 00200 - 00850     | 62.00%  | 62.00%                        | 66.40%                | 77,42%               | 70,00  |
|  | 00850 - 00850     | 65.00%  | 65.00%                        | 86,10%                | 79.52%               | 70,00  |
|  | 00850 - 02550     | 65.00%  | 65,00%                        | 85.90%                | 69,36%               | 70.00  |
|  | 02550 - 05000     | 55.00%  | 55.00%                        | 85.60%                | 64.68%               | 65.00  |
|  | 05000 - 10000     | 35.00%  | 35.00%                        | 85.50%                | 24.14%               | 35.00  |
|  | 10000 +           | 10.00%  | 10.00%                        | 0.50%                 | 24.14%               | 5,00   |
| Sent Mix - Distribution - % Underground  |                   | 2.00%   | 2.00%                         | 1.00%                 | 2.65E-03             | 0.00   |
|  | 00005 - 00100     | 8.00%   | 5.00%                         | 1.10%                 | 3.77E-03             | 0,00   |
|  | 00200 - 00850     | 8.00%   | 8.00%                         | 1,20%                 | 8.17E-03             |  |
|  | 00050 - 00850     | 15.00%  | 15.00%                        | 1,20%                 | 0.72E-05             | 0.00   |
|  | 00850 - 02550     | 25.00%  | 25.00%                        | 1,30%                 | 0.60E-03             | 0.00   |
|  | 02550 - 05000     | 40.00%  | 40.00%                        | 1.40%                 | 5.32E-03             | \$,00  |
|  | 05000 - 10000     | 60.00%  | 60.00%                        | 1.40%                 | 1.958-02             | \$.00  |
|  | 10000 +           | 80.00%  | 80.00%                        | 1.50%                 | 1.96E-02             |  |
| Sant Mix - Copper Feeder - % Aerial  | 00000 - 00005     | 40.00%  | 40.00%                        | 3,30%                 | 11,30%               | \$0.00   |
|  | 00005 - 00100     | 40.00%  | 40.00%                        | 3,10%                 | 11,30%               | 60.00  |
|  | 00100 - 00200     | 40.00%  | 40.00%                        | 2,80%                 | 17.24%               | 60.00  |
|  | 00200 - 00850     | 40,00%  | 40,00%                        | 2,80%                 | 16,12%               | 40,00  |
|  | 00650 - 00850     | 25.00%  | 25.00%                        | 2.70%                 | 11,65%               | 30.00  |
|  | 00850 - 02550     | 10.00%  | 10.00%                        | 2,80%                 | 16,00%               | 20.00  |
|  | 02550 - 05000     | 0.00%   | 0.00%                         | 2.80%                 | 20,03%               | 15.00  |
| the second in the second se  | 05000 - 10000     | 0.00%   | 0.00%                         | 2,30%                 | 13,24%               | 10.00  |
| Lost Max - Concess Freder, M. R  | 10000 +           | 0,00%   | 0.00%                         | 2,30%                 | 13.24%               |  |
| tent Mix - Copper Feeder - % Buried  | 00000 - 00005     | 45.00%  | 45,00%                        | 82,90%                | 82,41%               | 45.00  |
|  | 00100 - 002.0     | 40,00%  | 40.00%                        | 81,40%                | 68.36%               | 45.00  |
|  | 00200 - 00050     | 35,00%  | 35.00%                        | 80,10%                | 59.90%               | 40.00  |
|  | 00850 - 00850     | 30.00%  | 30.00%                        | 78,00%                | 60.37%               | 30,00  |
|  | 00850 - 02550     | 25,00%  | 25.00%                        | 78,10%                | 50.26%               | 20.00  |
|  | 02550 - 05000     | 20.00%  | 20.00%                        | 77,20%                | 48.32%               | 10,00  |
|  | 05000 - 10000     | 10.00%  | 10.00%                        | 78,50%                | 22.64%               | \$,00  |
|  | 10000 +           | 8,00%   | 5.00%                         | 75,80%                | 22,84%               |  |
| fant Mix - Copper Feeder - % Undergro  |                   | 10,00%  | 10.00%                        | 12.00%                | 6,208-02             | 6,00   |
|  | 00005 - 00100     | 18,00%  | 18,00%                        | 14,00%                | 6,208-02             |  |
|  | 00100 - 00200     | 20,00%  | 20.00%                        | 18,70%                | 14,40%               | 6,00   |
|  | 00200 - 00650     | 25,00%  | 25.00%                        | 17,10%                |                      |  |
|  | 00660 - 00850     | 45.00%  | 45,00%                        | 18,30%                | 28.08%               | 40,00  |
|  | 00850 - 02550     | 65.00%  | 45.00%                        | 19,40%                | 33.87%               | 60,00  |
|  | 02550 - 05000     | 80,00%  | 80,00%                        | 20,90%                | 31,00%               |  |
|  | 05000 - 10000     | 80.00%  | \$0,00%                       | 21,20%                | 64.22%               | 85,00  |
| Sant Mix - Filter Feeder - % Aerial  | 10000 + 00006     | 40.00%  | 95,00%<br>40,00%              | 21,90%                | 64.22%               |  |
|  | 1 00000 + 00006   | 40.00%  | 40,00%                        | 6.1976                | 0,21%                |  |
| SHOT FOR - FRISE FRISER,   | 00005 - 00100     | 40,00%  | 40,00%                        | 2.10%                 | 0.21%                | 25,00  |

#### Docket No. 800036-TP J. W. Wells Exhibit No. \_\_\_\_ (JWW-4) Input Value Comparisons

| INPUT VALUE DESCRIPTION  | Density Zone   | BCPM 3.1<br>BallSouth -<br>Default<br>[1/16/98] | BOPSA 3.1<br>BellSouth-FL<br>(9/3/98) | BCPM 3.1<br>8ptn:/L<br>(8/3/98) | 8CPM 3.1<br>GTE - FL<br>[8/3/90] | HM 8.0+<br>Fiorida<br>(8/3/94) |
|--|----------------|---|---------------------------------------|---------------------------------|----------------------------------|--------------------------------|
|  | 00200 - 00650  | 40.00%  | 40.00%                                | 2.00%                           | 0.97%                            | 30.00%                         |
|  | 00850 - 00850  | 28.00%  | 25.00%                                | 1.80%                           | 1,12%                            | 30.00%                         |
|  | 00850 - 02550  | 10.00%  | 10.00%                                | 1.80%                           | 1.88%                            | 20.00%                         |
|  | 02550 - 05000  | 0.00%   | 0.00%                                 | 1.70%                           | 2.33%                            | 15.00%                         |
|  | 05000 - 10000  | 0.00%   | 0.00%                                 | 1,50%                           | 3.33%                            | 10.00%                         |
|  | 10000 +        | 0.00%   | 0.00%                                 | 1.40%                           | 3.33%                            | 5.00%                          |
| Mant Mix - Fiber Feeder - % Buried   | 00000 - 00%*51 | 50.00%  | 50.00%                                | 74.40%                          | 12.89%                           | 60.00%                         |
| and the second state of th | 00005 - 00100  | 45.00%  | 45.00%                                | 72.10%                          | 12.09%                           | 60.00%                         |
|  | 00100 - 00200  | 40,00%  | 40.00%                                | 69,40%                          | 7.635-02                         | 00.00%                         |
|  | 00200 - 00650  | 38.00%  | 35.00%                                | 66.20%                          | 8.246-02                         | 60.00%                         |
|  | 00650 - 00850  | 30.00%  | 30.00%                                | 62.30%                          | 5,13%                            | 30.00%                         |
|  | 00850 - 02550  | 25.00%  | 25.00%                                | \$7.40%                         | 7.488-02                         | 20.00%                         |
|  | 02550 - 05000  | 20.00%  | 20.00%                                | \$1,10%                         | 2.972-02                         | 10.00%                         |
|  | 05000 - 10000  | 10.00%  | 10.00%                                | 42.70%                          | 0.00%                            | 5.00%                          |
|  | 10000 +        | 6.00%   | 5.00%                                 | 30,80%                          | 0.00%                            | 8.00%                          |
| Mant Mix - Fiber Feeder - % Undergroun   | 00000 - 00005  | 10.00%  | 10.00%                                | 23,50%                          | 80.01%                           | \$.00%                         |
| AND THE TRUE TRUE TO A STREET BOARD  | 00005 - 00100  | 16.00%  | 15.00%                                | 28.80%                          | 88.91%                           | 8.00%                          |
|  | 00100 - 00200  | 20.00%  | 20.00%                                | 28.60%                          | 02.14%                           | 6.00%                          |
|  | 00200 - 00650  | 25.00%  | 26.00%                                | 31.80%                          | 80.78%                           | 10.00%                         |
|  | 00650 - 00650  | 45.00%  | 45.00%                                | 25.80%                          | 83.74%                           | 40.00%                         |
|  | 00850 - 02550  | 65.00%  | 65.00%                                | 40.80%                          | 90.65%                           | 60.00%                         |
|  | 02550 - 05000  | 80.00%  | 80.00%                                | 47.20%                          | 84.70%                           | 75.00%                         |
|  | 05000 - 10000  | 80.00%  | 80.00%                                | 65.80%                          | 98.87%                           | 85.00%                         |
|  | 10000 +        | 85.00%  | 85.00%                                | 67.90%                          | 00.67%                           | 80.00%                         |
| Fill Factora - Distribution  | 00000 - 00005  | 100.00%   | 100.00%                               | 100.00%                         | 85.00%                           | 80.00%                         |
| M. L. WINNEL, WIND BORDON  | 00005 - 00100  | 100.00%   | 100.00%                               | 100.00%                         | 98.00%                           | 55.00%                         |
| the second se  | 00100 - 00200  | 100.00%   | 100.00%                               | 100.00%                         | 80.00%                           | 65.00%                         |
|  | 00200 - 00650  | 100.00%   | 100.00%                               | 100.00%                         | 68.00%                           | 60.00%                         |
|  | 00850 - 00850  | 100.00%   | 100.00%                               | 100.00%                         | 96.00%                           | 65.00%                         |
|  | 00850 - 02550  | 100.00%   | 100.00%                               | 100.00%                         | \$8.00%                          | 70.00%                         |
|  | 02550 - 05000  | 100.00%   | 100.00%                               | 100.00%                         | F8.00%                           | 78.00%                         |
|  | 05000 - 10000  | 100.00%   | 100.00%                               | 100.00%                         | 68.00%                           | 75.00%                         |
|  | 10000 +        | 100.00%   | 100.00%                               | 100.00%                         | 98.00%                           | 75.00%                         |
| Fill Fectors - Feoder  | 00000 - 00005  | 75.00%  | 71.10%                                | 53.45%                          | 65.00%                           | 65.00%                         |
|  | 00005 - 00100  | 80.00%  | 71,10%                                | 54,21%                          | 65.03%                           | 75.00%                         |
|  | 00100 - 00200  | 80.00%  | 71.10%                                | 54.84%                          | 65.00%                           | 80.00%                         |
|  | 00200 - 00850  | 85.00%  | 71.10%                                | 65.87%                          | 65.00%                           | 80.00%                         |
|  | 00850 - 00850  | 85.00%  | 71.10%                                | 58.30%                          | 65.00%                           | 80.00%                         |
|  | 00850 - 02550  | 85.00%  | 71.10%                                | 57.12%                          | 65.00%                           | 80,00%                         |
|  | 02550 - 05000  | 85.00%  | 71.10%                                | 57.85%                          | 65.00%                           |                                |
|  | 05000 - 10000  | 85.00%  | 71.10%                                | 58.57%                          | 65.00%                           | 80.00%                         |
|  | 10000 +        | 85.00%  | 71.10%                                | 59 30%                          | 65.00%                           | 80,00%                         |
| and the second se  | 10000.1        | 10.001  | 73.1978                               | 00.0/%                          | 60.00%                           | 80,00%                         |



Transcribed from DSC Communications Practices & shading enhanced for clarity

14

Docket No. 980696-TP ). W. Wells Exhibit No. \_\_\_ (JWW-6) Efficiency of Rectangular Lots Page 1 of 3

|      |       | 1000 |       |      |       |      |       |      |   | TTUNE            |   |       | Γ |     |   |   | Γ |       |                |       | Γ |
|------|-------|------|-------|------|-------|------|-------|------|---|------------------|---|-------|---|-----|---|---|---|-------|----------------|-------|---|
|      |       |      | Γ     | Ľ    |       |      |       |      | Γ | STATES IN COLUMN | Γ | Γ     |   |     | Γ | Γ |   | Γ     | Г              |       | Ī |
|      |       |      |       |      | Ī     | 825  | 0.22  | 1010 | Ī |                  |   |       | Ī | CAD |   |   | ľ |       |                |       | Ĩ |
|      | 1000  |      |       |      |       |      |       |      |   | THE ROOM         |   |       |   |     |   |   |   |       | and the second |       |   |
|      |       |      |       |      |       |      |       |      | Γ | <b>Intern</b>    |   |       |   |     |   |   |   |       |                |       |   |
| 1000 | 11221 |      | 10.02 |      | 11111 | 1000 |       |      |   | <b>TING</b>      |   |       |   |     |   |   |   |       |                |       |   |
|      |       |      |       |      | 1002  |      | 11111 |      |   | 101100           |   | 1000  |   |     |   |   |   |       | Π              |       |   |
|      |       |      |       |      | 11111 |      |       |      |   | CHARLEN IN       |   |       |   |     |   |   |   |       |                | 1000  |   |
|      | 10220 |      | 11111 | 2222 |       |      |       |      |   | THE R            |   | 11111 |   |     |   |   |   | 11111 |                | 10000 |   |
| E    |       |      | 100   |      |       |      |       |      |   | Con la           |   |       |   |     |   |   |   |       |                |       |   |

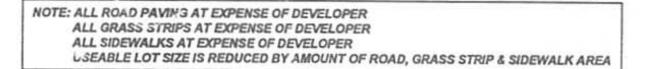
#### RECTANGULAR LOTS

# INEFFICIENT RECTANGULAR LOTS

| 5 40 50 2 | A DOUT                                  | 502 200          | 100       | 1000    | C-42 8.18 | A DESCRIPTION OF   |         |          |        |              |     |  |  |  |
|-----------|---|------------------|-----------|---------|-----------|--|---------|----------|--------|--------------|-----|--|--|--|
|           |   | 1.1.1.1          | 1111      | -1-1-   |           | 1  |         |          |        | 1            |     |  |  |  |
|           |   | 1111             |           |         |           | 1111   | TAR     |          | 1.1    |              |     |  |  |  |
| 1000      | Cardinates                              | Accession of the | 223       | 1000.0  | 0492      | - and a second   | 20074   | 199.20   | 20121  | <b>GERCE</b> | 28  |  |  |  |
| 9         |   |                  |           |         |           |  | 1.1.1   |          |        |              |     |  |  |  |
| 1         | 1111                                    | -                |           |         |           | 1  |         |          |        | _            |     |  |  |  |
|           |   | 1.1.1.1          |           | 1000    |           |  | 10000   | Care and | 20.8   | 115.0        | 100 |  |  |  |
|           |   |                  |           |         |           | 2 Marine   |         |          |        |              | -   |  |  |  |
|           | COLUMN ST                               | Contraction of   | -         | tion of | -         | 1223   | and and | L        | -      | L            | _   |  |  |  |
|           |   | 12121            | 1.11      | 211     | 8333      | Concession of the local division of the loca | 1000    |          |        | ALC: N       |     |  |  |  |
|           | 12.2.2.2                                | 10.11            | 1.1.1     | 1.11    |           | 11111  |         | 12121    |        | 1.1.1        | -   |  |  |  |
| ALC: N    | all | -100             | 100.00    | 100.0   | No. Co.   | (Lanes   | 001900  | 100.254  | 141.41 | No Mark      | -   |  |  |  |
|           | 11111                                   |                  |           |         |           | 1.1  |         | 12:2:1   |        |              | r   |  |  |  |
|           |   | 1993             | 100       |         |           | 11111  | 1111    |          | 1111   | 1.1.1.1      | 1.  |  |  |  |
| Sec.      | AV at S                                 | 1000             | - Carton  | -0      | Cleans    | all sont   | 30500   | 16-072   | 83.5   | 46.0         | 20  |  |  |  |
|           |   |                  |           |         |           |  | 100     | 1111     |        |              |     |  |  |  |
|           |   |                  | 12223     |         | 1993      |  |         |          |        |              |     |  |  |  |
| No.       | 1000                                    | 10000            | 1000      | 192.24  | 1000      | 10000  | 00000   | 100      | 80.51  | 1000         | 10  |  |  |  |
|           |   |                  |           | 1223    |           | 1212   |         | -1-1-    |        | -1-1-        |     |  |  |  |
|           |   |                  |           |         |           |  |         | 24243    |        | 0.00         |     |  |  |  |
|           | 10.00                                   | 11111            | CHOICE ST | 10010   | CREW COL  | 1000   | 1203    |          | A1.04  | 100.00       | 100 |  |  |  |
|           |   |                  |           |         |           | استعتما  | -       |          | _      |              | -   |  |  |  |
|           |   |                  |           |         |           |  |         |          |        |              |     |  |  |  |
| 10000     |   | 20103            | inter i   |         |           | 1000   |         | 1000     | 20.20  | 141000       |     |  |  |  |
| 10000     |   | 1.1.1.1          | 1.1.1     | 1.1.1   |           | 1.1.1.1.1  |         | 12011    |        | 27-32        |     |  |  |  |

# TROADS 14 LENGTHS OF GRASS STRIP 14 LENGTHS OF SIDEWALK

# 11 ROADS 22 LENGTHS OF GRASS STRIP 22 LENGTHS OF SIDEWALK



Docket No. 980696-TP J. W. Wells Exhibit No. \_\_\_ (JWW-5) Efficiency of Rectangular Lots Page 2 of 3

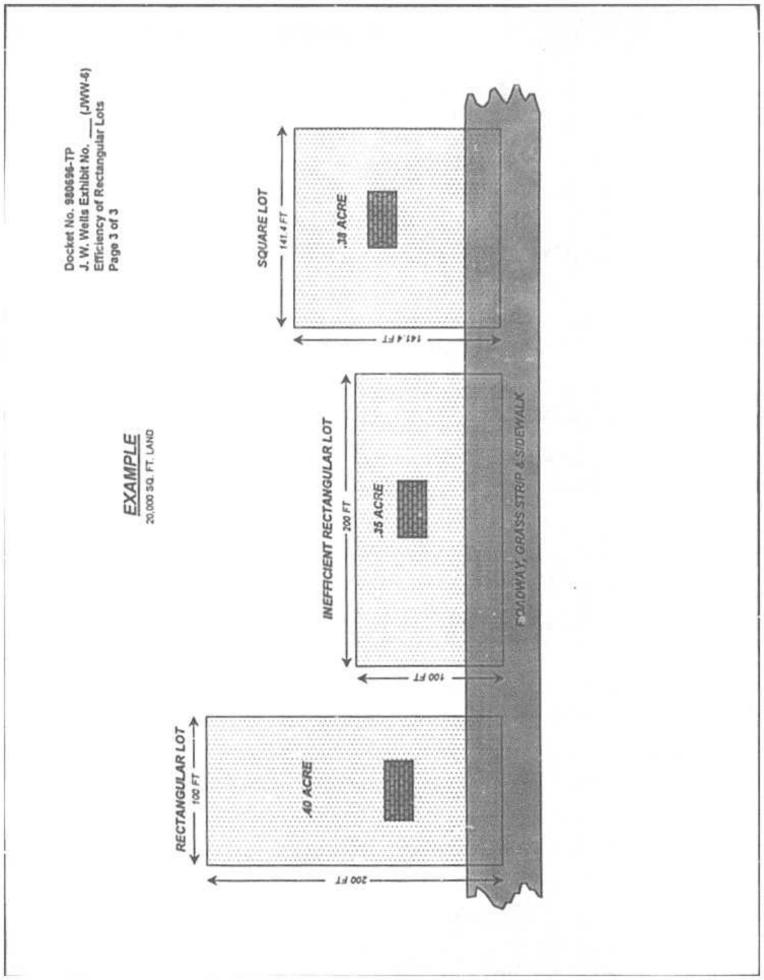
# SQUARE LOTS

# 7 ROADS 12 LENGTHS OF GRASS STRIP 12 LENGTHS OF SIDEWALK

RECTANGULAR LOTS

# 9 ROADS 18 LENGTHS OF GRASS STRIP 18 LENGTHS OF SIDEWALK

NOTE: ALL ROAD PAVING AT EXPENSE OF DEVELOPER ALL GRASS STRIPS AT EXPENSE OF DEVELOPER ALL SIDEWA! KS AT EXPENSE OF DEVELOPER USEABLE LOT SIZE IS REDUCED BY AMOUNT OF ROAD, GRASS STRIP & SIDEWALK AREA



# CERTIFICATE OF SERVICE

I HEREBY CERTIFY that a copy of the foregoing was furnished to the following parties by U.S. mail this <u>lst</u> day of October, 1998.

Will Cox Division of Legal Services Florida Public Service Commission 2540 Shumard Oak Boulevard Tallahassee, FL 32399

Charles J. Beck Deputy Public Counsel Office of Public Counsel c/c The Florida Legislature 111 West Madison Street Room 812 Tallahassee, Fl ?2399

Tracy Hatch, Esquire AT&T 101 N. Monroe Street, Suite 700 Tallahassee, Fl 32301

Joseph A. McGlothlin Vicki Gordon Kaugman McWhirter, Reeves, McGlothlin Davidson, Rief & Bakas, P.A. 117 S. Gadsden Street Tallahassee, FL 32301

Floyd R. Self, Esq. Messer, Caparello & Self, P.A. 215 S. Monroe St. Ste 701 Tallahassee, FL 32301

Mr. Brian Sulmonetti WorldCom, Inc. 1515 S. Federal Hgy, Suite 400 Boca Raton, Florida 33432

Robert G. Beatty Nancy B. White c/o Nancy H. Sims 150 S. Monroe St., Suite 400 Tallahassee, FL 32301

Michael A. Gross Office of The Attorney General PL-01 The Capitol Tallahassee, FL 32399-1050 Kimberly Caswell GTE Florida Incorporated P.O. Box 110, FLTC0007 Tampa, FL 33601-0110

Patrick Knight Wiggins Donna L. Canzano Wiggins & Villacorta, P.A. 2145 Delta Boulevard Suite 200 P.O. Drawer 1657 Tallahassee, FL 32302

Steve Brown Intermedia Communications Inc,. 3625 Queen Palm Drive Tampa, FL 33619-1309

David B. Erwin 127 Riversink Road Crawfordville, FL 32327

Tom McCabe P.O. Box 189 Quincy, Florida 32353-0189

Mark Ellmer P.O. Box 220 502 Fifth Street Port St. Joe, Florida 32456

Robert M. Post, Jr. P.O. Box 227 Indiantown, Florida 34956

Kelly Goodnight Frontier Communications 180 South Clinton Avenue Rochester, NY 14646

Lynn B. Hall Vista-United Telecommunications P.O. Box 10180 Lake Buena Vista, FL 32830 J. Jeffry Wahlen Ausley & McMullen P.O. Box 391 Tallahassee, FL 32302

Lynne G. Brewer Northeast Florida Telephone Co. P.O. Box 485 Macclenny, FL 32063-0485

Harviet Eudy ALLTEL Florida, Inc. P.O. Box 550 Live Oak, FL 32060

Laura L. Gallagher Vice President-Regulatory Affairs Florida Cable Tel. Asso. 310 N. Monroe Street Tallahassee, FL 32301

Paul Kouroupas Michael McRae, Esq. Teleport Com. Group, Inc. 2 Lafayette Centre 1133 Twenty-First Street, N.W. Suite 400 Washington, DC 20036

Suzanne F. Summerlin, Esq. 1311-B Paul Russell Rd., Ste.201 Tallahassee, FL 32301

Charles J. Rehwinkel Sprint-Florida, Incorporated P.O. Box 2214 MS: FLTLH00107 Tallahassee, FL 32316

Norman H. Horton, Jr. Messer, Caparello & Self, Esq. 215 S. Monroe Street Suite 701 Tallahassee, FL 32301-1876

James C. Falvey, Esq. e.spire(TM) Communications, Inc. 133 National Business Parkway Suite 200 Annapolis Junction, MD 20701

110807.1 CO8/9806/96 Peter M. Dunbar, Esg. Barbara D. Auger, Esg. Pennington, Moore, Wilkinson, Bell & Dunbar, P.A. P.O. Box 10095 Tallahassee, FL 32302

Carolyn Marek Vice President of Regulatory Affairs P.O. Box 210706 Time Warner Communications Nashville, TN 37221

Charles Murphy Booter Imhof Utilities and Communications Committee 428 House Office Building 402 S. Monroe Street Tallahassee, FL 32399-1300

Brian P. Farley Collier, Shannon, Pill & Scott. PLLC 3050 K. Street NW Washington, D.C. 20007

The D.

Attorney