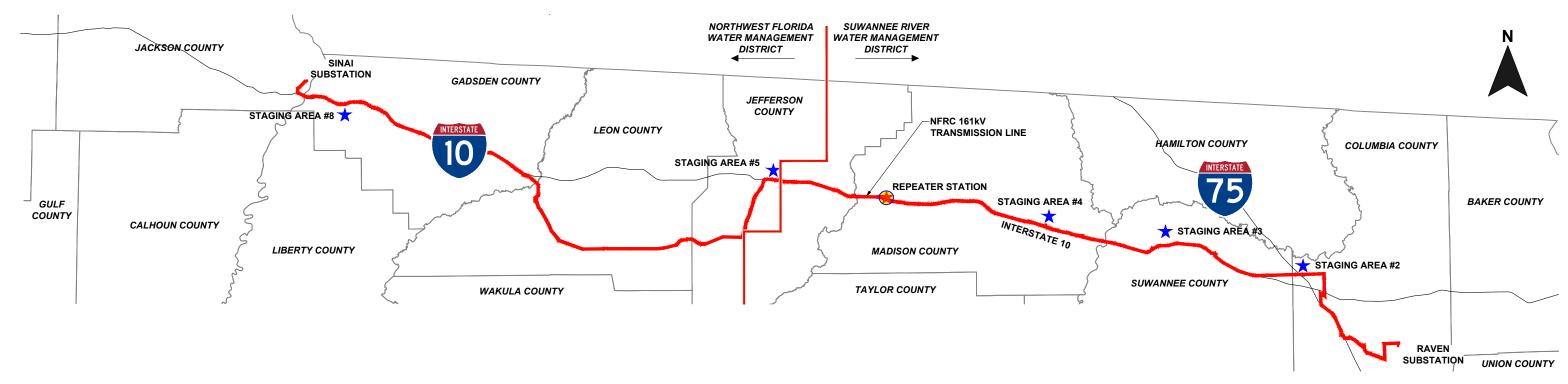
GULF POWER COMPANY

NFRC TRANSMISSION LINE PROJECT REPEATER STATION SITE PLAN EXHIBIT





LEGEND PROPOSED STAGING AREAS & REPEATER STATION



This document has been electronically signed and sealed by Michael Leahy, P.E., P.S.M. using a Digital Signature and date.

before you dig.

2 Printed copies of this document are not considered signed and sealed and the signature must be

REVISIONS, CLARIFICATIONS FOR RAI#2 RESPONSE 12-20-19

Gulf Power

NORTH FLORIDA RESILIENCY TRANSMISSION ENGINEERING DEPARTMENT REPEATER STATION SITE PLAN EXHIBIT

FOR TEMPORARY USE AS LAYDOWN YARDS OUNTY: MADISON FILE NAME: NFRC EXH REPEATER RO2.dwg

erified on any electronic copies.

REPEATER STATION SITE PLAN EXHIBIT

REPEATER STATION SITE EXHIBIT **GENERAL NOTES AND SITE INFORMATION PLAN VIEW AND CROSS SECTIONS** TYPICAL CONSTRUCTION DETAILS FENCE AND BMP DETAILS

SHEET 2 SHEETS 3 - 4 SHEET 5 SHEET 6

CONTRACTOR SHALL VERIFY ALL CONDITIONS ON JOB SITE & NOTIFY PROJECT MANAGER AND ENGINEER OF ANY VARIATIONS FROM DIMENSIONS SHOWN ON THESE DRAWINGS
BEFORE PROCEEDING WITH ANY
CONSTRUCTION.

PICKETT AND ASSOCIATES, INC 5025 WEST GRACE STREET PHONE: (813) 877-7770

CA #31323 LB #364

THE BEST OF THIS ENGINEER'S KNO FLORIDA LICENSED PROFESSIONAL ENCINEER No. 45287
PROFESSIONAL SLRVEY OR & MAPPER No. 5658

1 OF 3

Table 4: Summary of Treatment Volume and Recovery						
	Treatment	Treatmen	Recovery			
Basin No.	Volume Required (acft)	Rock Voids	Water Quality Basins	Time (hrs)		
I	0.006	0.004	Not Required for Treatment	2		

98 93

FLOOD ZONE NOTES:

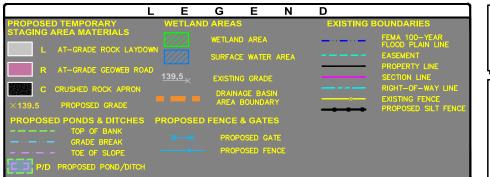
1. FLOOD ZONE INFORMATION BASED ON THE GADSDEN COUNTY, FLORIDA FLOOD INSURANCE RATE MAPS:

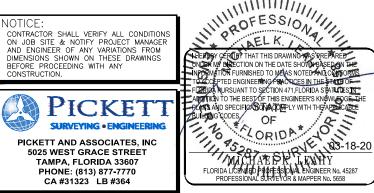
MAP NUMBER 12079C0235C (DATED 05-03-10)

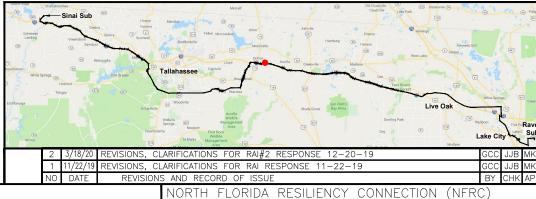
2. APPLICABLE FLOOD ZONE DELINEATIONS PER THE ABOVE REFERENCED FLOOD INSURANCE RATE MAP ARE AS FOLLOWS:

ZONE X AREA OUTSIDE THE 100-YEAR FLOOD PLAIN

- This document has been electronically signed and sealed by Michael Leahy, P.E., P.S.M. using a
 Digital Signature and date.
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TRANSMISSION ENGINEERING DEPARTMENT

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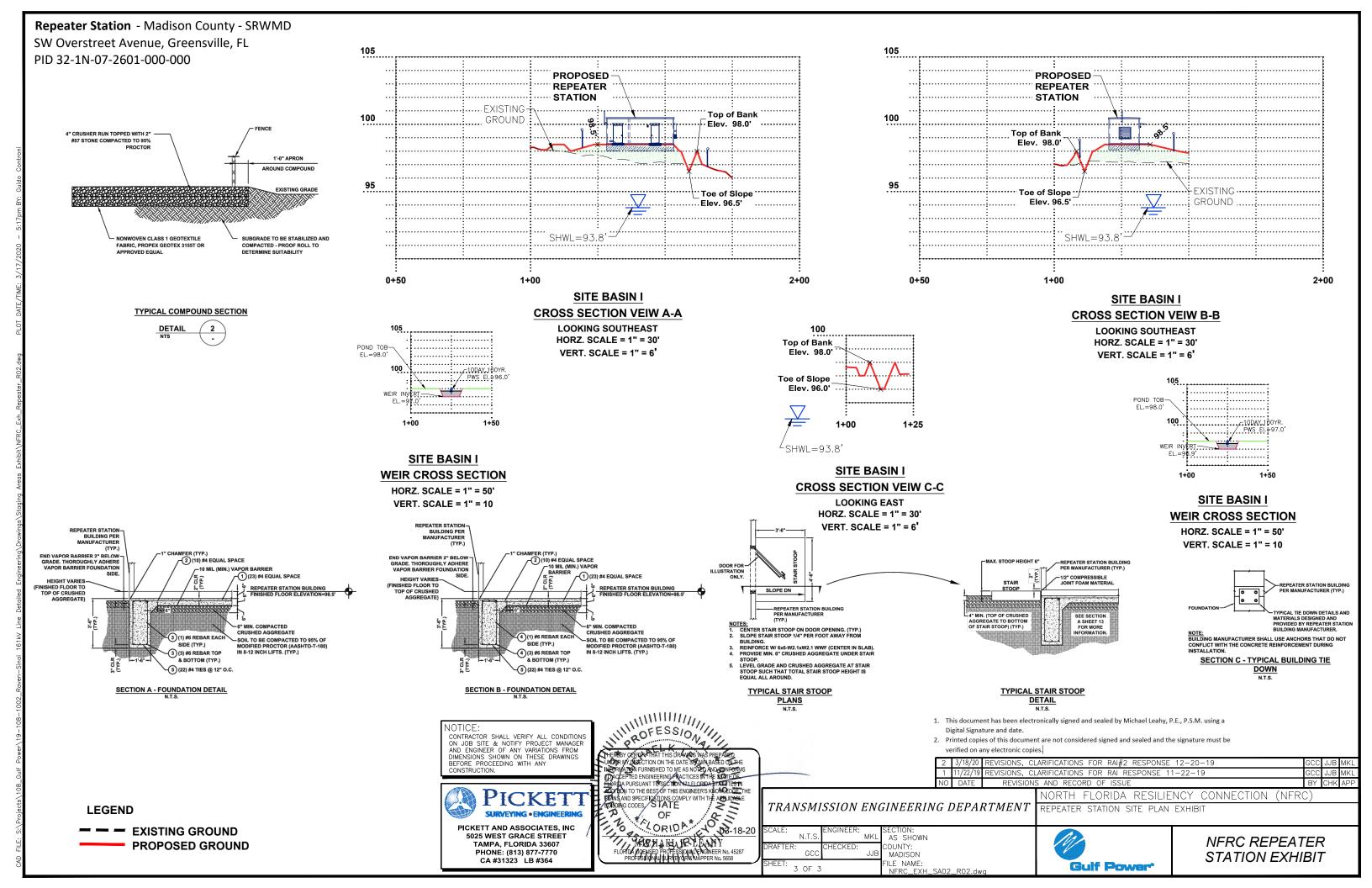
2 OF 3

MADISON

FILE NAME: NFRC_EXH_SA02_R02.dwg REPEATER STATION SITE PLAN EXHIBIT
SHOWING EXISTING BORINGS AND SITE PLAN REFERENCE



NFRC REPEATER STATION EXHIBIT



Repeater Station

Stormwater Calculations

for the

North Florida Resiliency Connection Project



Gulf Power 15430 Endeavor Drive Jupiter, FL 33478

Prepared by:



Pickett and Associates, Inc. 5025 W. Grace Street Tampa, FL 33607

Table of Contents

1.0	Site Data	3
2.0	Project Narrative	3
3.0	Stormwater Calculations	4
	Appendix A – Geotechnical Report (includes recovery analysis)	
	Appendix B - HydroCAD Report	
	Appendix C – Firm Map	
	Appendix D – SRWMD Rainfall Distribution Data	
	Appendix E – SRWMD Boundary Map	

1.0 Site Data

Madison County – SRWMD
SW Overstreet Ave., Greensville, FL
PID 32-1N-07-2601-000-000
Basin Area = 0.55 acres
Developed Area = 0.15 acres
Flood Zone X per FRIM Map 12079C0235C effective 05-03-10
Design Storm, Non Ag: 100 year, SCS Type II Distribution. 1-, 2-, 4-, 8-, 24-hour and 3-, 7-, and 10-day duration.

Recovery (Attenuation)

1. Provide treatment volumes within 72 hours following the end of the design storm event.

2.0 Project Narrative

Temporary Staging Area #2 will stage and store construction materials (poles, conductor, insulators, etc.) and equipment (drill rigs, line trucks, cranes, etc.). The developed area will consist of an at grade #57 crushed limerock surface to facilitate the storage of poles and equipment along with a perimeter road to facilitate access. The site has been reviewed to ensure that existing surface water flow will not be impeded and existing water quality will not be adversely impacted. All proposed semi-pervious material will be installed at the existing natural ground elevation throughout the site to prevent impedance of the existing watershed.

The staging area will use the void space between the #57 crushed limerock for storage for the first 1" of runoff. Gulf Power has done extensive testing on this void ratio and has determined that a 35% void ratio provides a good conservative value. In addition to utilizing the voids for storage, each site will have a swale / berm constructed on the low side(s) of each to ensure no stormwater runoff escapes to adjacent properties. Each site will also have a dry retention pond to account for attenuation. The ponds will be designed to recover within 72 hours. Soil Borings and Double Ring Infiltrometer Testing have been performed at each site to facilitate the design of each dry pond. The site will use the interior uncompacted gravel as additional area for recovery by incorporating the use of a check dam system. Since the site has a slight grade change, an impervious, flexible water barrier (CR-PE12-20) will be installed along each contour line to slow the progression of water over the site to allow recovery within 72 hours. This is detailed in the construction drawings.

The staging area will remain in place for the duration of the project. At the conclusion of the project, each staging area will be returned to its pre-construction state. The anticipated duration is approximately 12 - 18 months.

Construction and maintenance access to each staging area will be gained via existing road right-of-way. Connector aprons will be constructed in accordance with county / state requirements.

Deliveries and active use of staging areas will be consistent with construction hours.

No tree removal will be necessary to facilitate construction of staging area #2.

3.0 Repeater Design Criteria

The SCS TR-20 method was used to calculate the pre and post-development peak runoff. The time of concentration was generated from the sheet, shallow concentrated flow and Lag/CN method. A complete list of the procedure follows.

Assumptions and Methodology

The SRWMD requires that the difference between the 100-year pre-developed and post-developed storm volume be stored on-site with the maximum release rate not exceed the pre developed flow, Q. Per the SRWMD Handbook, the 100-year storm shall be evaluated for the greatest of the 1, 2, 4, 8, and 24 hour, 3, 7, and 10 days storms.

- Storm Frequency Type II 100 Year, 1, 2, 4, 8, and 24 hour, 3, 7, and 10 day storms
- Runoff Curve Number Weighted Curve Numbers were calculated for each area
 - Existing Conditions Curve Number Range: 73
 - Post-Developed Condition Curve Number Range: 75-98
- Calculation of Time of Concentrations
 - Lag/CN Method Which is used for areas of 2000 acres or less. The formula is provided below:
 - $T_c = 0.00526 \times L^{0.8} (1000/CN-9)^{0.7} \times S^{-0.5}$
- Peak Flow Rate Calculations HydroCAD Version 10.0
- Pond Recovery Calculations PONDS Version 3.3

Pre-Development Summary

The Repeater Station has mild slopes of up to 2% and generally consists of grasses and small shrubs. Table 1 below includes the results of the pre-development drainage area runoff calculations for the peak flow. These were developed using the topography which can be seen on the plan set and HydroCAD (Appendix B). Table 1 summarizes the peak flows for the various 100-year design storm in the pre-developed condition. The storm with the greatest runoff volume was used in the calculations. In this case, the 100-year, 10-day storm generated the greatest runoff and thus was used as the design storm.

	Table 1: Pre-Developed Peak Discharge										
Sub-	Area	Weighted	Time of Type II, 100-Year Storm, Q ₁₀₀ Concentration (CFS)								
Basin	(Acre)	CN	(Min.)	1 HR	2 HR	4 HR	8 HR	24 HR	3 DAY	7 DAY	10 DAY
I	0.55	60	7.4	0.00	0.00	0.00	0.07	1.10	1.59	1.89	2.30

Post-Development Summary

Upon completion of construction, the Repeater Station will consist of uncompacted gravel yard with compacted gravel drives and the repeater station shelter. Water quality basins will be generally located at low points in each sub-basin within the site. Table 2 below includes the results of the post-development calculations for the 100-year, 1, 2, 4, 8, and 24 hour, 3, 7, and 10 day peak flows. These

were developed using the topography which can be seen on the plan set and HydroCAD (Appendix B). The difference between the pre-development and post-development storm will be contained within the pond, and anything greater will be conveyed through the outflow weir per the Suwannee River Management District Design Requirement. The storm with the greatest runoff volume was used in the calculations. Again, in this case, the 100-year, 10-day storm generated the greatest runoff and thus was used as the design storm.

	Table 2: Post-Developed Peak Discharge											
	Sub- Basin	Area (Acre)	Weighted Concentration Type II, 100-Year Storm, Q ₁₀₀ (CFS)									
	Dasiii	(Acre)	CN	(Min.)	1 HR	2 HR	4 HR	8 HR	24 HR	3 DAY	7 DAY	10 DAY
Ī	I	0.55	73	9.4	0.00	0.00	0.00	0.09	1.36	1.84	2.13	2.52

Table 3 below summarizes the stormwater quality basin design and key pond elevations with required and provided volumes. It shows that each basin provides the required amount of freeboard (1-foot) and storage required to retain the peak runoff. Peak water surface elevation calculations for detention ponds were developed using HydroCAD (Appendix B).

	Table 3: Pond Storage Data						
Basin No.	Elevation (ft, NAVD 88)		Area (ac)	Provided Volume (acft)	Required Volume (acft)	Provided Discharge at Weir (cfs)	
	Top of Pond	98.0	0.003				
1.1	Peak Water Elev.	96.0		0.101	0.019		
South	Weir Elev.	97.0		0.101		0.53	
	Bottom of Pond	96.0	0.001				
	Top of Pond	98.0	0.004				
1.2	Peak Water Elev.	97.0		0.034	0.033	1.26	
North	Weir Elev.	96.9					
	Bottom of Pond	96.5	0.002				

Water Quality/Treatment Methodology

The SRWMD Handbook requires that all stormwater management systems provide the minimum state water quality treatment requirements. The method utilized for this project consists of one or a combination of percolation in the existing soils within the rock voids of the laydown storage and/or percolation within the stormwater quality basin. To determine the treatment runoff volume, the first 1.0-inch of rainfall was used along with the composite runoff coefficient for each sub-basin. This was compared with the volume from the first 0.5-inch rainfall without the coefficient. The greater volume was used for treatment evaluation and recovery. The calculations can be found starting on Page 7.

Recovery was calculated utilizing the PONDS software, as approved by the district. The rate of recovery was calculated within both the rock voids and if needed, the water quality basins. To model the rock voids, we calculated the available void space within the laydown area using a 35% uncompacted void ratio. An adjusted stage-storage table was input into the PONDS model utilizing a one-half foot

increment stage, which corresponds to the height of the check dam. All treatment volumes must recover within 72-hours. See Table 4 for a summary of treatment volumes and recovery times for each sub-basin within the staging area.

Table 4: Summary of Treatment Volume and Recovery						
	Treatment	Treatmen	Recovery			
Basin No.	Volume Required (acft)	Rock Voids	Water Quality Basins	Time (hrs)		
I	0.006	0.004	Not Required for Treatment	2		

Water Quality Recovery Volume Calculations

BASIN I:

Areas:

Total Area =
$$(6,326 \text{ S. F.}) \times \left(\frac{1 \text{ Ac.}}{43.560 \text{ S. F.}}\right) = 0.15 \text{ Ac.}$$

Crushed Rock for Laydown Area =
$$(973 \text{ S. F.}) \times \left(\frac{1 \text{ Ac.}}{43,560 \text{ S. F.}}\right) = 0.02 \text{ Ac.}$$

Crushed Rock Road Area =
$$(1,283 S.F.) \times \left(\frac{1Ac.}{43,560 S.F.}\right) = 0.03Ac.$$

Pond Area =
$$(284 \, S.F.) \times \left(\frac{1Ac.}{43.560 \, S.F.}\right) = 0.007 \, Ac.$$

Building Area/Concrete =
$$(397 \text{ S. F.}) \times \left(\frac{1 \text{ Ac.}}{43560 \text{ S. F.}}\right) = .009 \text{ Ac.}$$

Grass Area =
$$0.015 \, Ac. -0.02 \, Ac. -0.03 \, Ac. -0.007 \, Ac. -0.009 \, Ac. = 0.084 \, Ac.$$

Composite Runoff Coefficient:

$$C = \frac{\left[\left(C_{rock\; laydown}\; x\; Area\right) + \; \left(C_{rock\; road\; area}\; x\; Area\right) + \left(C_{pond\; area}\; x\; Area\right) + \left(C_{building}x\; Area\right) + \; \left(C_{grass}\; x\; Area\right)\right]}{Total\; Project\; Area}$$

$$C = \frac{\left[(0.5 \times 0.02 \, Ac.) + (0.7 \times 0.03 \, Ac.) + (1.0 \times 0.007 \, Ac.) + (1.0 \times 0.009 Ac.) + (0.17 \times 0.084 \, Ac.) \right]}{.15}$$

Total Treatment Volume from 1 inch of Rainfall:

Treatment Volume = $(C) \times (1 \text{ inch}) \times (Project Contributing area)$

Treatment Volume =
$$(.28) \times (1 \text{ in.}) \times (0.15 \text{Ac.}) \times \left(\frac{1 \text{Ft.}}{12 \text{ in.}}\right) = 0.0035 \text{ Ac.} - \text{Ft.}$$

Total Treatment Volume from ½ inch of Rainfall:

Treatment Volume = $(0.5 \text{ inch}) \times (Project Contributing area)$

Treatment Volume =
$$(0.5in.) \times (0.15Ac.) \times \left(\frac{1Ft.}{12 in.}\right) = 0.006Ac. -Ft.$$

The treatment volume for the project is the larger value, **0.006 Ac.-Ft**.





GEOTECHNICAL REPORT





NFRC REPEATER STATION MA-105



MADISON COUNTY, FLORIDA

MARCH 2020 BJR 19-198B





March 13, 2020

Mike Leahy, P.E. **Pickett & Associates** 5025 W. Grace Street Tampa, FL 33607

Geotechnical Exploration Report NFRC Repeater Station MA-105 Madison County, Florida BJR No. 19-198B

Dear Mr. Leahy:

BJ Rock, LLC (BJR) has completed the geotechnical exploration for the referenced project as authorized by Pickett & Associates for Gulf Power. The purposes of this study were to explore general subsurface conditions for the proposed staging areas and to use the data obtained to develop engineering recommendations to guide the design of the planned ponds/swales. This report describes our exploration procedure, presents the data obtained, and presents our conclusions and recommendations regarding the geotechnical engineering aspects of the design.

BJR appreciates the opportunity to participate in this project and we trust that the information included in this report is sufficient for your design. If you have any questions or comments concerning the contents of this report, please contact us.

Sincerely,

BJ Rock, LLC

BJR FL Certificate of Authorization No. 29100

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Definition 3 Soil Suitability Recommendations 4 Placement 4	
TESTING AND MONITORING	4
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ATTACHMENTS

Field Test Location Plan (Figure 1)
Soil Boring Logs (Figure 2)
Stormwater Pond Recovery Analysis Results
NRCS Soil Survey Data
Field Testing Standards and Procedures



PROJECT INFORMATION

Existing Site

Based on the information provided for our review from Pickett & Associates, we understand a repeater station area is planned off CR150, north of I-10 in Madison County, Florida (Figure 1).

Project Approach

The objective of the geotechnical investigation for the proposed project was to obtain information concerning the subsurface conditions in order to make geotechnical engineering estimates and recommendations in each of the following areas:

- Soil stratigraphy at the boring locations and the development of the approximate soil profile.
- General location and description of potentially deleterious materials which may interfere with construction or new structure performance, including buried or surficial existing fills, organics, construction debris, etc.
- Identification of some critical design or construction details, including present groundwater levels, estimated wet season levels, and seasonal fluctuations in the specified areas.

Scope of Work

In order to address the above objectives, our scope of work for this project included the following:

- Reviewed available published information on the site, including the United States
 Department of Agriculture (USDA) National Resources Conservation Service
 (NRCS) soil survey data for Madison County.
- Conducted a subsurface exploration program consisting of the advancement of auger borings with DRI / field permeability testing for the pond/swales, subsurface sampling, and field testing.
- Measured the stabilized groundwater levels at the boring locations.
- Reviewed and visually classified the recovered soils in the laboratory using the Unified Soil Classification System (ASTM D 2487). Developed the general soil stratigraphy at the boring locations.
- Performed geotechnical engineering studies and analyses in order to develop geotechnical engineering recommendations for each of the objectives previously discussed for the proposed project.
- Performed stormwater pond recovery analysis per referenced staging area.
 Analysis performed by our subconsultant, Native GeoSciences, Inc.
- Prepared a geotechnical report that summarizes the course of our study, the field and laboratory data generated, the subsurface conditions encountered, stormwater pond recovery analysis results and our geotechnical engineering recommendations for the proposed project.



Soil Survey Review

According to the USDA NRCS "Soil Survey of Madison County", the soil types generally present on the site are attached in the appendix and are generalized as follows: *Blanton sand, Albany sand and Plummer sand and Dorovan and Pamlico soils depressional.*

SUBSURFACE EXPLORATION

Field Exploration Procedures

The procedures used by BJ Rock, LLC for field sampling and testing are in general accordance with industry standards of care and established geotechnical engineering practice. BJR performed 3 auger borings to approximate depths of up to 5 feet each with 3 field permeability tests at the proposed locations.

Our staff located the staked borings in the field per the plans and field information provided by Pickett & Associates. The approximate testing locations are noted on the provided Field Test Location Plan (Figure 1) in the Appendix. The standards and procedures for the Standard Penetration Test (SPT) Boring and soil sample handling and classification are described in our Field Testing Standards and Procedures in the Appendix.

Field Exploration Results

Subsurface Conditions

The auger borings generally encountered fine to silty fine sands and sandy clays to an approximate depth of 5 feet below existing grade. The soil testing results are shown on the attached Soil Boring Logs (Figure 2) in the Appendix.

Field Permeability Test

The field permeability falling head tests were performed at the specified location on the site as shown on Figure 2 in the Appendix. The tests were performed at approximate depth of 1^{+/-} feet below existing grade. The tests were performed utilizing slotted casing seated in a uniform soil condition. The results of the tests are as follows:

Re	Recommended Existing Groundwater Parameters for Pond Design							
	STAGING AREAS - NFRC TRANSMISSION LINE FPL							
Test	Test Depth (ft) Vertical Infiltration Estimated Horizontal Infiltration (ft/day)* SHGWL Depth							
R-1	1	0.6	1.2	3				
R-2	1	1 0.9 1.8 3						
R-3	1 0.4 0.8 2							
*	Estimated horizontal permeability rate is 2x the vertical permeability test result.							
Note:	Horizontal and vertical permeability rates do not include a factor of safety.							

Groundwater

Groundwater was not encountered to an approximate depth of 5 feet below existing ground surface in the soil test borings performed in January 2020. Based on our past site experience, the results of our investigation, and our review of the NRCS soil survey, it is our opinion that the seasonal high

NFRC Repeater Station MA-105 Madison County, Florida BJR Job No. 19-198B Page 3



groundwater table will be encountered at an approximate depth of 2 to 3^{+/-} feet below existing ground surface in the areas of borings performed. Significant fluctuations in the groundwater levels should be expected due to seasonal variations in rainfall, runoff, and other site-specific factors across the site such as shallow perched conditions due to encountered clayey soils.

Stormwater Pond Recovery Analysis

Native GeoSciences (NGS) completed the stormwater pond recovery analysis for the staging area(s). NGS utilized the commercially available software PONDS (version 3.3) to perform the stormwater pond recovery analysis. The analysis included recovery of the treatment volume within 30 days. The description of the input parameters and a Copy of the PONDS software outputs are included in the Attachments in the Appendix.

SITE PREPARATION RECOMMENDATIONS

Site Stripping

Prior to any construction, the site must be properly prepared. To prepare the site for construction, all existing topsoil, muck, debris, vegetation, and large roots down to finger-size should be removed, including a 5-foot margin in a horizontal direction away from the footprints of the structures. The resulting excavations should be backfilled with soils as discussed in the structural fill section of this report.

Proofrolling

Following site stripping and any related excavation activity, and prior to any fill placement, proofrolling of the on-site soils should be performed. We recommend using a vibratory roller having a static weight of at least ten tons. Placement of fill materials may then proceed. Compaction of the fill materials should continue until the roller has made at least ten passes over all areas of the site and the soils appear to be relatively firm and unyielding. Half of the roller passes should be perpendicular to the direction of travel of the other passes. Proofrolling should be closely monitored by our engineering technician to look for unusual deflection of the soils beneath the compacting equipment. If unusual or excessive deflection is observed, the areas should be undercut to firm soils and backfilled with structural fill placed in maximum one-foot thick lifts. Backfill soils should be of the same composition and should be compacted to the same criteria as structural fill soils.

Structural Fill

Definition

Soil used for structural fill can be defined as clean fine sand containing less than twelve percent material by weight that is finer than a number 200 sieve (fines) (material conforming to SP to SP-SM in the Unified Soil Classification System) and less than 5 percent organics by weight. However, materials containing up to 25 percent fines (materials conforming to SC or SM in the Unified Soil Classification System) may be utilized as structural fill, if their plasticity index is less than 20 and the working subgrade is at least 2 feet above water or groundwater level.

If fill material with higher fines content is used (< 25 percent fines), the material will require the use of compaction equipment designed for clayey soils. This includes a sheeps foot or vibratory pad foot roller. In addition, a disk could be required to assist with drying the clayey soils in order to place them at or near their optimum moisture content. These materials must be placed in 6-inch thick maximum lifts so that they can be effectively compacted with a vibratory pad foot roller.

NFRC Repeater Station MA-105 Madison County, Florida BJR Job No. 19-198B Page 4



Soil Suitability Recommendations

Based on the results of the auger borings in Figure 3, the soil materials encountered in the borings appear to be acceptable general and/or structural fill from ground surface to 2 to 3⁺ feet below existing grade excluding any organic material, clays and unsuitable rock/shell/limestone, etc. Stratum 1 (SP/SP-SM) can be utilized as structural fill material. Stratum 2 (SM/SC) can be utilized as general fill material.

Placement

Fill should be placed in lifts not to exceed one foot thick. The fill material should be compacted to at least 95 percent of its modified Proctor maximum dry density (ASTM D 1557). Confined areas, such as utility trenches, should be compacted with manually operated vibratory compaction equipment.

TESTING AND MONITORING

Construction monitoring and testing are essential to proper site construction and performance. Compliance with the recommended foundation specification must be verified by our engineering technician familiar with the project construction. Observation of site preparation work is an integral part of the engineering recommendations contained in this report.

Safe working conditions are necessary. Temporary excavations should be sloped and/or braced as required by applicable local, state, and federal safety regulations, as well as the current Occupational Safety and Health Organization (OSHA) Excavation and Trench Safety Standards. Generally, the grading contractor is responsible for constructing stable, temporary excavations that are dewatered, shored, sloped and/or benched to maintain stability of the sides and bottom of the trench.

LIMITATIONS

This report has been prepared for the exclusive use of **Pickett & Associates and Gulf Power** for the specific application to the project previously discussed. Our conclusions and recommendations have been rendered using generally accepted standards of geotechnical engineering geology practice in the state of Florida. No other warranty is expressed or implied.

Our conclusions and recommendations are based on the design information furnished to us, the data obtained from the previously described subsurface exploration, and our experience. They do not reflect variations in the subsurface conditions that are likely to exist in the region of our boring and in unexplored areas of the site. These variations are due to the inherent variability of the subsurface conditions in this geologic region. Should variations become apparent during construction, it will be necessary to re-evaluate our conclusions and recommendations based upon our on-site observations of the conditions.

The site is underlain by limestone bedrock that is susceptible to dissolution and the subsequent development of karst features such as voids and sinkholes in the natural soil overburden. Construction in a sinkhole prone area is therefore accompanied by some risk that internal soil erosion and ground subsidence could affect new structures in the future. It is not possible to investigate or design to completely eliminate the possibility of future sinkhole-related problems. In any event, the Owner must understand and accept this risk.

The scope of our services does not include any environmental assessments or investigations for the possible presence of hazardous or toxic substances in the soil, groundwater, or surface water

NFRC Repeater Station MA-105 Madison County, Florida BJR Job No. 19-198B Page 5



within or in the general vicinity of the site studied. Any statements made in this report or shown on the test boring log regarding unusual subsurface conditions and/or composition, odor, staining, origin, or other characteristics of the surface and/or subsurface materials are strictly for the information of our client and may or may not be indicative of an environmental problem.

If changes are made in the overall design or the location of the proposed structure(s), the recommendations presented in this report must not be considered valid unless the changes are reviewed by our firm and recommendations modified or verified in writing. We should be given the opportunity to review the foundation plan and the applicable portions of the project specifications when the design is finalized. This review will allow us to check whether these documents are consistent with the intent of our recommendations.

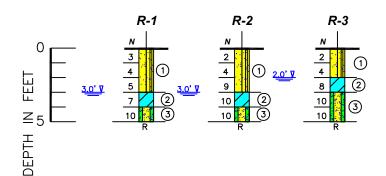






NFRC REPEATER STATION MA-105 FIELD TEST LOCATION PLAN MADISON COUNTY, FLORIDA

DATE: 03/10/20	SCALE: NOT TO SCALE	JOB NO. 19-198B
DRAWN BY: J.	FIGURE 1	
CK'D BY: B. JO		



LEGEND

1 = TAN, BROWN, ORANGE/BROWN FINE TO SLIGHTLY SILTY FINE SANDS (SP)/(SP-SM)

2 = ORANGE, BROWN SANDY CLAY (CL)

3 = DARK ORANGE, BROWN SILTY CEMENTED SANDS (SM)

(SP) = UNIFIED SOIL CLASSIFICATION GROUP SYMBOL

N= CORRELATED "N"-VALUE FROM CPT DEVICE

R = REFUSAL MATERIAL (CEMENTED SANDS)

0.0'T = ESTIMATED SEASONAL HIGH GROUNDWATER LEVEL

NOTES: HAND AUGER WITH CPT BORINGS PERFORMED JANUARY 21, 2020.

EXISTING GROUNDWATER LEVEL NOT ENCOUNTERED TO 5 FEET.



NFRC REPEATER STATION MA-105 SOIL BORING LOGS MADISON COUNTY, FL DATE: 1-23-20

SCALE: JOB NO.

AS SHOWN 19-198A

DRAWN BY: E. COLO'N
CK'D BY: J. PEAK

FIGURE 2 SHEET 1 OF 1 Stormwater Pond Recovery Analysis NFRC – Repeater Station March 13, 2020 Page 1 of 3

March 13, 2020

Re: Stormwater Pond Recovery Analysis

NFRC Repeater Station Madison County, Florida BJR Job No: 19-198(B)

As authorized, BJ Rock, LLC (BJR) has completed the stormwater pond recovery analysis for the above-referenced repeater station. The project site is located on SW Overstreet Avenue in Madison County, Florida.

We understand that one crushed rock area will be constructed along with one dry stormwater management pond within the proposed project. The pond will be constructed along the north and east boundaries of the project. The Repeater Station consists of one drainage basin (I).

We used soil and groundwater information collected during the geotechnical exploration on the site and provided in the BJR Geotechnical data. In addition, we used site survey data, crushed rock area design, and stormwater pond design information provided by Pickett Surveying and Engineering. We utilized the commercially available software PONDS (version 3.3) to perform the stormwater recovery analysis. Copies of the PONDS software outputs are included in the Attachments.

The PONDS software is generally limited to analyzing flat bottom stormwater ponds. Since the rock area is planned to be constructed at or above existing grade and will be sloping, it was necessary to analyze the area as a flat basin using average soil and groundwater parameters. We understand that you plan to utilize CR-PE Multi-Purpose Root & Water Barrier Molded Rolls by Century Products (or similar) to retain water within the rock area for recharge before discharging excess water to the pond. Based on this plan, it is our opinion that using average soil and groundwater parameters for this analysis is appropriate. Please note that the treatment volume was recovered within the rock basin area within 72 hours. Therefore, discharge and recovery within the stormwater pond was not needed.

Below are Average Soil and Groundwater Calculations and Model Input Parameters for the basin. We assumed a Base of Aquifer depth below the Seasonal High Water Table (SHWT) of 2 feet or less. This depth is generally conservative based on our experience with similar projects in soils with relatively high silt/clay content. The actual Base of Aquifer is likely deeper.

Lastly, we assumed a porosity of 35% for the crushed rock for void space storage.

<u>Stormwater Recovery Analysis – Repeater – Basin I</u>

Average Soil and Groundwater Calculations

Below are the average soil and groundwater calculations for the stormwater pond recovery analysis.

Repeater						
	Basin I					
	Crushed Rock Elevation					
Low El. (ft) High El. (ft) Average El. (ft.)						
97	97 98 97.5					
	Horizontal Saturated Hydraulic	Depth to				
Boring	Conductivity (ft/day)*	SHWT (ft)				
R-1	0.6	3				
R-2	0.9	3				
R-3 0.4 2						
AVG. 0.63 2.67						
Average SH	Average SHWT Elevation (ft)					
* Hydraulic conductivity values include a factor of safety of 3						

^{*} Hydraulic conductivity values include a factor of safety of 2 based on the field test results.

Model Input Parameters

Below are the input parameters used for the stormwater pond recovery analysis.

Aquifer and Geometry Data

Input Parameter	REPEATER - BASIN I			
Base of Aquifer Elevation (feet)	93.8			
Water Table Elevation (feet)	94.8			
Horizontal Saturated Hydraulic Conductivity (ft/day)*	0.63			
Fillable Porosity (%)	25			
Unsaturated Vertical Infiltration Rate (ft/day)*,**	0.316			
Maximum Area for Unsaturated Infiltration (ft ²) 340.6				
Equivalent Pond Length (ft)	34			
Equivalent Pond Width (ft) 10				
* Hydraulic conductivity values include a factor of safety of 2 based	on the field test results.			
** Unsaturated vertical Infiltration rate is 1/2 the field tested Horizo	ontal Saturated Hydraulic Conductivity rate.			

Stage vs Area Data for REPEATER - BASIN I

Stage (ft)	Area (ft²)
97.5	340.6
98	340.6

Stormwater Input Data

REPEATER	Hydrograph Type	slug load	
BASIN I	Treatment Volume (ft ³)	261.36	

Stormwater Pond Recovery Analysis NFRC – Repeater Station March 13, 2020 Page 3 of 3

Results

Based on the results of this analysis, the proposed crushed rock area recovers the associated treatment volume within 72 hours.

Closing

We appreciate the opportunity to be of service to you on this project and look forward to a continued relationship. Should you have any questions or concerns regarding this report, please feel free to call us at (407) 342-1443.

Sincerely,

Native Geoscience, Inc.

Certificate of Authorization No. 30474

John C. Diehl, P.G. Principal Geologist

P.G. 2460

Brian W. Jory, P.E. Principal Engineer P.E. 46634 3/13/20

Attachments:

PONDS Output – Repeater Station – Basin I – Rock Voids (7 pages)

Project Data

Project Name: NFRC Staging Area

Simulation Description: Repeater Station - Basin I - Rock Voids

Project Number: BJR 19-198A

Engineer: CW

Supervising Engineer: JCD

Date: 03-12-2020

Aquifer Data

Base Of Aquiter Elevation, [B]	(π datum):	93.80

Water Table Elevation, [WT] (ft datum): 94.80

Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day): 0.63

Fillable Porosity, [n] (%):

Unsaturated Vertical Infiltration Rate, [Iv] (ft/day): 0.316

Maximum Area For Unsaturated Infiltration, [Av] (ft²): 340.6

Geometry Data

Equivalent Pond Length, [L] (ft): 34.0

Equivalent Pond Width, [W] (ft): 10.0

Ground water mound is expected to intersect the pond bottom

Stage vs Area Data

Stage	Area		
(ft datum)	(ft²)		
97.50	340.6		
98.00	340.6		

Ditch Data

Ditch (or interceptor trench) parallel to length axis is inactive

Ditch (or interceptor trench) parallel to width axis is inactive

Discharge Structures

Discharge Structure #1 is inactive

Discharge Structure #2 is inactive

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Discharge Structures (cont'd.)

Discharge Structure #3 is inactive

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PONDS Version 3.3.0278 **Retention Pond Recovery - Refined Method** Copyright 2012

Devo Seereeram, Ph.D., P.E.

Scenario Input Data

Scenario 1 :: 261.36 ft³ slug load

Slug Load

Hydrograph Type: Modflow Routing: Routed with infiltration

Treatment Volume (ft³) 261.36

Initial ground water level (ft datum) 94.80 (default)

| Time After
Storm Event
(days) |
|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|
| 0.100 | 4.000 | 8.500 | 16.000 | 25.000 |
| 0.250 | 4.500 | 9.000 | 17.000 | 26.000 |
| 0.500 | 5.000 | 9.500 | 18.000 | 27.000 |
| 1.000 | 5.500 | 10.000 | 19.000 | 28.000 |
| 1.500 | 6.000 | 11.000 | 20.000 | 29.000 |
| 2.000 | 6.500 | 12.000 | 21.000 | 30.000 |
| 2.500 | 7.000 | 13.000 | 22.000 | |
| 3.000 | 7.500 | 14.000 | 23.000 | |
| 3.500 | 8.000 | 15.000 | 24.000 | |

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Detailed Results :: Scenario 1 :: 261.36 ft³ slug load

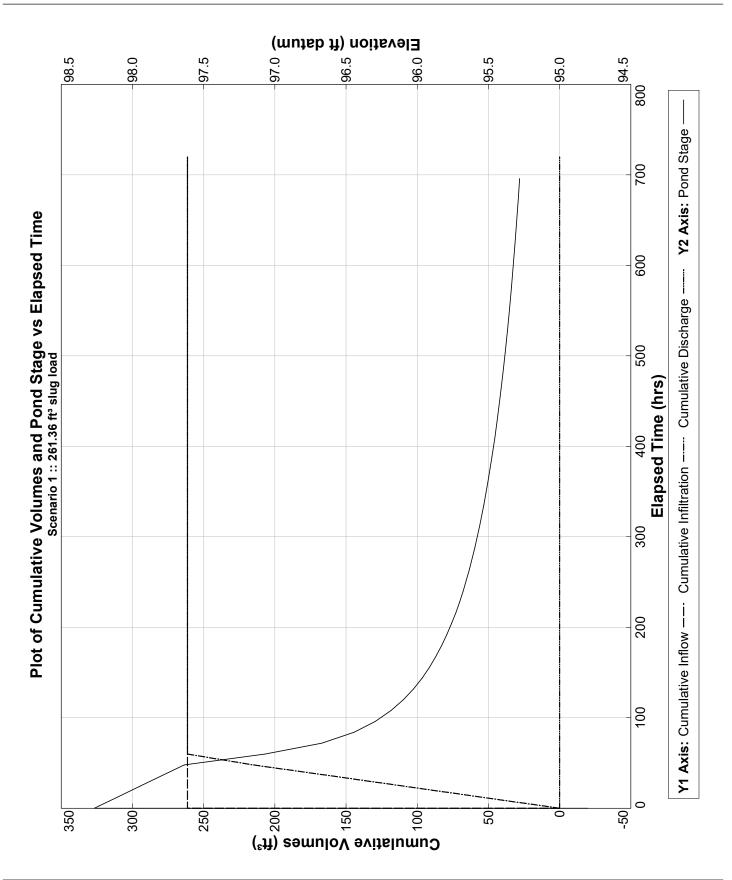
Elapsed Time (hours)	Instantaneous Inflow Rate (ft³/s)	Outside Recharge (ft/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Combined Instantaneous Discharge Rate (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft³)	Combined Cumulative Discharge (ft³)	Flow Type
0.000	43.5600	0.00000	94.80000	0.00000	0	0.000	0.0	0	N.A.
0.002	43.5600	0.00000	98.26744	0.00125	0	261.360	0.0	0	U/P
2.400	0.0000	0.00000	98.23586	0.00125	0	261.360	10.8	0	U/P
6.000	0.0000	0.00000	98.18846	0.00125	0	261.360	26.9	0	U/P
12.000	0.0000	0.00000	98.10947	0.00125	0	261.360	53.8	0	U/P
24.000	0.0000	0.00000	97.95146	0.00125	0	261.360	107.6	0	U/P
36.000	0.0000	0.00000	97.79346	0.00125	Ö	261.360	161.4	0	U/P
48.000	0.0000	0.00000	97.63547	0.00126	0	261.360	215.2	0	U/P
60.000	0.0000	0.00000	97.06869	0.00053	0	261.360	261.4	0	U/S
72.000	0.0000	0.00000	96.66942	0.00000	0	261.360	261.4	0	S
84.000	0.0000	0.00000	96.44394	0.00000	0	261.360	261.4	0	S
96.000	0.0000	0.00000	96.29443	0.00000	0	261.360	261.4	0	S
108.000	0.0000	0.00000	96.18405	0.00000	0	261.360	261.4	0	S
120.000	0.0000	0.00000	96.09710	0.00000	0	261.360	261.4	0	s
132.000	0.0000	0.00000	96.02574	0.00000	Ö	261.360	261.4	0	Š
144.000	0.0000	0.00000	95.96549	0.00000	Ö	261.360	261.4	Ö	Š
156.000	0.0000	0.00000	95.91357	0.00000	Ö	261.360	261.4	0	Š
168.000	0.0000	0.00000	95.86810	0.00000	0	261.360	261.4	0	S
180.000	0.0000	0.00000	95.82778	0.00000	0	261.360	261.4	0	S
192.000	0.0000	0.00000	95.79166	0.00000	0	261.360	261.4	0	99999999999
204.000	0.0000	0.00000	95.75903	0.00000	0	261.360	261.4	0	S
216.000	0.0000	0.00000	95.72931	0.00000	Ő	261.360	261.4	0	S
228.000	0.0000	0.00000	95.70209	0.00000	Ö	261.360	261.4	Ö	Š
240.000	0.0000	0.00000	95.67701	0.00000	Ő	261.360	261.4	Ö	Š
264.000	0.0000	0.00000	95.63358	0.00000	Ö	261.360	261.4	Ö	Š
288.000	0.0000	0.00000	95.59546	0.00000	Ö	261.360	261.4	Ö	Š
312.000	0.0000	0.00000	95.56165	0.00000	0	261.360	261.4	0	Š
336.000	0.0000	0.00000	95.53137	0.00000	Ö	261.360	261.4	Ö	S S
360.000	0.0000	0.00000	95.50408	0.00000	Ö	261.360	261.4	Ö	Š
384.000	0.0000	0.00000	95.47925	0.00000	Ö	261.360	261.4	Ö	Š
408.000	0.0000	0.00000	95.45646	0.00000	Ö	261.360	261.4	Ö	S S S
432.000	0.0000	0.00000	95.43568	0.00000	Ö	261.360	261.4	Ö	Š
456.000	0.0000	0.00000	95.41640	0.00000	Ö	261.360	261.4	Ö	Š
480.000	0.0000	0.00000	95.39864	0.00000	Ö	261.360	261.4	Ö	Š
504.000	0.0000	0.00000	95.38205	0.00000	0	261.360	261.4	0	S
528.000	0.0000	0.00000	95.36664	0.00000	Ö	261.360	261.4	Ö	Š
552.000	0.0000	0.00000	95.35211	0.00000	Ö	261.360	261.4	Ö	Š
576.000	0.0000	0.00000	95.33855	0.00000	Ö	261.360	261.4	Ö	Š
600.000	0.0000	0.00000	95.32574	0.00000	Ö	261.360	261.4	Ö	Š
624.000	0.0000	0.00000	95.31371	0.00000	Ö	261.360	261.4	Ö	Š
648.000	0.0000	0.00000	95.30229	0.00000	Ö	261.360	261.4	Ö	Š
672.000	0.0000	0.00000	95.29151	0.00000	Ö	261.360	261.4	Ö	Š
696.000	0.0000	0.00000	95.28124	0.00000	0	261.360	261.4	0	Š
720.000	0.0000	0.00000	95.27152			261.360	261.4	Ö	N.A.

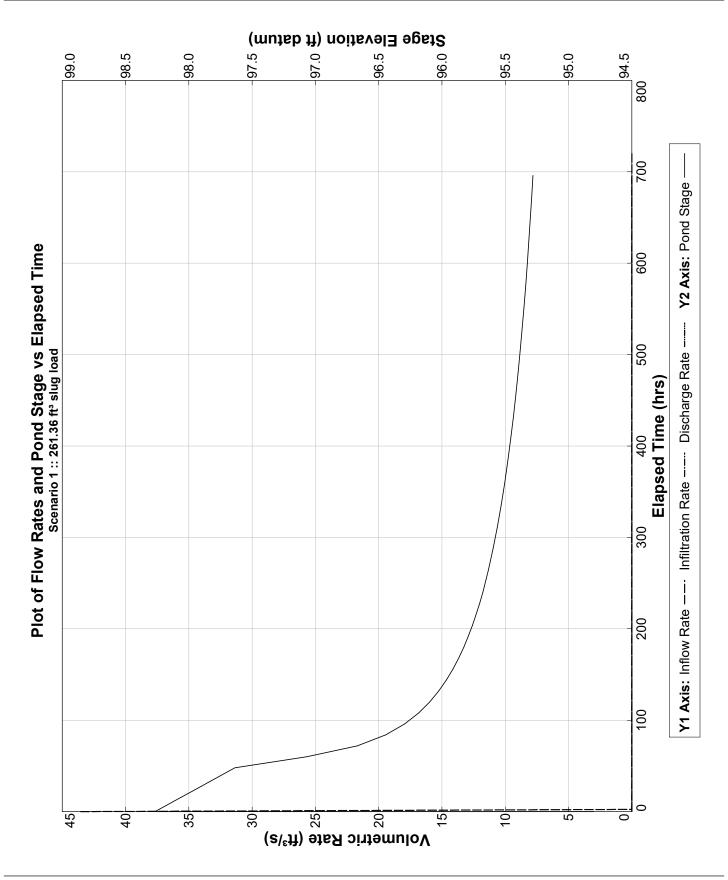
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Summary of Results :: Scenario 1 :: 261.36 ft³ slug load

	Time (hours)	Stage (ft datum)	Rate (ft³/s)	Volume (ft³)
Stage Minimum Maximum	0.000 0.002	94.80 98.27		
Inflow Rate - Maximum - Positive Rate - Maximum - Negative Cumulative Volume - Maximum Positive Cumulative Volume - Maximum Negative Cumulative Volume - End of Simulation	0.002 None 0.002 None 720.000		43.5600 None	261.4 None 261.4
Infiltration Rate - Maximum - Positive Rate - Maximum - Negative Cumulative Volume - Maximum Positive Cumulative Volume - Maximum Negative Cumulative Volume - End of Simulation	0.002 None 60.000 None 720.000		0.0012 None	261.4 None 261.4
Combined Discharge Rate - Maximum - Positive Rate - Maximum - Negative Cumulative Volume - Maximum Positive Cumulative Volume - Maximum Negative Cumulative Volume - End of Simulation	None None None 720.000		None None	None None 0.0
Discharge Structure 1 - inactive Rate - Maximum - Positive Rate - Maximum - Negative Cumulative Volume - Maximum Positive Cumulative Volume - Maximum Negative Cumulative Volume - End of Simulation	disabled disabled disabled disabled disabled		disabled disabled	disabled disabled disabled
Discharge Structure 2 - inactive Rate - Maximum - Positive Rate - Maximum - Negative Cumulative Volume - Maximum Positive Cumulative Volume - Maximum Negative Cumulative Volume - End of Simulation	disabled disabled disabled disabled disabled		disabled disabled	disabled disabled disabled
Discharge Structure 3 - inactive Rate - Maximum - Positive Rate - Maximum - Negative Cumulative Volume - Maximum Positive Cumulative Volume - Maximum Negative Cumulative Volume - End of Simulation	disabled disabled disabled disabled disabled		disabled disabled	disabled disabled disabled
Pollution Abatement: 36 Hour Stage and Infiltration Volume 72 Hour Stage and Infiltration Volume	36.000 72.000	97.79 96.67		161.4 261.4

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MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

36

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

۵

Landfill



Lava Flow Marsh or swamp



Mine or Quarry



Miscellaneous Water Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

0

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

â

Spoil Area Stony Spot

00

Very Stony Spot

Wet Spot Other

Δ

Special Line Features

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15.800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Madison County, Florida Survey Area Data: Version 14, Sep 17, 2019

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Dec 16. 2014—Dec 9. 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
2	Albany sand, 0 to 5 percent slopes	4.5	8.1%
5	Blanton sand, 0 to 5 percent slopes	10.7	19.0%
23	Plummer sand	14.0	24.9%
26	Troup sand, 0 to 5 percent slopes	0.2	0.4%
65	Lovett sand, 0 to 5 percent slopes	0.1	0.1%
74	Dorovan and Pamlico soils, depressional	26.7	47.5%
Totals for Area of Interest	'	56.2	100.0%

Madison County, Florida

2—Albany sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w4gt

Elevation: 20 to 350 feet

Mean annual precipitation: 49 to 63 inches Mean annual air temperature: 63 to 73 degrees F

Frost-free period: 241 to 306 days

Farmland classification: Not prime farmland

Map Unit Composition

Albany and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Albany

Setting

Landform: Knolls on marine terraces, rises on marine terraces

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve, talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 10 inches: sand E - 10 to 50 inches: sand

Bt - 50 to 80 inches: sandy clay loam

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.60 to 1.98 in/hr) Depth to water table: About 12 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Very low (about 2.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: A/D

Forage suitability group: Sandy soils on rises and knolls of mesic

uplands (G133AA131FL)

Hydric soil rating: No

Minor Components

Blanton

Percent of map unit: 5 percent

Landform: Knolls on marine terraces, ridges on marine terraces

Landform position (two-dimensional): Shoulder

Landform position (three-dimensional): Side slope, interfluve

Down-slope shape: Convex Across-slope shape: Linear

Hydric soil rating: No

Plummer

Percent of map unit: 5 percent

Landform: Drainageways on marine terraces Landform position (three-dimensional): Talf

Down-slope shape: Concave, linear

Across-slope shape: Linear Hydric soil rating: No

Data Source Information

Soil Survey Area: Madison County, Florida Survey Area Data: Version 14, Sep 17, 2019

Madison County, Florida

5—Blanton sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2w4gr Elevation: 100 to 400 feet

Mean annual precipitation: 40 to 69 inches Mean annual air temperature: 52 to 72 degrees F

Frost-free period: 190 to 310 days

Farmland classification: Not prime farmland

Map Unit Composition

Blanton and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Blanton

Setting

Landform: Knolls on marine terraces, interfluves, ridges on marine

terraces

Landform position (two-dimensional): Shoulder

Landform position (three-dimensional): Side slope, interfluve

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy and loamy marine deposits

Typical profile

Ap - 0 to 12 inches: sand E1 - 12 to 37 inches: sand E2 - 37 to 53 inches: sand E3 - 53 to 69 inches: sand Bt - 69 to 80 inches: sandy loam

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High

(1.98 to 5.95 in/hr)

Depth to water table: About 48 to 80 inches

Frequency of flooding: None Frequency of ponding: None

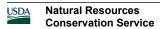
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Available water storage in profile: Very low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified



Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Forage suitability group: Sandy soils on rises, knolls, and ridges of

mesic uplands (G133AA121FL)

Hydric soil rating: No

Minor Components

Albany

Percent of map unit: 5 percent Landform: Flats, interfluves

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

Fuquay

Percent of map unit: 5 percent

Landform: Interfluves

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Bonifay

Percent of map unit: 4 percent

Landform: Knolls on marine terraces, ridges on marine terraces

Landform position (two-dimensional): Summit

Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Alpin

Percent of map unit: 3 percent

Landform: Flats on marine terraces, knolls on marine terraces,

ridges on marine terraces

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, talf

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Ocilla

Percent of map unit: 3 percent Landform: Stream terraces

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex Across-slope shape: Linear

Hydric soil rating: No

Data Source Information

Soil Survey Area: Madison County, Florida Survey Area Data: Version 14, Sep 17, 2019

Madison County, Florida

23—Plummer sand

Map Unit Setting

National map unit symbol: 1hbb4

Elevation: 20 to 400 feet

Mean annual precipitation: 49 to 57 inches Mean annual air temperature: 64 to 72 degrees F

Frost-free period: 262 to 292 days

Farmland classification: Not prime farmland

Map Unit Composition

Plummer and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Plummer

Setting

Landform: Flats on marine terraces, drainageways on marine

terraces

Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 7 inches: sand E - 7 to 57 inches: sand

Btg - 57 to 80 inches: fine sandy loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.57 to 1.98 in/hr) Depth to water table: About 6 to 18 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 3.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: A/D

Forage suitability group: sandy soils on flats of mesic or hydric

lowlands (G133AA141FL)

Hydric soil rating: No

Minor Components

Chipley

Percent of map unit: 5 percent

Landform: Flats on marine terraces, knolls on marine terraces,

rises on marine terraces

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Surrency, depressional

Percent of map unit: 5 percent

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Madison County, Florida Survey Area Data: Version 14, Sep 17, 2019

Madison County, Florida

74—Dorovan and Pamlico soils, depressional

Map Unit Setting

National map unit symbol: 1hbc3

Elevation: 10 to 450 feet

Mean annual precipitation: 49 to 57 inches Mean annual air temperature: 64 to 72 degrees F

Frost-free period: 262 to 292 days

Farmland classification: Not prime farmland

Map Unit Composition

Dorovan and similar soils: 58 percent Pamlico and similar soils: 31 percent Minor components: 11 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Dorovan

Setting

Landform: Depressions on marine terraces

Landform position (three-dimensional): Interfluve, talf

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Organic material over sandy marine deposits

Typical profile

Oe - 0 to 6 inches: muck Oa - 6 to 70 inches: muck C - 70 to 80 inches: sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.57 to 1.98 in/hr) Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: Frequent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Very high (about 20.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: B/D

Forage suitability group: Organic soils in depressions and on flood

plains (G133AA645FL)

Hydric soil rating: Yes

Description of Pamlico

Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Herbaceous organic material over sandy marine

deposits

Typical profile

Oa - 0 to 33 inches: muck C1 - 33 to 60 inches: sand

C2 - 60 to 80 inches: sandy clay loam

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.57 to 5.95 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Very high (about 12.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: A/D

Forage suitability group: Organic soils in depressions and on flood

plains (G133AA645FL)

Hydric soil rating: Yes

Minor Components

Sapelo, hydric

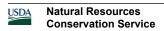
Percent of map unit: 4 percent Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Plummer, depressional

Percent of map unit: 4 percent



Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Surrency, depressional

Percent of map unit: 3 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Madison County, Florida Survey Area Data: Version 14, Sep 17, 2019



FIELD TESTING STANDARDS AND PROCEDURES

Standard Penetration Test (SPT) Boring

The SPT borings were advanced by means of a truck or track mounted drill rig employing wet rotary drilling techniques. The SPT testing was performed continuously in the upper ten feet and at five-foot intervals thereafter. The soil samples were obtained at the depths where the SPT testing was performed. The soil samples were then classified in the field, placed in sealed containers, and returned to our laboratory for further evaluation by a geotechnical engineer.

The SPT borings were performed in general compliance with standard field penetration test procedures (ASTM D 1586-99). After drilling to the sampling depth and flushing the borehole, the standard two-inch O.D. split-barrel sampler was seated by driving it six inches into the undisturbed soil at the bottom of the borehole. The sampler was then driven an additional 12 inches by a 140-pound hammer falling 30 inches. The number of blows required to produce the 12 inches of penetration is recorded as the standard penetration test value (N). These values are plotted on the left side of the boring log Figure 3.

In the upper ten feet sampling was performed by driving the split-barrel sampler 24 inches and the blows required to drive the sampler the middle two 6-inch increments were recorded as the "N" value. Through this technique, the upper ten feet of the soil was sampled continuously. Detailed descriptions of the soils encountered during the advancement of the SPT boring are presented in the Boring Logs.

Soil Sample Handling and Classification

The soil samples obtained from the SPT borings were placed in sealed containers to retain moisture and returned to our laboratory. The samples were then reviewed by a geotechnical engineer to confirm classifications, visually estimate the relative percentages of the soil's constituents (sand, clay, etc.), and identify pertinent structural features. We visually classified the soils according to the Unified Soil Classification System (ASTM D 2487). The stratification lines shown on the boring logs in Figure 3 represent our interpretation of approximate boundaries between soil types. The transition between strata may be gradual. Our classifications are based on a visual estimation of the soil properties and our engineering experience with the soils found in this geologic area.

The SPT "N" values are presented adjacent along the left side of the boring logs. The correlation of the SPT "N" values with relative density, unconfined compressive strength, and consistency are provided in the following table:

Coarse-Gra	ined Soils	Fine Grained Soils				
Penetration Resistance N (blows/ft)	Relative Density of Sand	Penetration Resistance N (blows/ft)	Unconfined Compressive Strength of Clay (tons/ft²)	Consistency of Clay		
0-4	Very Loose	<2	<0.25	Very Soft		
4-10	Loose	2-4	0.25-0.50	Soft		
10-30	Medium-Dense	4-8	0.50-1.00	Medium		
30-50	30-50 Dense		1.00-2.00	Stiff		
>50	>50 Very Dense		2.00-4.00	Very Stiff		
	,		>4.00	Hard		

Hand Auger Borings

The auger borings were performed with a manually advanced hand auger. The auger was advanced by rotating it into the ground in approximate 6-inch increments. After each incremental penetration, the auger was retracted, and the soils collected in the auger bucket were placed in sealed containers. The samples were then reviewed by a geotechnical engineer and classified as described above. Detailed descriptions of the soils encountered in the auger borings are presented in the Auger Boring Logs.

Appendix B – HydroCAD Report

PRE-DEVELOPED SITE **1S** Pre-Developed Basin I Outfall **POST DEVELOPED** SITE 6L Split Rock Void Post Developed Basin I North Pond 5P 10L South Pond **Combined Outflow**









Type II 24-hr 3 DAY-100YR. Rainfall=12.40"

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Page 3

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>6.39"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=1.59 cfs 0.074 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>8.27"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=1.84 cfs 0.095 af

Pond 4P: Rock Void

Peak Elev=98.04' Storage=170 cf Inflow=0.92 cfs 0.048 af

Outflow=0.91 cfs 0.044 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.046 af Inflow=0.92 cfs 0.048 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=97.03' Storage=59 cf Inflow=0.91 cfs 0.044 af

Outflow=0.91 cfs 0.043 af

Link 2L: Outfall

Inflow=1.59 cfs 0.074 af Primary=1.59 cfs 0.074 af

Link 6L: Split

x 0.50 Inflow=1.84 cfs 0.095 af

Primary=0.92 cfs 0.048 af Secondary=0.92 cfs 0.048 af

Link 10L: Combined Outflow

Inflow=0.91 cfs 0.043 af Primary=0.91 cfs 0.043 af

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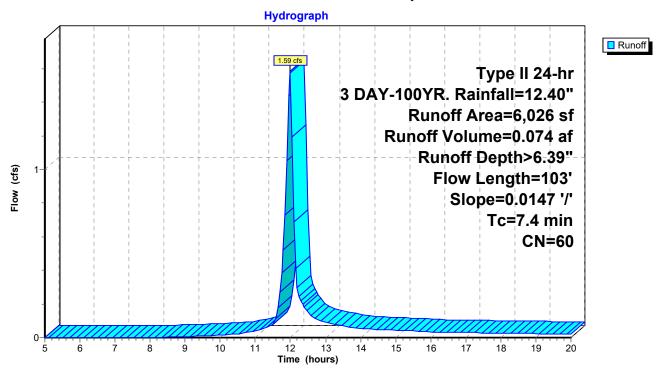
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 1.59 cfs @ 11.99 hrs, Volume= 0.074 af, Depth> 6.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 3 DAY-100YR. Rainfall=12.40"

	Α	rea (sf)	CN [Description								
*		6,026	60 V	60 Woods/grass comb., Poor, HSG B								
		6,026 100.00% Pervious Area										
	Tc	Length	Slope	,	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	7.4	103	0.0147	0.23		Lag/CN Method, Woods						

Subcatchment 1S: Pre-Developed Basin I



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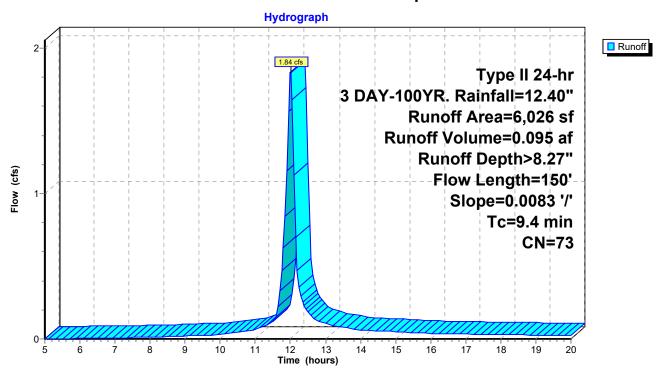
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 1.84 cfs @ 12.00 hrs, Volume= 0.095 af, Depth> 8.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 3 DAY-100YR. Rainfall=12.40"

	Aı	rea (sf)	CN I	Description								
		300	98	Roofs, HSG B								
		97	98 I	Paved parking, HSG B								
*		973	65	Uncompacted Gravel 35% Void								
		1,283	85	Gravel road	ls, HSG B							
		3,373	67 I	Brush, Poo	r, HSG B							
		6,026	73 \	Weighted A	verage							
		5,629	9	93.41% Pei	rvious Area							
		397	(6.59% Impe	ervious Area	a						
	Тс	Length	Slope	ope Velocity Capacity Description								
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	9.4	150	0.0083	0.27		Lag/CN Method,						

Subcatchment 3S: Post Developed Basin I



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Summary for Pond 4P: Rock Void

Inflow = 0.92 cfs @ 12.00 hrs, Volume= 0.048 af

Outflow = 0.91 cfs @ 12.01 hrs, Volume= 0.044 af, Atten= 1%, Lag= 0.1 min

Primary = 0.91 cfs @ 12.01 hrs, Volume= 0.044 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.04' @ 12.01 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 47.0 min calculated for 0.044 af (91% of inflow)

Center-of-Mass det. time= 18.0 min (782.9 - 764.8)

Volume	Inv	ert Avail.S	Storage	ge Storage Description		
#1	97.	50'	170 cf		stage Data (Perall x 35.0%	rismatic)Listed below (Recalc) Voids
Elevation (fee		Surf.Area (sq-ft)		Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	Inve	rt Outl	et Devices		
#1	Primary	98.0	Hea	d (feet) 0.2	0.40 0.60	road-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32

Primary OutFlow Max=0.90 cfs @ 12.01 hrs HW=98.04' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.90 cfs @ 0.54 fps)

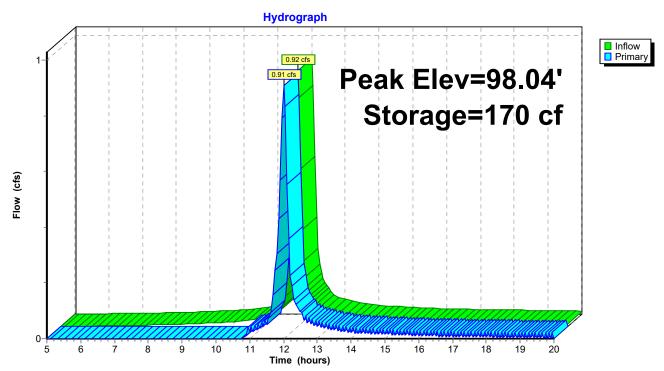
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Pond 4P: Rock Void



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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 4.14" for 3 DAY-100YR. event

Inflow = 0.92 cfs @ 12.00 hrs, Volume= 0.048 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 20.00 hrs Surf.Area= 61.115 ac Storage= 0.046 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert A	Avail.Storage	Storage Descri	ption
#1	96.00'	356.830 a	Custom Stage	Data (Prismatic)Listed below (Recalc)
Elevatior (feet				
96.00	60.960) (000 0.	000
97.00	265.600	163	280 163.	280
98.00	121.500) 193	550 356.	830
	Routing Primary		tlet Devices	ng x 1.00' rise Sharp-Crested Vee/Trap Weir
π1	i ililiai y		= 2.49 (C= 3.11)	•

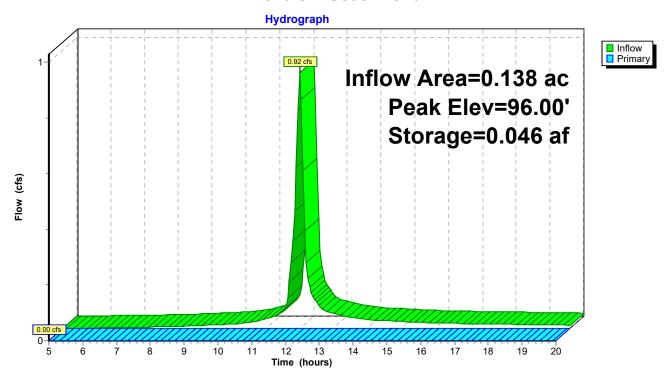
Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 3 DAY-100YR. Rainfall=12.40"

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Summary for Pond 9P: North Pond

Inflow = 0.91 cfs @ 12.01 hrs, Volume= 0.044 af

Outflow = 0.91 cfs @ 12.01 hrs, Volume= 0.043 af, Atten= 0%, Lag= 0.2 min

Primary = 0.91 cfs @ 12.01 hrs, Volume= 0.043 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.03' @ 12.01 hrs Surf.Area= 147 sf Storage= 59 cf

Plug-Flow detention time= 11.7 min calculated for 0.043 af (98% of inflow)

Center-of-Mass det. time= 3.3 min (786.2 - 782.9)

Volume	Inv	ert Avail	.Storage	Storage	Description	
#1	96.	50'	209 cf	Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
96.5	0	72		0	0	
97.0	0	147		55	55	
98.0	0	162		155	209	
Device	Routing	lnv	ert Outl	let Device	s	
#1	Primary	96.		.0 deg x 6 2.49 (C=		rise Sharp-Crested Vee/Trap Weir

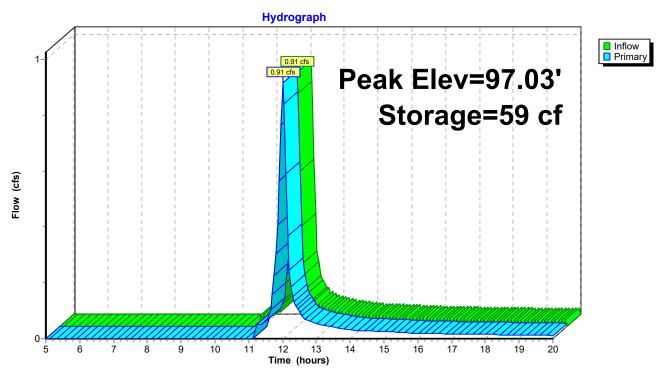
Primary OutFlow Max=0.90 cfs @ 12.01 hrs HW=97.03' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Weir Controls 0.90 cfs @ 1.12 fps)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

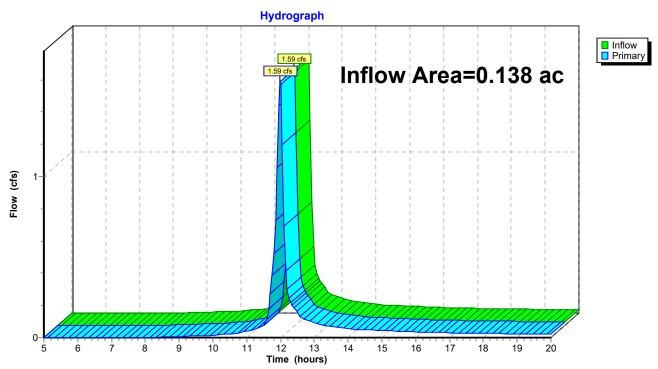
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 6.39" for 3 DAY-100YR. event

Inflow = 1.59 cfs @ 11.99 hrs, Volume= 0.074 af

Primary = 1.59 cfs @ 11.99 hrs, Volume= 0.074 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 8.27" for 3 DAY-100YR. event

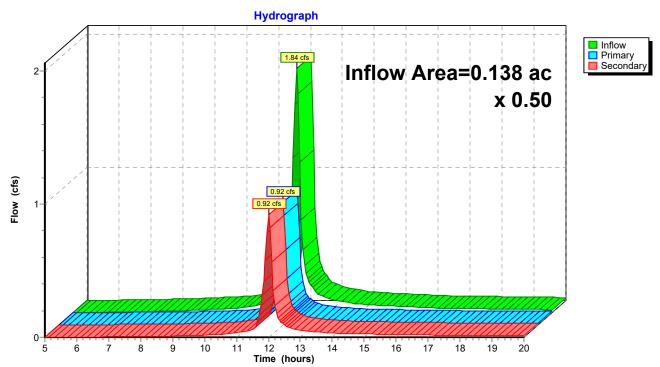
Inflow = 1.84 cfs @ 12.00 hrs, Volume= 0.095 af

Primary = 0.92 cfs @ 12.00 hrs, Volume= 0.048 af, Atten= 50%, Lag= 0.0 min

Secondary = 0.92 cfs @ 12.00 hrs, Volume= 0.048 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

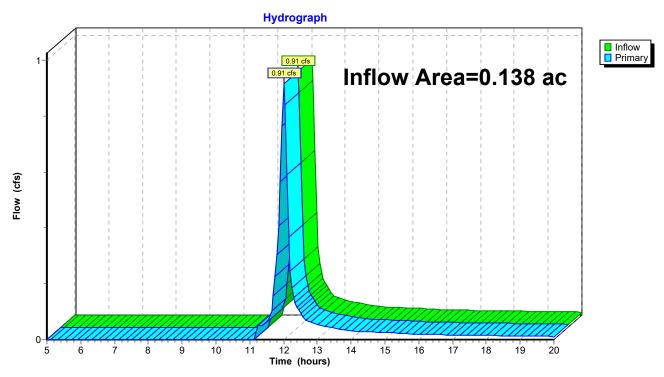
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 3.72" for 3 DAY-100YR. event

Inflow = 0.91 cfs @ 12.01 hrs, Volume= 0.043 af

Primary = 0.91 cfs @ 12.01 hrs, Volume= 0.043 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 7 DAY-100YR Rainfall=14.00"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>7.70"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=1.89 cfs 0.089 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>9.71"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=2.13 cfs 0.112 af

Pond 4P: Rock Void

Peak Elev=98.04' Storage=170 cf Inflow=1.07 cfs 0.056 af

Outflow=1.06 cfs 0.052 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.054 af Inflow=1.07 cfs 0.056 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=97.05' Storage=61 cf Inflow=1.06 cfs 0.052 af

Outflow=1.06 cfs 0.051 af

Link 2L: Outfall

Inflow=1.89 cfs 0.089 af Primary=1.89 cfs 0.089 af

Link 6L: Split

x 0.50 Inflow=2.13 cfs 0.112 af

Primary=1.07 cfs 0.056 af Secondary=1.07 cfs 0.056 af

Link 10L: Combined Outflow

Inflow=1.06 cfs 0.051 af Primary=1.06 cfs 0.051 af

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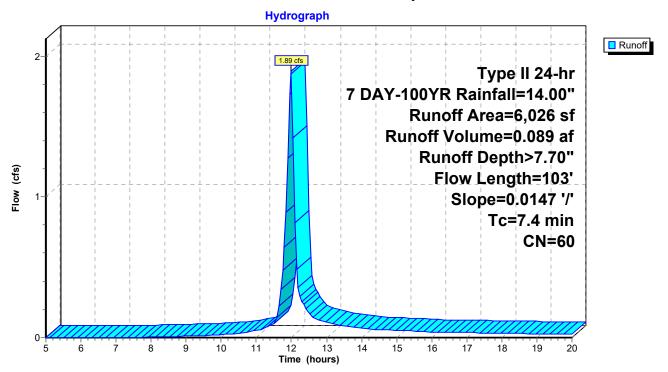
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 1.89 cfs @ 11.99 hrs, Volume= 0.089 af, Depth> 7.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 7 DAY-100YR Rainfall=14.00"

	Α	rea (sf)	CN [Description								
*		6,026	60 V	60 Woods/grass comb., Poor, HSG B								
		6,026 100.00% Pervious Area										
	Tc	Length	Slope	,	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	7.4	103	0.0147	0.23		Lag/CN Method, Woods						

Subcatchment 1S: Pre-Developed Basin I



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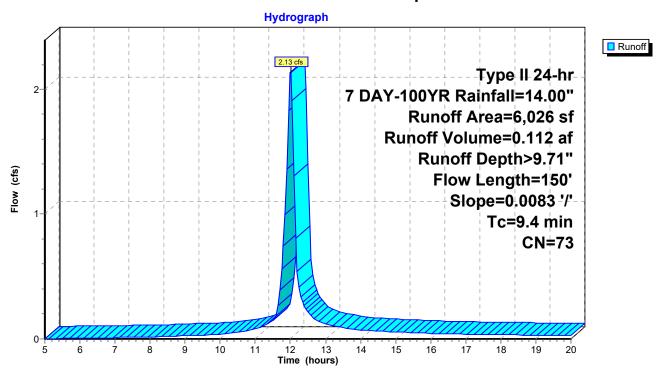
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 2.13 cfs @ 12.00 hrs, Volume= 0.112 af, Depth> 9.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 7 DAY-100YR Rainfall=14.00"

	Aı	rea (sf)	CN I	Description								
		300	98	Roofs, HSG B								
		97	98 I	Paved parking, HSG B								
*		973	65	Uncompacted Gravel 35% Void								
		1,283	85	Gravel road	ls, HSG B							
		3,373	67 I	Brush, Poo	r, HSG B							
		6,026	73 \	Weighted A	verage							
		5,629	9	93.41% Pei	rvious Area							
		397	(6.59% Impe	ervious Area	a						
	Тс	Length	Slope	ope Velocity Capacity Description								
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	9.4	150	0.0083	0.27		Lag/CN Method,						

Subcatchment 3S: Post Developed Basin I



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Summary for Pond 4P: Rock Void

Inflow = 1.07 cfs @ 12.00 hrs, Volume= 0.056 af

Outflow = 1.06 cfs @ 12.00 hrs, Volume= 0.052 af, Atten= 0%, Lag= 0.0 min

Primary = 1.06 cfs @ 12.00 hrs, Volume= 0.052 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.04' @ 12.00 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 42.9 min calculated for 0.052 af (93% of inflow)

Center-of-Mass det. time= 17.5 min (778.7 - 761.2)

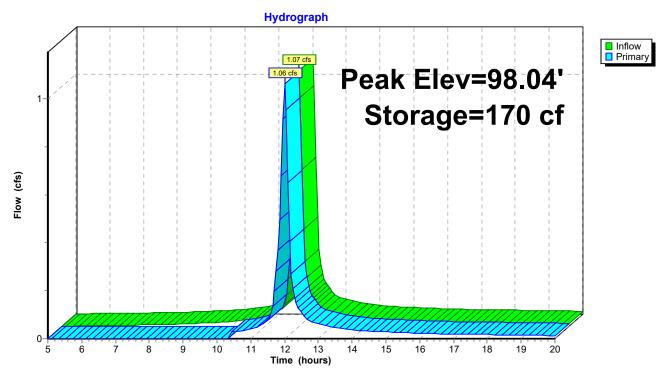
Volume	Inv	ert Avail.	Storage	Storage D	escription	
#1 97.50' 17		170 cf		stage Data (Perall x 35.0%	rismatic)Listed below (Recalc) Voids	
Elevatio		Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	Inve	ert Outl	et Devices		
#1	Primary	98.0	Hea	d (feet) 0.2	0.40 0.60	road-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32

Primary OutFlow Max=1.05 cfs @ 12.00 hrs HW=98.04' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 1.05 cfs @ 0.57 fps)

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Pond 4P: Rock Void



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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 4.85" for 7 DAY-100YR event

Inflow = 1.07 cfs @ 12.00 hrs, Volume= 0.056 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 20.00 hrs Surf.Area= 61.142 ac Storage= 0.054 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

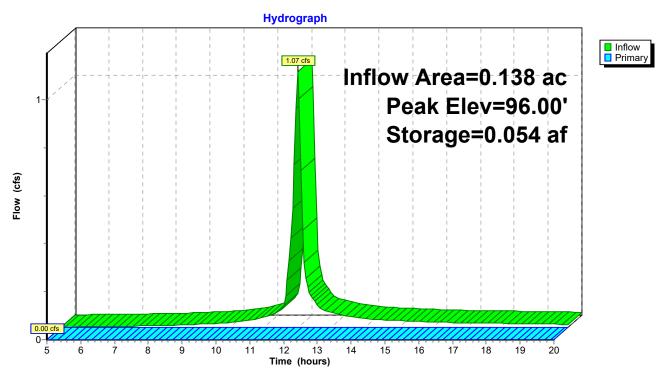
Volume	Invert A	Avail.Storage	Storage Descri	ption
#1	96.00'	356.830 a	Custom Stage	Data (Prismatic)Listed below (Recalc)
Elevatior (feet				
96.00	60.960) (000 0.	000
97.00	265.600	163	280 163.	280
98.00	121.500) 193	550 356.	830
	Routing Primary		tlet Devices	ng x 1.00' rise Sharp-Crested Vee/Trap Weir
π1	i ililiai y		= 2.49 (C= 3.11)	•

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



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Summary for Pond 9P: North Pond

Inflow = 1.06 cfs @ 12.00 hrs, Volume= 0.052 af

Outflow = 1.06 cfs @ 12.01 hrs, Volume= 0.051 af, Atten= 0%, Lag= 0.2 min

Primary = 1.06 cfs @ 12.01 hrs, Volume= 0.051 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.05' @ 12.01 hrs Surf.Area= 148 sf Storage= 61 cf

Plug-Flow detention time= 10.4 min calculated for 0.051 af (98% of inflow) Center-of-Mass det. time= 3.1 min (781.8 - 778.7)

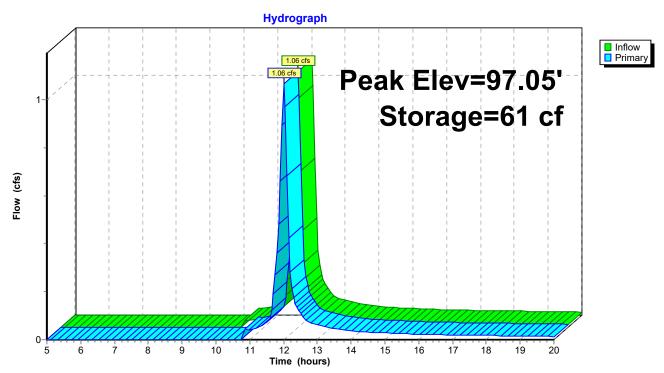
Genter-or-Mass det. time= 5.1 min (701.0 - 776.7)

Volume	Inv	<u>rert Avail</u>	.Storage	Storage	Description		
#1	96.	50'	209 cf	Custom	Stage Data (Prisr	natic)Listed below	(Recalc)
Elevation (fee		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)		
96.5	50	72		0	0		
97.0	00	147		55	55		
98.0	00	162		155	209		
Device	Routing	Inv	ert Outl	et Device	S		
#1	Primary	96.		.0 deg x 6 2.49 (C=	6.0' long x 1.00' ris 3.11)	e Sharp-Crested	Vee/Trap Weir

Primary OutFlow Max=1.05 cfs @ 12.01 hrs HW=97.04' (Free Discharge)
—1=Sharp-Crested Vee/Trap Weir (Weir Controls 1.05 cfs @ 1.18 fps)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

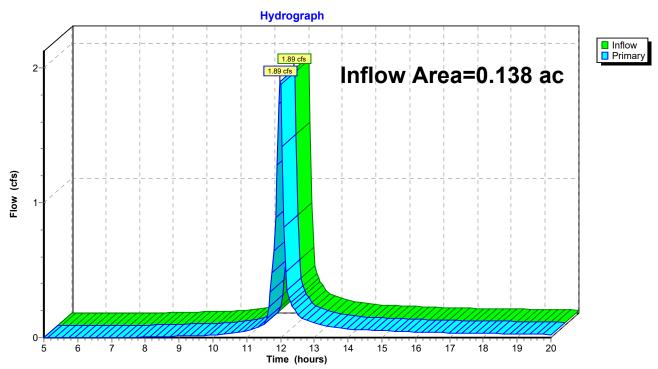
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 7.70" for 7 DAY-100YR event

Inflow = 1.89 cfs @ 11.99 hrs, Volume= 0.089 af

Primary = 1.89 cfs @ 11.99 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 9.71" for 7 DAY-100YR event

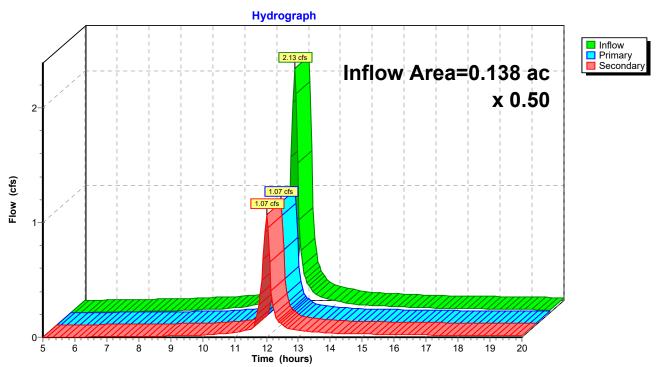
Inflow = 2.13 cfs @ 12.00 hrs, Volume= 0.112 af

Primary = 1.07 cfs @ 12.00 hrs, Volume= 0.056 af, Atten= 50%, Lag= 0.0 min

Secondary = 1.07 cfs @ 12.00 hrs, Volume= 0.056 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

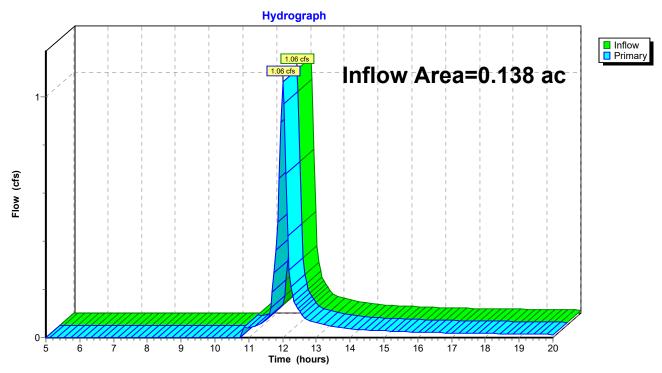
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 4.43" for 7 DAY-100YR event

Inflow = 1.06 cfs @ 12.01 hrs, Volume= 0.051 af

Primary = 1.06 cfs @ 12.01 hrs, Volume= 0.051 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 10 DAY-100YR Rainfall=16.10"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>9.46"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=2.30 cfs 0.109 af

Subcatchment3S: Post Developed Basin I Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>11.60"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=2.52 cfs 0.134 af

Pond 4P: Rock Void

Peak Elev=98.05' Storage=170 cf Inflow=1.26 cfs 0.067 af

Outflow=1.26 cfs 0.063 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.065 af Inflow=1.26 cfs 0.067 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=97.06' Storage=64 cf Inflow=1.26 cfs 0.063 af

Outflow=1.26 cfs 0.062 af

Link 2L: Outfall

Inflow=2.30 cfs 0.109 af Primary=2.30 cfs 0.109 af

Link 6L: Split

x 0.50 Inflow=2.52 cfs 0.134 af

Primary=1.26 cfs 0.067 af Secondary=1.26 cfs 0.067 af

Link 10L: Combined Outflow

Inflow=1.26 cfs 0.062 af Primary=1.26 cfs 0.062 af

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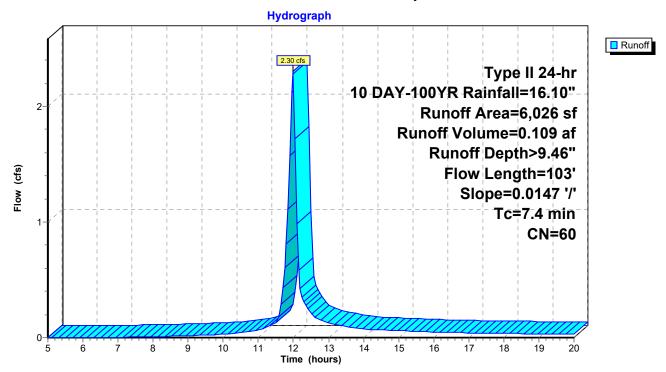
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 2.30 cfs @ 11.99 hrs, Volume= 0.109 af, Depth> 9.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10 DAY-100YR Rainfall=16.10"

	Α	rea (sf)	CN [Description						
*		6,026	60 V	Woods/grass comb., Poor, HSG B						
		6,026	1	00.00% Pe	ervious Are	a				
	Tc	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	7.4	103	0.0147	0.23		Lag/CN Method, Woods				

Subcatchment 1S: Pre-Developed Basin I



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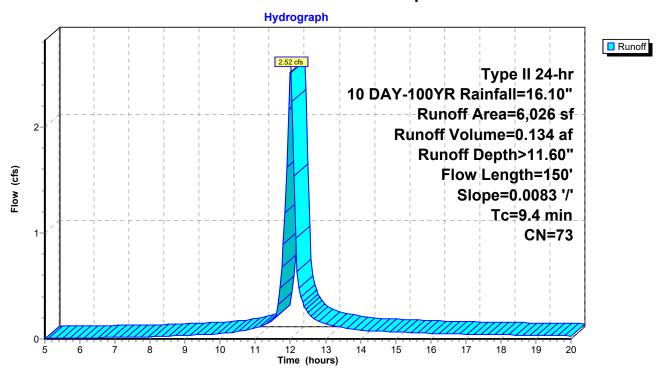
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 2.52 cfs @ 12.00 hrs, Volume= 0.134 af, Depth>11.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10 DAY-100YR Rainfall=16.10"

	Aı	rea (sf)	CN	Description					
		300	98	Roofs, HSG B					
		97	98	B Paved parking, HSG B					
*		973	65	Uncompacted Gravel 35% Void					
		1,283	85	Gravel roads, HSG B					
		3,373	67	Brush, Poor, HSG B					
		6,026	73	Weighted A	verage				
		5,629	!	93.41% Pei	rvious Area				
		397	(6.59% Impe	ervious Are	a			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	9.4	150	0.0083	0.27		Lag/CN Method,			

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 10 DAY-100YR Rainfall=16.10"

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Summary for Pond 4P: Rock Void

Inflow = 1.26 cfs @ 12.00 hrs, Volume= 0.067 af

Outflow = 1.26 cfs @ 12.00 hrs, Volume= 0.063 af, Atten= 0%, Lag= 0.0 min

Primary = 1.26 cfs @ 12.00 hrs, Volume= 0.063 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.05' @ 12.00 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 38.8 min calculated for 0.063 af (94% of inflow)

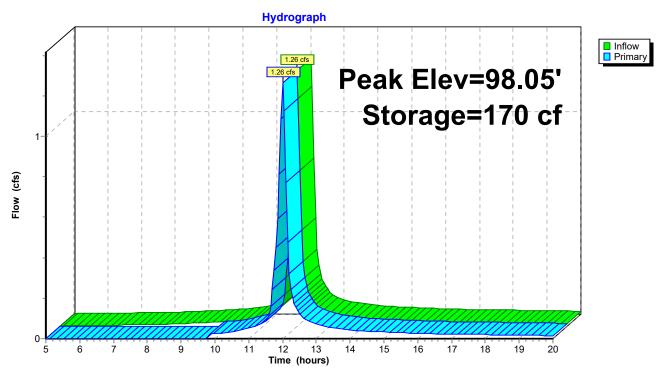
Center-of-Mass det. time= 16.5 min (773.8 - 757.4)

Volume	Inv	ert Avail.S	Storage	Storage D	escription	
#1	97.	50'	170 cf		Stage Data (Perall x 35.0%	rismatic)Listed below (Recalc) Voids
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	Inve	rt Outl	et Devices		
#1	Primary	98.0	Hea	d (feet) 0.2	0.40 0.60	road-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32

Primary OutFlow Max=1.25 cfs @ 12.00 hrs HW=98.05' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 1.25 cfs @ 0.60 fps)

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Pond 4P: Rock Void



Type II 24-hr 10 DAY-100YR Rainfall=16.10"

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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 5.80" for 10 DAY-100YR event

Inflow 1.26 cfs @ 12.00 hrs, Volume= 0.067 af

5.00 hrs, Volume= Outflow 0.000 af, Atten= 100%, Lag= 0.0 min 0.00 cfs @

5.00 hrs, Volume= Primary 0.00 cfs @ 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 20.00 hrs Surf.Area= 61.177 ac Storage= 0.065 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

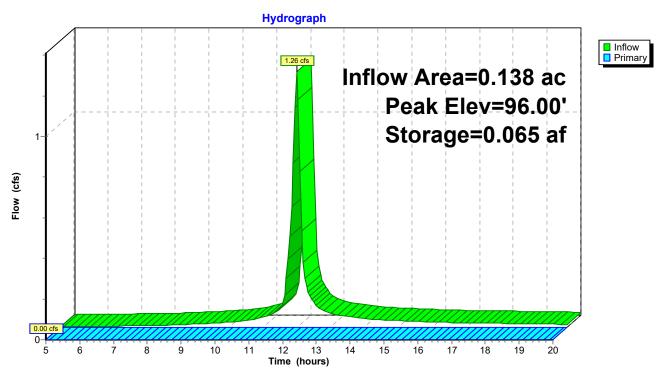
Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert A	Avail.Storage	Storage Description			
#1	96.00'	356.830 af	Custom Stage Data (Prismatic)Listed below (Recalc)			
Elevatio						
96.0	0 60.960	0	.000 0.000			
97.0	0 265.600	163	.280 163.280			
98.0	0 121.500	193	.550 356.830			
Device	Routing		utlet Devices			
#1	Primary		100.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir Cv= 2.49 (C= 3.11)			

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 10 DAY-100YR Rainfall=16.10"

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Summary for Pond 9P: North Pond

Inflow = 1.26 cfs @ 12.00 hrs, Volume= 0.063 af

Outflow = 1.26 cfs @ 12.01 hrs, Volume= 0.062 af, Atten= 0%, Lag= 0.2 min

Primary = 1.26 cfs @ 12.01 hrs, Volume= 0.062 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.06' @ 12.01 hrs Surf.Area= 148 sf Storage= 64 cf

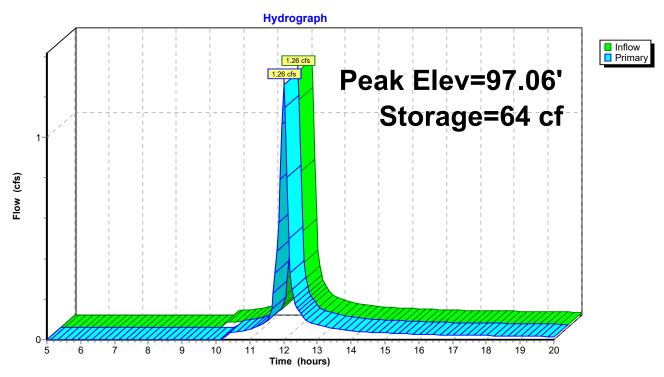
Plug-Flow detention time= 9.1 min calculated for 0.062 af (98% of inflow) Center-of-Mass det. time= 3.0 min (776.8 - 773.8)

Volume	Inv	ert Avail.	Storage	Storage D	escription	
#1	96.	50'	209 cf	Custom S	tage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
96.5	50	72		0	0	
97.0	0	147		55	55	
98.0	0	162		155	209	
Device	Routing	Inve		et Devices		
#1	Primary	96.9		0 deg x 6.0 2.49 (C= 3.		' rise Sharp-Crested Vee/Trap Weir

Primary OutFlow Max=1.24 cfs @ 12.01 hrs HW=97.06' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Weir Controls 1.24 cfs @ 1.24 fps)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

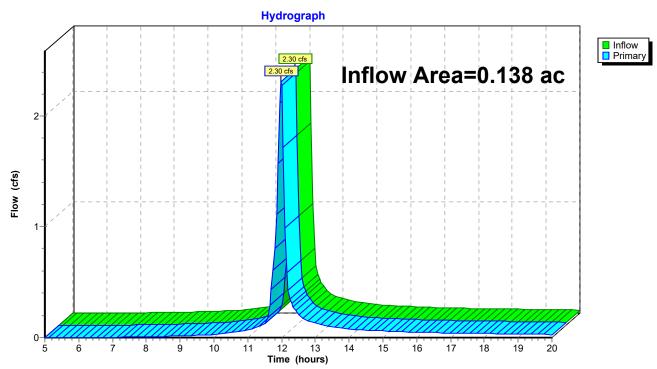
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 9.46" for 10 DAY-100YR event

Inflow = 2.30 cfs @ 11.99 hrs, Volume= 0.109 af

Primary = 2.30 cfs @ 11.99 hrs, Volume= 0.109 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 11.60" for 10 DAY-100YR event

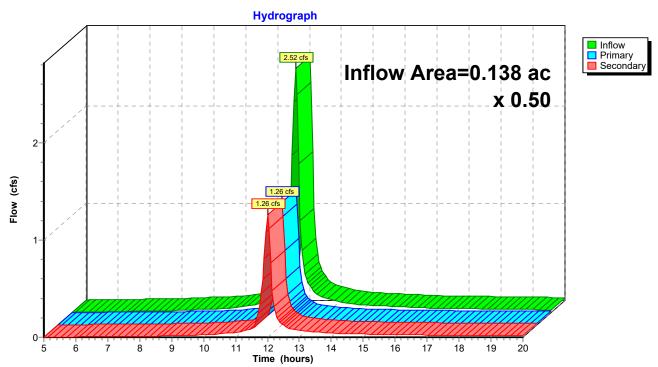
Inflow = 2.52 cfs @ 12.00 hrs, Volume= 0.134 af

Primary = 1.26 cfs @ 12.00 hrs, Volume= 0.067 af, Atten= 50%, Lag= 0.0 min

Secondary = 1.26 cfs @ 12.00 hrs, Volume= 0.067 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

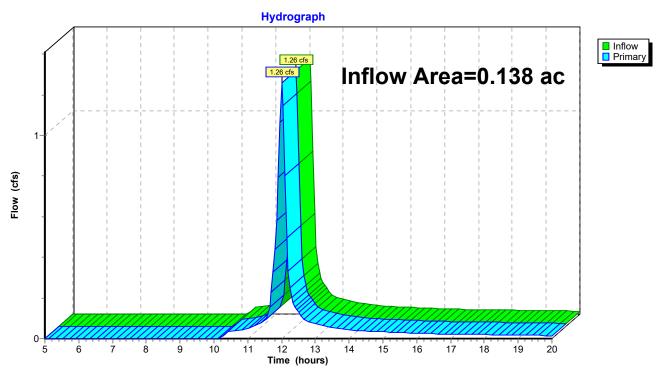
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 5.38" for 10 DAY-100YR event

Inflow = 1.26 cfs @ 12.01 hrs, Volume= 0.062 af

Primary = 1.26 cfs @ 12.01 hrs, Volume= 0.062 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>2.18"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=0.55 cfs 0.025 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>3.41"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=0.79 cfs 0.039 af

Peak Elev=98.03' Storage=170 cf Inflow=0.40 cfs 0.020 af Outflow=0.57 cfs 0.016 af

Pond 5P: South Pond

Pond 4P: Rock Void

Peak Elev=96.00' Storage=0.019 af Inflow=0.40 cfs 0.020 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=96.99' Storage=54 cf Inflow=0.57 cfs 0.016 af

Outflow=0.53 cfs 0.015 af

Link 2L: Outfall

Inflow=0.55 cfs 0.025 af Primary=0.55 cfs 0.025 af

Link 6L: Split

x 0.50 Inflow=0.79 cfs 0.039 af

Primary=0.40 cfs 0.020 af Secondary=0.40 cfs 0.020 af

Link 10L: Combined Outflow

Inflow=0.53 cfs 0.015 af

Primary=0.53 cfs 0.015 af

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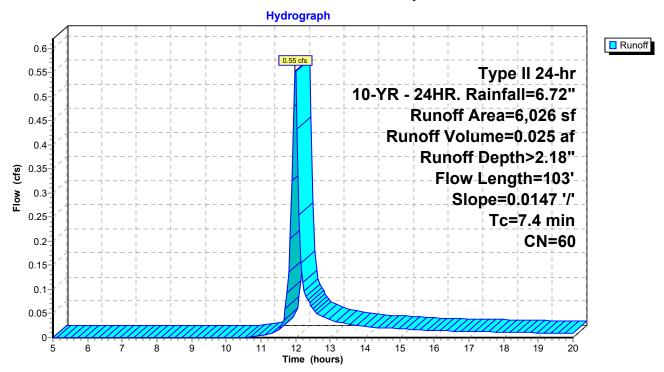
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 0.55 cfs @ 11.99 hrs, Volume= 0.025 af, Depth> 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

_	Α	rea (sf)	CN [Description							
,	•	6,026	60 \	Noods/grass comb., Poor, HSG B							
-		6,026	,	100.00% Pervious Area							
	Тс	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	ft) (ft/sec) (cfs)							
	7.4	103	0.0147	0.23		Lag/CN Method, Woods					

Subcatchment 1S: Pre-Developed Basin I



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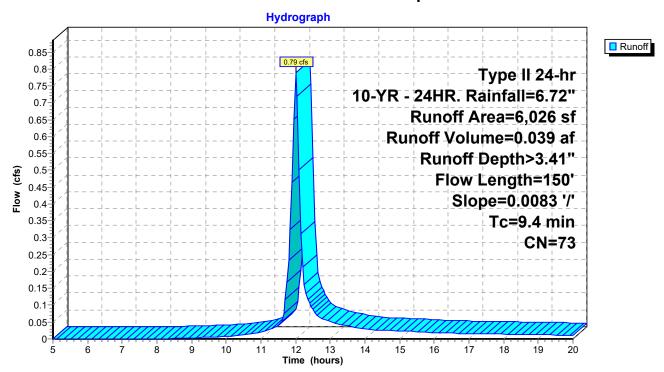
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 0.79 cfs @ 12.01 hrs, Volume= 0.039 af, Depth> 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

	Α	rea (sf)	CN	Description					
300 98 Roofs, HSG B									
	97 98 Paved parking, HSG B								
*		973	65	Uncompacted Gravel 35% Void					
		1,283	85	Gravel roads, HSG B					
		3,373	67	Brush, Poo	r, HSG B				
		6,026	73	Weighted A	verage				
		5,629		93.41% Pervious Area					
		397		6.59% Impe	ervious Are	a			
		Length	Slope	,	Capacity	Description			
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	9.4	150	0.0083	0.27		Lag/CN Method,			

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

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Summary for Pond 4P: Rock Void

Inflow = 0.40 cfs @ 12.01 hrs, Volume= 0.020 af

Outflow = 0.57 cfs @ 12.05 hrs, Volume= 0.016 af, Atten= 0%, Lag= 2.3 min

Primary = 0.57 cfs @ 12.05 hrs, Volume= 0.016 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.03' @ 12.04 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 74.8 min calculated for 0.016 af (82% of inflow)

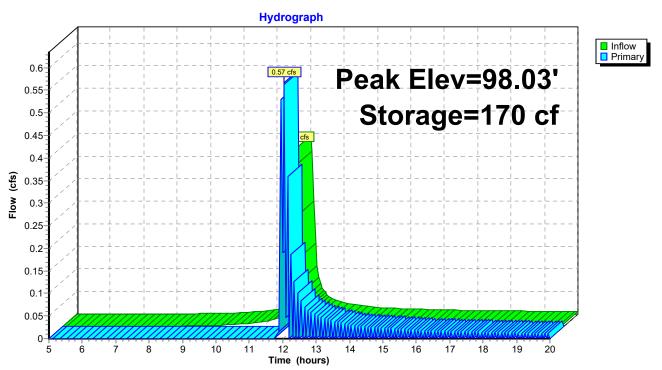
Center-of-Mass det. time= 23.6 min (808.5 - 784.9)

Volume	Inv	ert Avail.S	Storage	Storage D	escription	
#1	97.	50'	170 cf		Stage Data (Perall x 35.0%	rismatic)Listed below (Recalc) Voids
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	Inve	rt Outl	et Devices		
#1	Primary	98.0	Hea	d (feet) 0.2	0.40 0.60	road-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32

Primary OutFlow Max=0.53 cfs @ 12.05 hrs HW=98.03' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.53 cfs @ 0.45 fps)

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Pond 4P: Rock Void



Repeater Station Basin I Prepared by HP Inc.

Type II 24-hr 10-YR - 24HR. Rainfall=6.72" Printed 3/16/2020

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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 1.71" for 10-YR - 24HR. event

Inflow = 0.40 cfs @ 12.01 hrs, Volume= 0.020 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 20.00 hrs Surf.Area= 61.024 ac Storage= 0.019 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

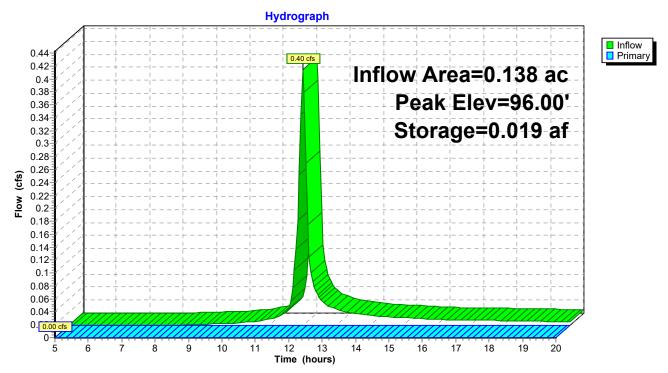
Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert A	vail.Storage	Storage Description
#1	96.00'	356.830 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee		Inc.S (acre-f	
96.0	0 60.960	0	0.000 0.000
97.0	0 265.600	163	.280 163.280
98.0	0 121.500	193	.550 356.830
Device	Routing	Invert O	utlet Devices
#1	Primary		00.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir v= 2.49 (C= 3.11)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

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Summary for Pond 9P: North Pond

Inflow = 0.57 cfs @ 12.05 hrs, Volume= 0.016 af

Outflow = 0.53 cfs @ 12.01 hrs, Volume= 0.015 af, Atten= 6%, Lag= 0.0 min

Primary = 0.53 cfs @ 12.01 hrs, Volume= 0.015 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.99' @ 12.01 hrs Surf.Area= 146 sf Storage= 54 cf

Plug-Flow detention time= 27.1 min calculated for 0.015 af (94% of inflow)

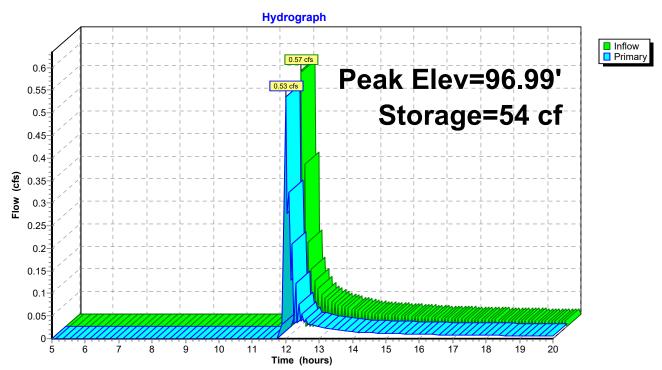
Center-of-Mass det. time= 6.6 min (815.1 - 808.5)

Volume	Inv	ert Avail	.Storage	Storage	Description	
#1	96.	50'	209 cf	Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
96.5	0	72		0	0	
97.0	0	147		55	55	
98.0	0	162		155	209	
Device	Routing	Inv	ert Outl	let Device	s	
#1	Primary	96.		.0 deg x 6 2.49 (C=		rise Sharp-Crested Vee/Trap Weir

Primary OutFlow Max=0.49 cfs @ 12.01 hrs HW=96.99' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Weir Controls 0.49 cfs @ 0.92 fps)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

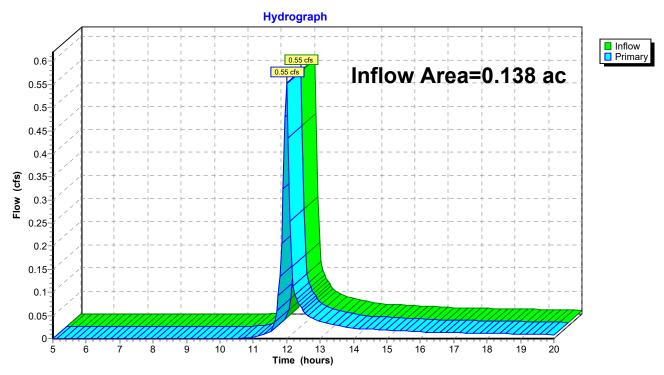
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 2.18" for 10-YR - 24HR. event

Inflow = 0.55 cfs @ 11.99 hrs, Volume= 0.025 af

Primary = 0.55 cfs @ 11.99 hrs, Volume= 0.025 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 3.41" for 10-YR - 24HR. event

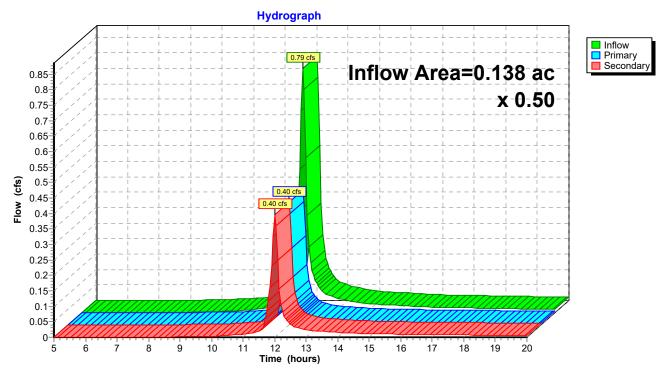
Inflow = 0.79 cfs @ 12.01 hrs, Volume= 0.039 af

Primary = 0.40 cfs @ 12.01 hrs, Volume= 0.020 af, Atten= 50%, Lag= 0.0 min

Secondary = 0.40 cfs @ 12.01 hrs, Volume= 0.020 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

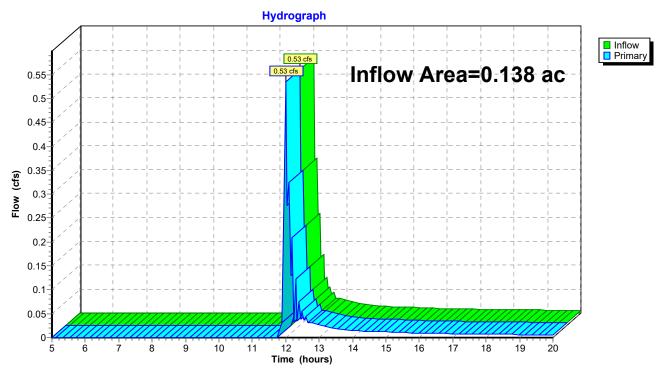
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 1.32" for 10-YR - 24HR. event

Inflow = 0.53 cfs @ 12.01 hrs, Volume= 0.015 af

Primary = 0.53 cfs @ 12.01 hrs, Volume= 0.015 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>2.99"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=0.76 cfs 0.034 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>4.39"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=1.01 cfs 0.051 af

Pond 4P: Rock Void

Peak Elev=98.03' Storage=170 cf Inflow=0.50 cfs 0.025 af

Outflow=0.58 cfs 0.022 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.025 af Inflow=0.50 cfs 0.025 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=96.99' Storage=53 cf Inflow=0.58 cfs 0.022 af

Outflow=0.50 cfs 0.021 af

Link 2L: Outfall

Inflow=0.76 cfs 0.034 af Primary=0.76 cfs 0.034 af

Link 6L: Split

x 0.50 Inflow=1.01 cfs 0.051 af

Primary=0.50 cfs 0.025 af Secondary=0.50 cfs 0.025 af

Link 10L: Combined Outflow

Inflow=0.50 cfs 0.021 af Primary=0.50 cfs 0.021 af

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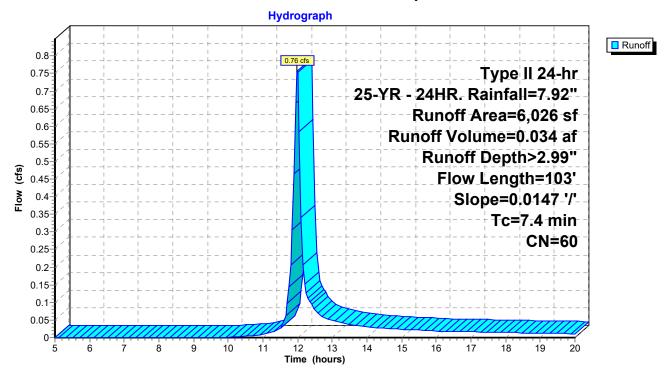
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 0.76 cfs @ 11.99 hrs, Volume= 0.034 af, Depth> 2.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

_	Α	rea (sf)	CN [Description						
4		6,026	60 V	Noods/grass comb., Poor, HSG B						
_		6,026	1	100.00% Pervious Area						
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	t/ft) (ft/sec) (cfs)						
	7.4	103	0.0147	0.23		Lag/CN Method, Woods				

Subcatchment 1S: Pre-Developed Basin I



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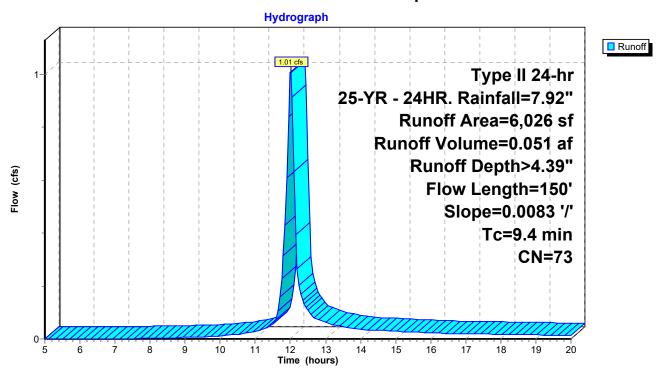
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 1.01 cfs @ 12.01 hrs, Volume= 0.051 af, Depth> 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

	Α	rea (sf)	CN I	Description					
		300	98 I						
		97	98 I						
*		973	65 l	Uncompacted Gravel 35% Void					
		1,283	85 (Gravel roads, HSG B					
		3,373	67 I	Brush, Poo	r, HSG B				
		6,026	73 \	Neighted A	verage				
		5,629	(93.41% Pei	rvious Area				
		397	(6.59% Impe	ervious Area	a			
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	9.4	150	0.0083	0.27		Lag/CN Method,			

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

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Summary for Pond 4P: Rock Void

Inflow 0.50 cfs @ 12.01 hrs, Volume= 0.025 af

Outflow 0.58 cfs @ 12.04 hrs, Volume= 0.022 af, Atten= 0%, Lag= 2.1 min

0.58 cfs @ 12.04 hrs, Volume= Primary 0.022 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.03' @ 12.04 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 64.9 min calculated for 0.022 af (85% of inflow)

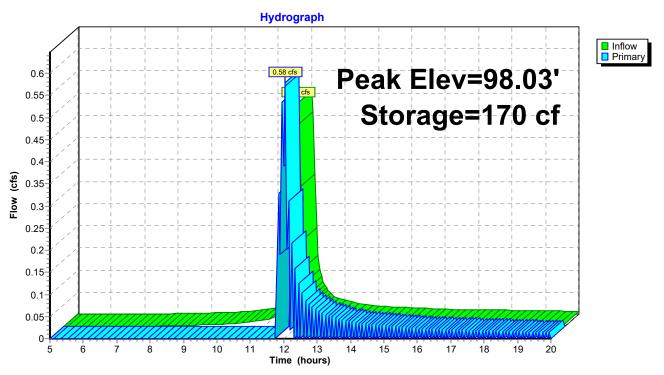
Center-of-Mass det. time= 21.1 min (800.5 - 779.4)

Volume	Inv	ert Avail.S	orage	Storage D	escription			
#1	97.	50'	170 cf		Stage Data (Preerall x 35.0%	rismatic)Listed below (Recalc) Voids		
Elevatio (fee		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)			
97.5	0	973		0	0			
98.0	0	973		487	487			
Device	Routing	Inver	t Outl	et Devices				
#1	Primary	98.00	Hea	45.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32				

Primary OutFlow Max=0.54 cfs @ 12.04 hrs HW=98.03' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.54 cfs @ 0.45 fps)

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Pond 4P: Rock Void



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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 2.20" for 25-YR - 24HR. event

Inflow = 0.50 cfs @ 12.01 hrs, Volume= 0.025 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 20.00 hrs Surf.Area= 61.042 ac Storage= 0.025 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

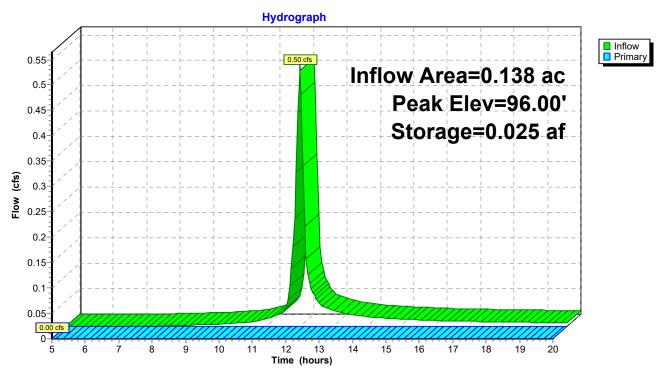
Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storaç	je Stor	age Description		
#1	96.00'	356.830	af Cus	tom Stage Data (Prisma	tic)Listed below (Recalc)	
Elevatio (fee			Store e-feet)	Cum.Store (acre-feet)		
96.0	0 60.96	0	0.000	0.000		
97.0	0 265.60	0 16	3.280	163.280		
98.0	0 121.50	0 19	93.550	356.830		
Device Routing			Outlet D			
#1	#1 Primary		100.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir Cv= 2.49 (C= 3.11)			

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

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Summary for Pond 9P: North Pond

Inflow = 0.58 cfs @ 12.04 hrs, Volume= 0.022 af

Outflow = 0.50 cfs @ 12.01 hrs, Volume= 0.021 af, Atten= 13%, Lag= 0.0 min

Primary = 0.50 cfs @ 12.01 hrs, Volume= 0.021 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.99' @ 12.01 hrs Surf.Area= 145 sf Storage= 53 cf

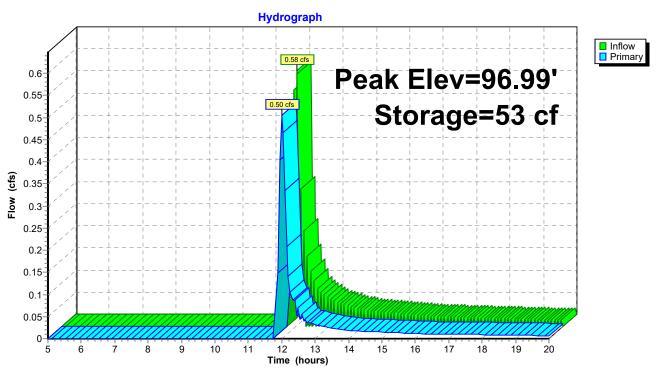
Plug-Flow detention time= 20.6 min calculated for 0.021 af (95% of inflow) Center-of-Mass det. time= 4.8 min (805.3 - 800.5)

Volume	Inv	ert Avail.	Storage	Storage D	escription	
#1	96.	50'	209 cf	Custom S	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
96.5	50	72		0	0	
97.0	00	147		55	55	
98.0	0	162		155	209	
Device	Routing	Inv		et Devices		
#1	Primary	96.9		.0 deg x 6.0 2.49 (C= 3		' rise Sharp-Crested Vee/Trap Weir

Primary OutFlow Max=0.49 cfs @ 12.01 hrs HW=96.99' (Free Discharge)
—1=Sharp-Crested Vee/Trap Weir (Weir Controls 0.49 cfs @ 0.92 fps)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

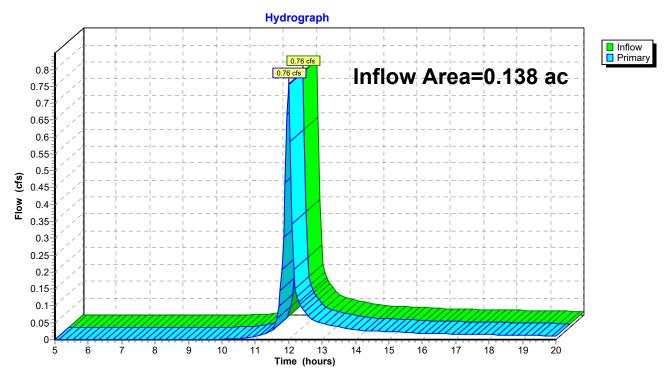
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 2.99" for 25-YR - 24HR. event

Inflow = 0.76 cfs @ 11.99 hrs, Volume= 0.034 af

Primary = 0.76 cfs @ 11.99 hrs, Volume= 0.034 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 4.39" for 25-YR - 24HR. event

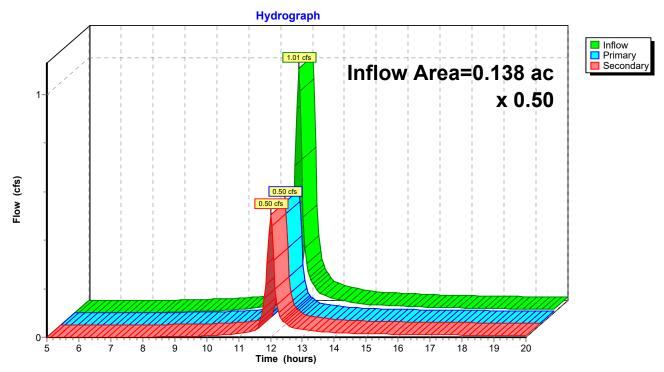
Inflow = 1.01 cfs @ 12.01 hrs, Volume= 0.051 af

Primary = 0.50 cfs @ 12.01 hrs, Volume= 0.025 af, Atten= 50%, Lag= 0.0 min

Secondary = 0.50 cfs @ 12.01 hrs, Volume= 0.025 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

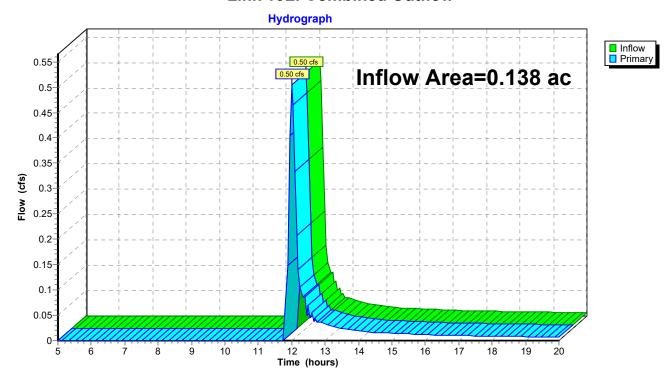
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 1.79" for 25-YR - 24HR. event

Inflow = 0.50 cfs @ 12.01 hrs, Volume= 0.021 af

Primary = 0.50 cfs @ 12.01 hrs, Volume= 0.021 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth=0.00"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=0.00 cfs 0.000 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth=0.00"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=0.00 cfs 0.000 af

Pond 4P: Rock Void

Peak Elev=97.50' Storage=0 cf Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.000 af Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=96.50' Storage=0 cf Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Link 2L: Outfall

Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af

Link 6L: Split

x 0.50 Inflow=0.00 cfs 0.000 af

Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af

Link 10L: Combined Outflow

Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af

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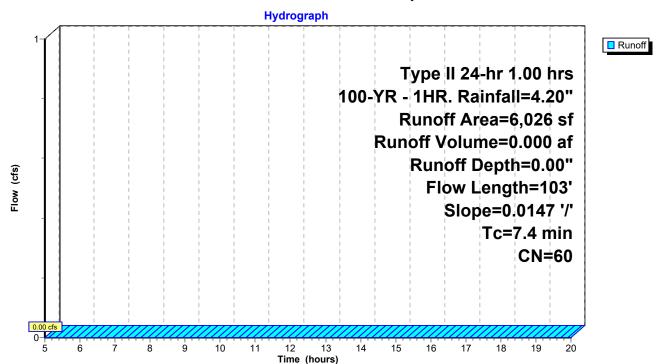
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

	Α	rea (sf)	CN E	CN Description							
*		6,026	60 V	60 Woods/grass comb., Poor, HSG B							
		6,026	1	100.00% Pervious Area							
	Tc Length Slope Velocity Capacity D (min) (feet) (ft/ft) (ft/sec) (cfs)				. ,	Description					
	7.4	103	0.0147	0.23		Lag/CN Method, Woods					

Subcatchment 1S: Pre-Developed Basin I



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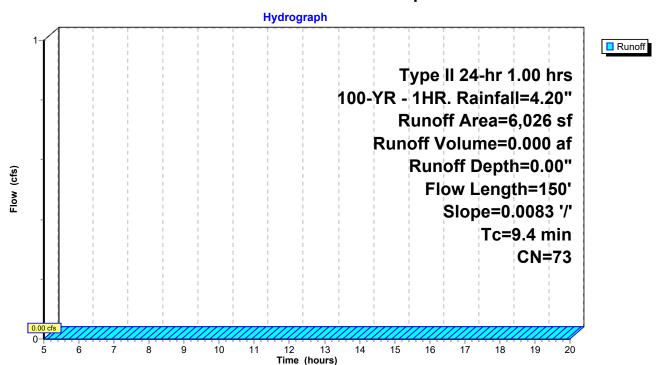
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

	Aı	rea (sf)	CN	Description							
		300	98	Roofs, HSC	Roofs, HSG B						
		97	98	Paved parking, HSG B							
*		973	65	Uncompacted Gravel 35% Void							
		1,283	85	Gravel roads, HSG B							
		3,373	67	Brush, Poor, HSG B							
		6,026	73	Weighted A	verage						
		5,629		93.41% Pe	rvious Area						
		397		6.59% Impe	ervious Are	a					
	Тс	Length	Slope	Velocity	Capacity	Description					
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	9.4	150	0.0083	0.27		Lag/CN Method,					

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

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Summary for Pond 4P: Rock Void

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = $0.00 \text{ cfs } \bar{\text{@}}$ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.50' @ 5.00 hrs Surf.Area= 973 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

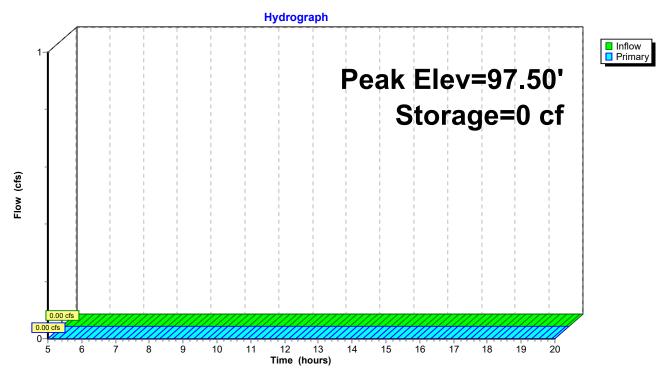
Center-of-Mass det. time= (not calculated: no inflow)

Volume	Inv	ert Avail.St	orage	Storage D	escription			
#1	97.	50'	170 cf		stage Data (Perall x 35.0%	Prismatic)Listed below (Recalc) Voids		
Elevation (fee		Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)			
97.5	50	973		0	0			
98.0	00	973		487	487			
Device	Routing	Inver	Outle	et Devices				
#1 Prima		98.00' 4 { H		5.0' long x 0.5' breadth Broad-Crested Rectangular Weir ead (feet) 0.20 0.40 0.60 0.80 1.00 oef. (English) 2.80 2.92 3.08 3.30 3.32				

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=97.50' (Free Discharge)
—1=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

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Pond 4P: Rock Void



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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 1HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 5.00 hrs Surf.Area= 60.960 ac Storage= 0.000 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

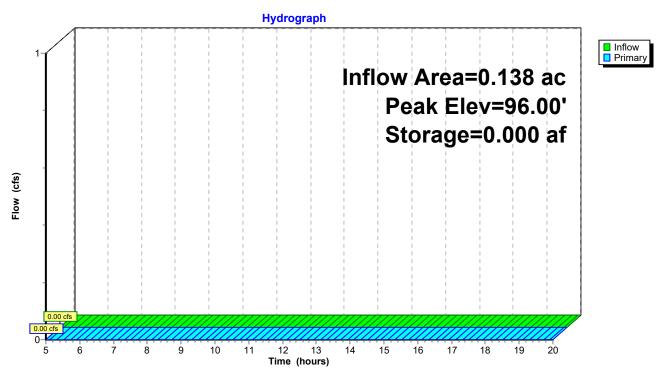
Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert A	vail.Storage	Storage Description
#1	96.00'	356.830 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio		Inc.S (acre-f	
96.0	0 60.960	0.	000 0.000
97.0	0 265.600	163.	280 163.280
98.0	0 121.500	193.	550 356.830
Device	Routing	Invert O	utlet Devices
#1	Primary		0.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir y= 2.49 (C= 3.11)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

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Summary for Pond 9P: North Pond

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.50' @ 5.00 hrs Surf.Area= 72 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

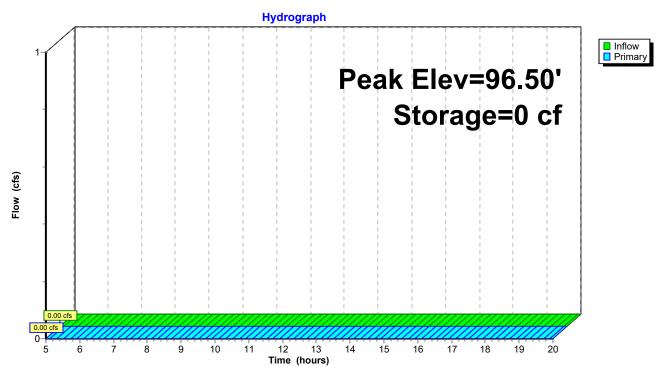
Volume	Invert	Avail.Sto	rage :	Storage D	escription	
#1	96.50'	20)9 cf (Custom S	tage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)		.Area sq-ft)	Inc.S (cubic-	Store feet)	Cum.Store (cubic-feet)	
96.50		72		0	0	
97.00		147	55		55	
98.00		162		155	209	
	uting mary	Invert 96.90'	100.0	t <u>Devices</u> deg x 6.0		' rise Sharp-Crested Vee/Trap Weir

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.50' (Free Discharge)

1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

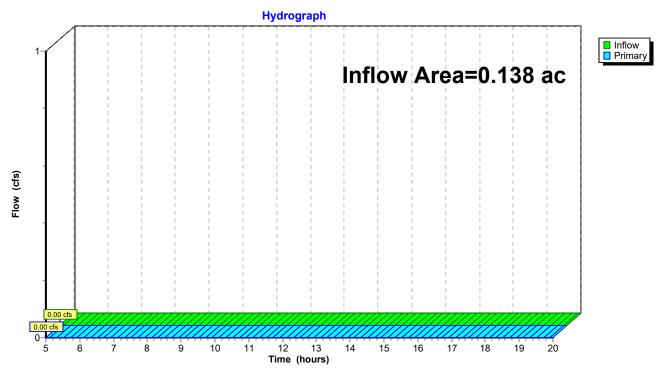
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth = 0.00" for 100-YR - 1HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 1HR. event

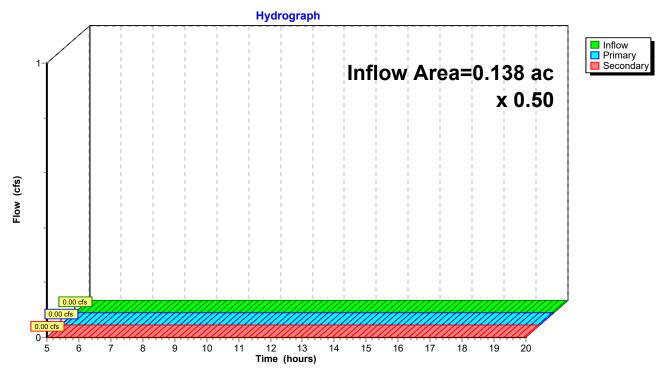
Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

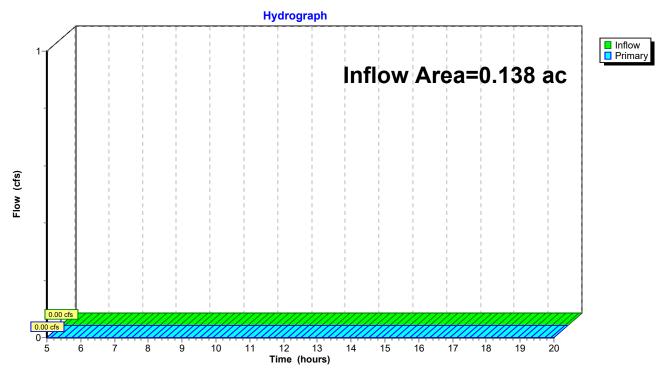
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 1HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>4.38"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=1.10 cfs 0.051 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>6.02"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=1.36 cfs 0.069 af

Pond 4P: Rock Void

Peak Elev=98.03' Storage=170 cf Inflow=0.68 cfs 0.035 af

Outflow=0.70 cfs 0.031 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.034 af Inflow=0.68 cfs 0.035 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=97.01' Storage=56 cf Inflow=0.70 cfs 0.031 af

Outflow=0.68 cfs 0.030 af

Link 2L: Outfall

Inflow=1.10 cfs 0.051 af Primary=1.10 cfs 0.051 af

Link 6L: Split

x 0.50 Inflow=1.36 cfs 0.069 af

Primary=0.68 cfs 0.035 af Secondary=0.68 cfs 0.035 af

Link 10L: Combined Outflow

Inflow=0.68 cfs 0.030 af Primary=0.68 cfs 0.030 af

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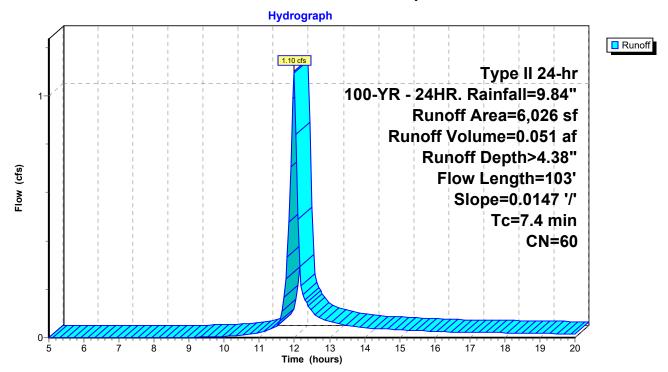
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 1.10 cfs @ 11.99 hrs, Volume= 0.051 af, Depth> 4.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

	Α	rea (sf)	CN [Description						
*		6,026	60 V	Woods/grass comb., Poor, HSG B						
_		6,026	1	100.00% Pervious Area						
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	7.4	103	0.0147	0.23		Lag/CN Method, Woods				

Subcatchment 1S: Pre-Developed Basin I



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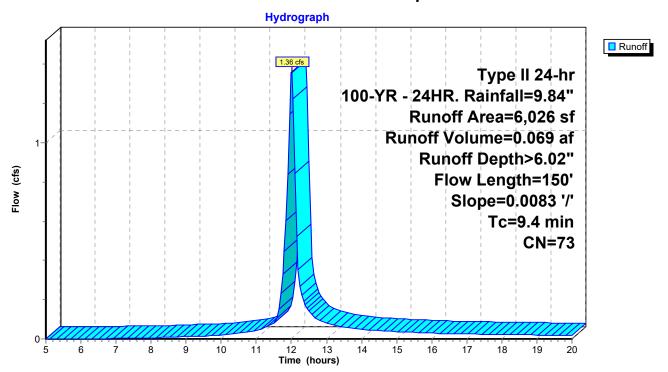
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 1.36 cfs @ 12.01 hrs, Volume= 0.069 af, Depth> 6.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

	Α	rea (sf)	CN I	Description						
		300	98 I	Roofs, HSG B						
		97	98 I	Paved parking, HSG B						
*		973	65 l	Uncompacted Gravel 35% Void						
		1,283	85 (Gravel roads, HSG B						
		3,373	67 I	Brush, Poo	r, HSG B					
		6,026	73 \	Neighted A	verage					
		5,629	(93.41% Pei	rvious Area					
		397	(6.59% Impe	ervious Area	a				
	Tc	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	9.4	150	0.0083	0.27		Lag/CN Method,				

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

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Summary for Pond 4P: Rock Void

Inflow = 0.68 cfs @ 12.01 hrs, Volume= 0.035 af

Outflow = 0.70 cfs @ 12.00 hrs, Volume= 0.031 af, Atten= 0%, Lag= 0.0 min

Primary = 0.70 cfs @ 12.00 hrs, Volume= 0.031 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.03' @ 12.00 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 55.7 min calculated for 0.031 af (89% of inflow)

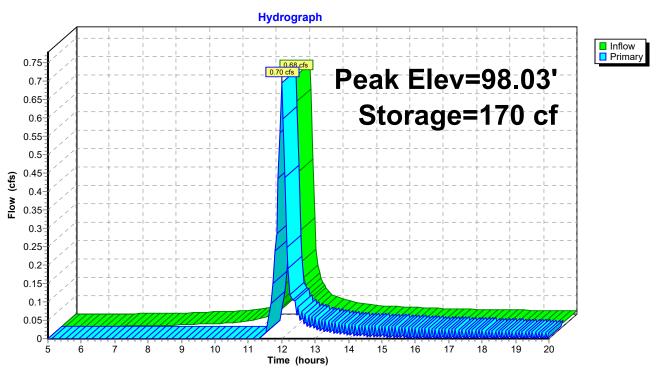
Center-of-Mass det. time= 19.8 min (792.0 - 772.2)

Volume	Inv	ert Avail.	Storage	Storage D	escription			
#1	97.	50'	170 cf	Custom Stage Data (Prismatic)Listed below (Recalc) 487 cf Overall x 35.0% Voids				
Elevatio		Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)			
97.5	50	973		0	0			
98.0	00	973		487	487			
Device	Routing	Inve	ert Outl	et Devices				
#1	Primary	<u> </u>		45.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32				

Primary OutFlow Max=0.69 cfs @ 12.00 hrs HW=98.03' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.69 cfs @ 0.49 fps)

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Pond 4P: Rock Void



Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 3.01" for 100-YR - 24HR. event

Inflow = 0.68 cfs @ 12.01 hrs, Volume= 0.035 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 20.00 hrs Surf.Area= 61.073 ac Storage= 0.034 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

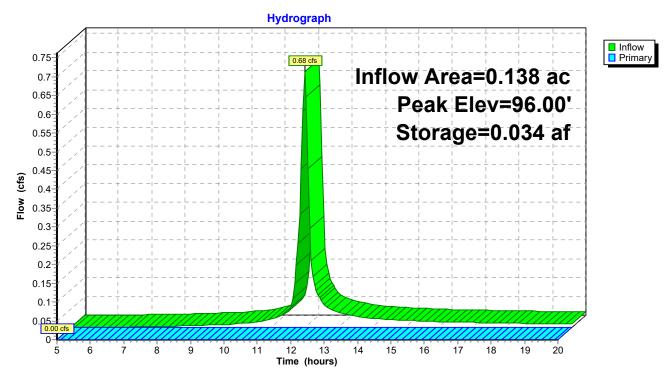
Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert A	Avail.Storage	Storage Description
#1	96.00'	356.830 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio			
96.0	0 60.960	0	.000 0.000
97.0	0 265.600	163	.280 163.280
98.0	0 121.500	193	.550 356.830
Device	Routing		utlet Devices
#1	Primary		00.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir v= 2.49 (C= 3.11)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

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Summary for Pond 9P: North Pond

Inflow = 0.70 cfs @ 12.00 hrs, Volume= 0.031 af

Outflow = 0.68 cfs @ 12.01 hrs, Volume= 0.030 af, Atten= 2%, Lag= 0.4 min

Primary = 0.68 cfs @ 12.01 hrs, Volume= 0.030 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.01' @ 12.01 hrs Surf.Area= 147 sf Storage= 56 cf

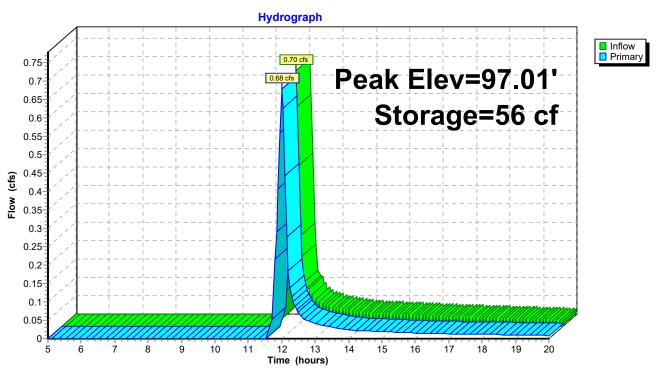
Plug-Flow detention time= 15.2 min calculated for 0.030 af (97% of inflow) Center-of-Mass det. time= 3.1 min (795.2 - 792.0)

Volume	Inv	ert Avail.	Storage	Storage D	escription	
#1	96.	50'	209 cf	Custom S	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
96.5	50	72		0	0	
97.0	00	147		55	55	
98.0	0	162		155	209	
Device	Routing	Inv		et Devices		
#1	Primary	96.9		.0 deg x 6.0 2.49 (C= 3		' rise Sharp-Crested Vee/Trap Weir

Primary OutFlow Max=0.66 cfs @ 12.01 hrs HW=97.01' (Free Discharge)
—1=Sharp-Crested Vee/Trap Weir (Weir Controls 0.66 cfs @ 1.01 fps)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

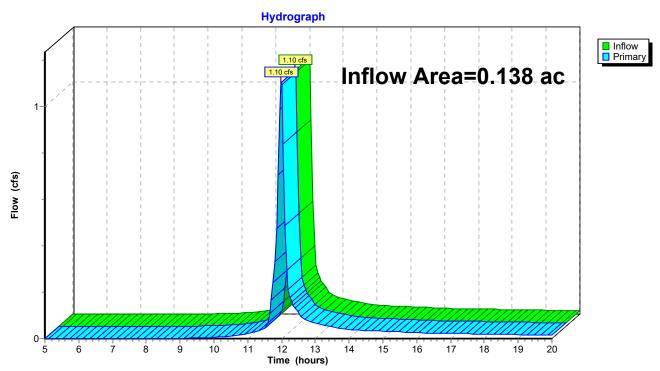
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 4.38" for 100-YR - 24HR. event

Inflow = 1.10 cfs @ 11.99 hrs, Volume= 0.051 af

Primary = 1.10 cfs @ 11.99 hrs, Volume= 0.051 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 6.02" for 100-YR - 24HR. event

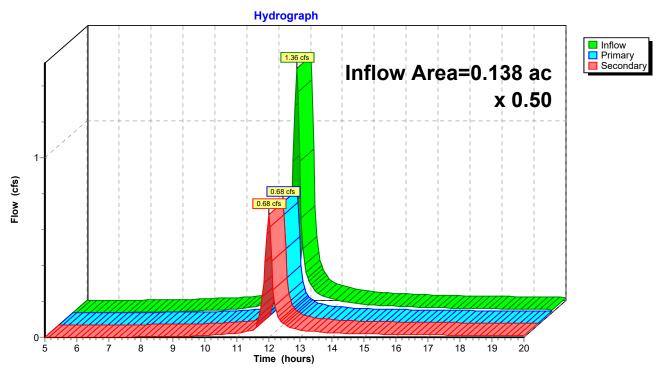
Inflow = 1.36 cfs @ 12.01 hrs, Volume= 0.069 af

Primary = 0.68 cfs @ 12.01 hrs, Volume= 0.035 af, Atten= 50%, Lag= 0.0 min

Secondary = 0.68 cfs @ 12.01 hrs, Volume= 0.035 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

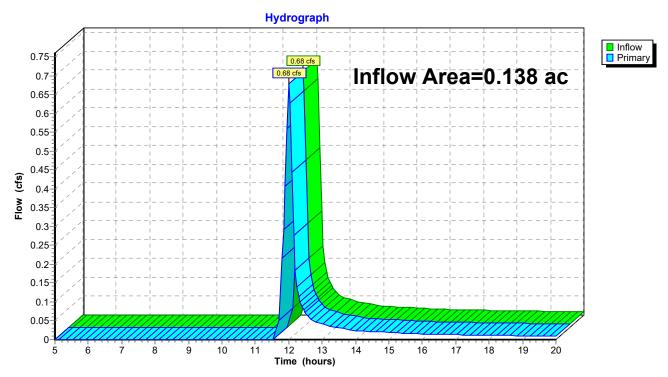
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 2.59" for 100-YR - 24HR. event

Inflow = 0.68 cfs @ 12.01 hrs, Volume= 0.030 af

Primary = 0.68 cfs @ 12.01 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth=0.00"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=0.00 cfs 0.000 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth=0.00"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=0.00 cfs 0.000 af

Pond 4P: Rock Void

Peak Elev=97.50' Storage=0 cf Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.000 af Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=96.50' Storage=0 cf Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Link 2L: Outfall

Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af

Link 6L: Split

x 0.50 Inflow=0.00 cfs 0.000 af

Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af

Link 10L: Combined Outflow

Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af

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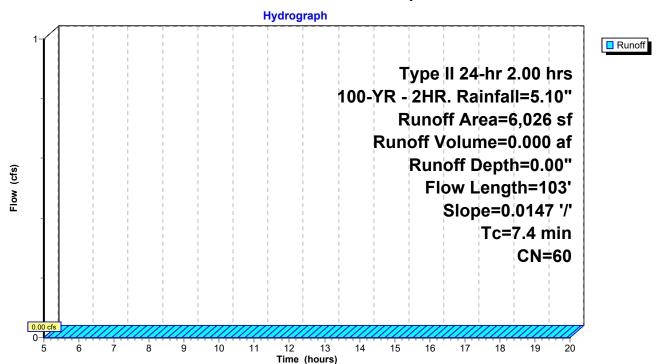
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

	Α	rea (sf)	CN [Description						
*		6,026	60 V	Woods/grass comb., Poor, HSG B						
_		6,026	1	100.00% Pervious Area						
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	7.4	103	0.0147	0.23		Lag/CN Method, Woods				

Subcatchment 1S: Pre-Developed Basin I



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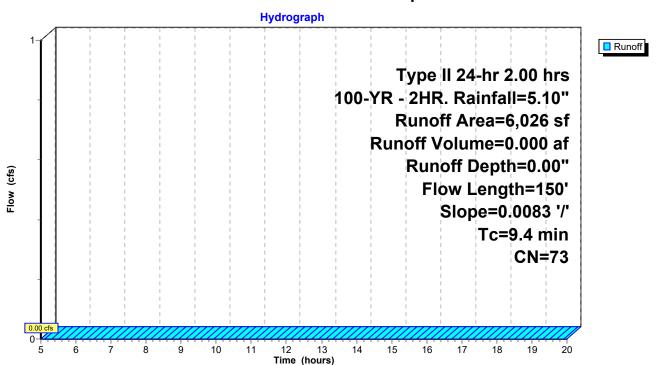
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

	Aı	rea (sf)	CN	Description						
		300	98	Roofs, HSG B						
		97	98	Paved parking, HSG B						
*		973	65	Uncompacted Gravel 35% Void						
		1,283	85	Gravel roads, HSG B						
		3,373	67	Brush, Poor, HSG B						
		6,026	73	Weighted A	verage					
		5,629	!	93.41% Pei	rvious Area					
		397	(6.59% Impe	ervious Are	a				
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	9.4	150	0.0083	0.27		Lag/CN Method,				

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

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Summary for Pond 4P: Rock Void

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = $0.00 \text{ cfs } \bar{\text{@}}$ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.50' @ 5.00 hrs Surf.Area= 973 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

Volume	Inv	ert Avail.St	orage	Storage D	escription	
#1	97.	50'	170 cf		tage Data (Perall x 35.0%	Prismatic) Listed below (Recalc) Voids
Elevatio	•••	Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	ng Invert Outle		et Devices		
#1	Primary 98.00' 45.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32					0.80 1.00

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=97.50' (Free Discharge) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

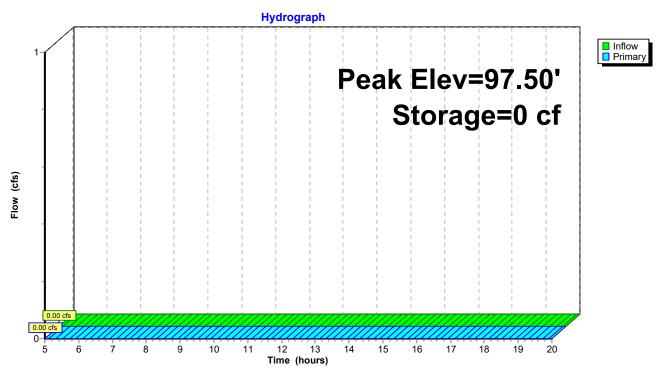
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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 2HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 5.00 hrs Surf.Area= 60.960 ac Storage= 0.000 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

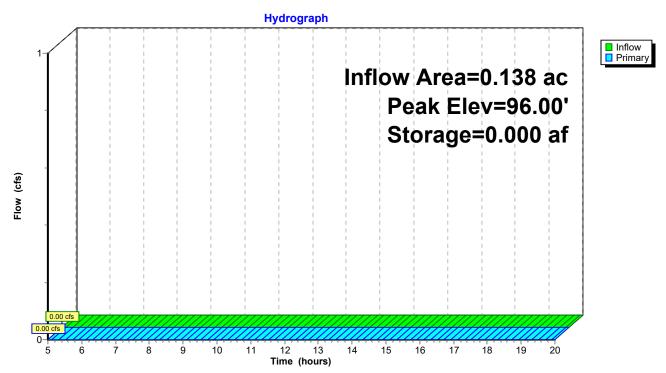
Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert	Avail.Storaç	je Stor	age Description		
#1	96.00'	356.830	af Cus	tom Stage Data (Prisma	tic)Listed below (Recalc)	
Elevatio (fee			Store e-feet)	Cum.Store (acre-feet)		
96.0	0 60.96	0	0.000	0.000		
97.0	0 265.60	0 16	3.280	163.280		
98.0	0 121.50	0 19	93.550	356.830		
Device Routing			Outlet D			
#1	#1 Primary		100.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir Cv= 2.49 (C= 3.11)			

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

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Summary for Pond 9P: North Pond

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 96.50' @ 5.00 hrs Surf.Area= 72 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

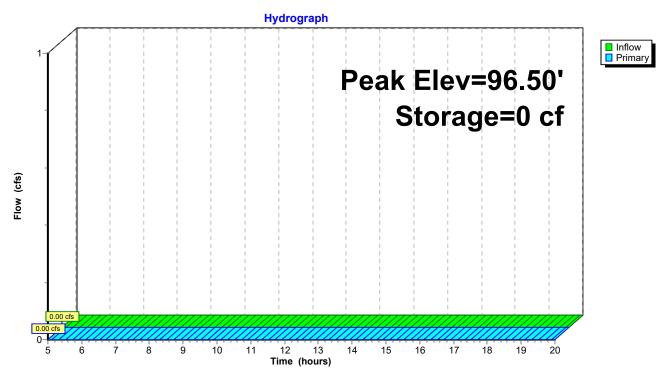
Center-of-Mass det. time= (not calculated: no inflow)

Volume	Inv	ert Avai	l.Storage	Storage [Description		
#1	96.	50'	209 cf	Custom	Stage Data (Pi	rismatic)Listed below (Recalc)	
Elevatio	• •	Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)		
96.5	50	72		0	0		
97.0	0	147		55	55		
98.0	00	162		155	209		
Device	Routing	In	vert Outl	et Devices	i		
#1	Primary	96		100.0 deg x 6.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir Cv= 2.49 (C= 3.11)			

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.50' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

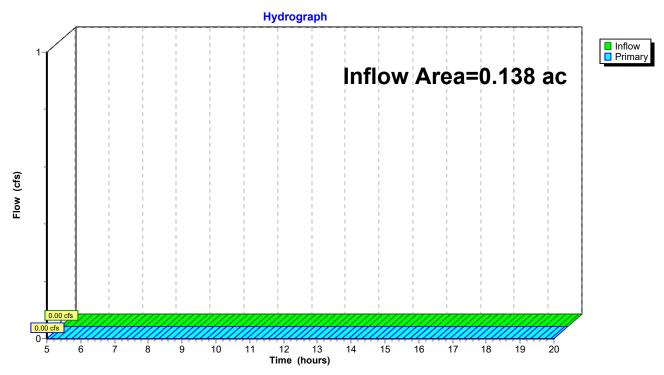
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth = 0.00" for 100-YR - 2HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 2HR. event

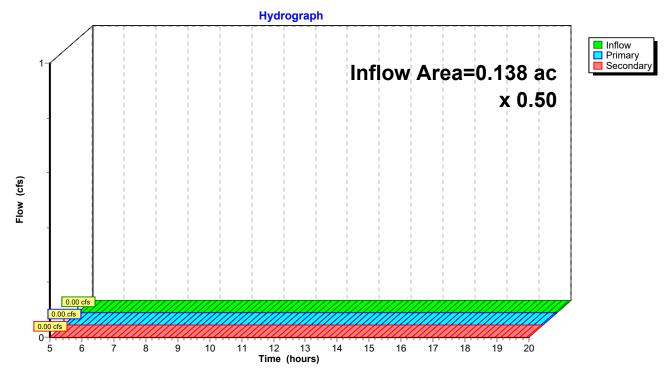
Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

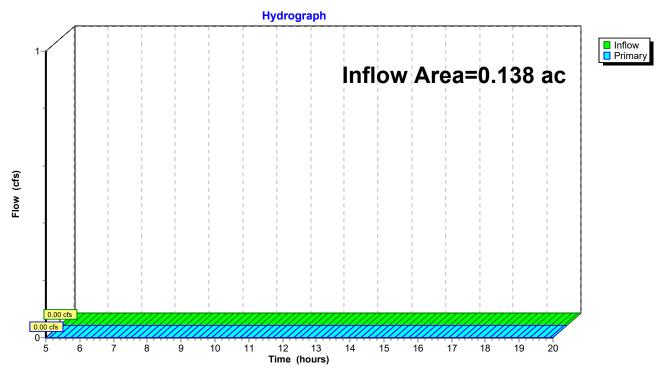
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 2HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 4.00 hrs 100-YR - 4HR. Rainfall=6.08"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth=0.00"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=0.00 cfs 0.000 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth=0.00"

Flow Length=150' Slope=0.0083 '/' Tc=9.4 min CN=73 Runoff=0.00 cfs 0.000 af

Pond 4P: Rock Void

Peak Elev=97.50' Storage=0 cf Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.000 af Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=96.50' Storage=0 cf Inflow=0.00 cfs 0.000 af

Outflow=0.00 cfs 0.000 af

Link 2L: Outfall

Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af

Link 6L: Split

x 0.50 Inflow=0.00 cfs 0.000 af

Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af

Link 10L: Combined Outflow

Inflow=0.00 cfs 0.000 af

Primary=0.00 cfs 0.000 af

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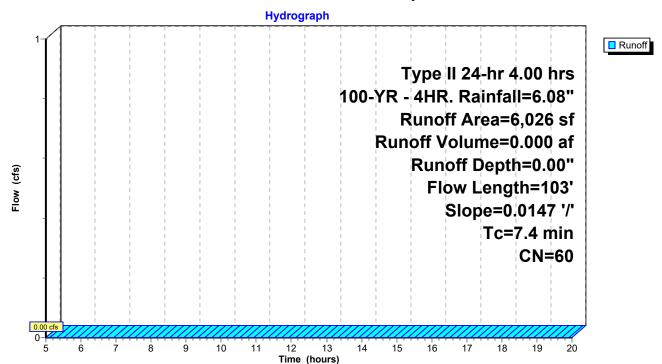
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 4.00 hrs 100-YR - 4HR. Rainfall=6.08"

_	Α	rea (sf)	CN Description									
*		6,026	60 V	0 Woods/grass comb., Poor, HSG B								
		6,026	1	100.00% Pervious Area								
	Tc Length Slope Velocity Capacity (min) (feet) (ft/ft) (ft/sec) (cfs)					Description						
	7.4	103	0.0147	0.23		Lag/CN Method, Woods						

Subcatchment 1S: Pre-Developed Basin I



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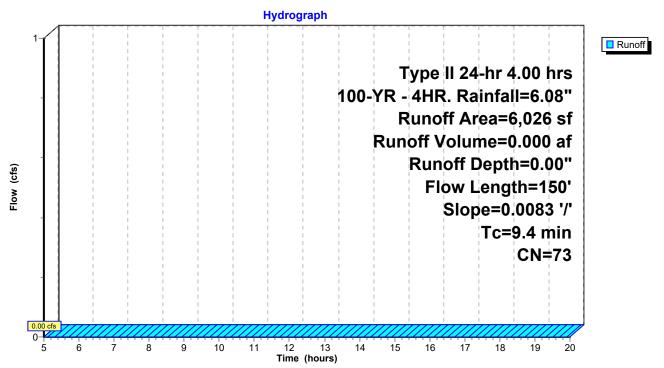
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 4.00 hrs 100-YR - 4HR. Rainfall=6.08"

	Aı	rea (sf)	CN	Description								
		300	98	Roofs, HSC	oofs, HSG B							
		97	98	Paved park	aved parking, HSG B							
*		973	65	Uncompact	ncompacted Gravel 35% Void							
		1,283	85	Gravel road	avel roads, HSG B							
		3,373	67	Brush, Poo	sh, Poor, HSG B							
		6,026	73	Weighted A	verage							
		5,629		93.41% Pe	rvious Area							
		397		6.59% Impe	ervious Are	a						
	Тс	Length	Slope	Velocity	Capacity	Description						
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	9.4	150	0.0083	0.27		Lag/CN Method,						

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 4.00 hrs 100-YR - 4HR. Rainfall=6.08"

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Summary for Pond 4P: Rock Void

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.50' @ 5.00 hrs Surf.Area= 973 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

Volume	Inv	ert Avail.9	Storage	Storage D	escription	
#1	97.	50'	170 cf		tage Data (Perall x 35.0%	rismatic)Listed below (Recalc) Voids
Elevatio		Surf.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	Inve	ert Outl	et Devices		
#1	Primary	98.0	Hea	d (feet) 0.2	0 0.40 0.60	road-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32

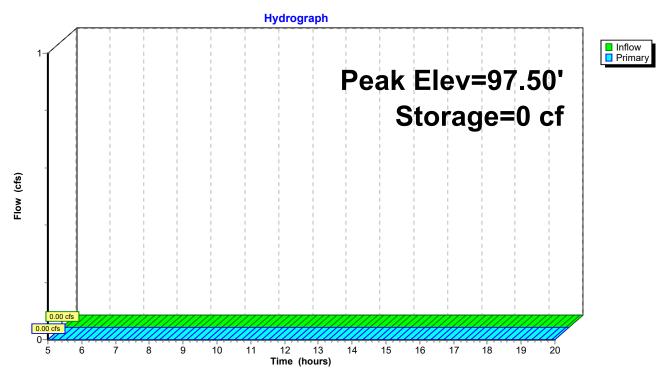
Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=97.50' (Free Discharge)
—1=Broad-Crested Rectangular Weir(Controls 0.00 cfs)

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Pond 4P: Rock Void



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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 4HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 5.00 hrs Surf.Area= 60.960 ac Storage= 0.000 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

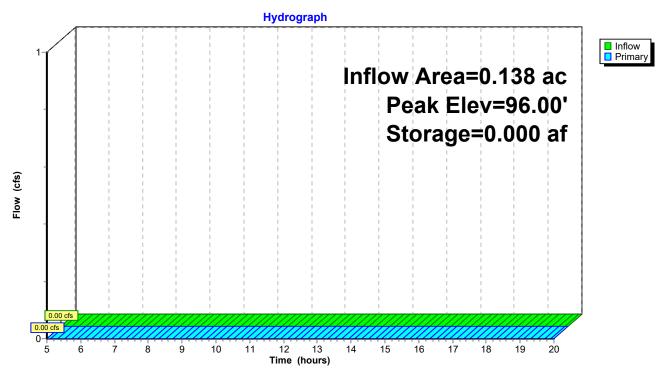
Volume	Invert	Avail.Storaç	je Stoi	age Description	
#1	96.00'	356.830	af Cus	tom Stage Data (Prisma	tic)Listed below (Recalc)
Elevatio (fee			Store e-feet)	Cum.Store (acre-feet)	
96.0	0 60.96	0	0.000	0.000	
97.0	0 265.60	0 16	3.280	163.280	
98.0	0 121.50	0 19	93.550	356.830	
Device	Routing		Outlet D		
#1	Primary			eg x 8.0' long x 1.00' rise 9 (C= 3.11)	Sharp-Crested Vee/Trap Weir

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



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Summary for Pond 9P: North Pond

Inflow 0.00 cfs @ 5.00 hrs, Volume= 0.000 af =

Outflow 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min =

5.00 hrs, Volume= Primary 0.00 cfs @ 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 96.50' @ 5.00 hrs Surf.Area= 72 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

Volume	Inv	ert Avail.	Storage	Storage [Description	
#1	96.	50'	209 cf	Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio	• •	Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
96.5	0	72		0	0	
97.0	0	147		55	55	
98.0	0	162		155	209	
Device	Routing	Inv		et Devices		
#1	Primary	96.9		. 0 deg x 6. 2.49 (C= 3		rise Sharp-Crested Vee/Trap Weir

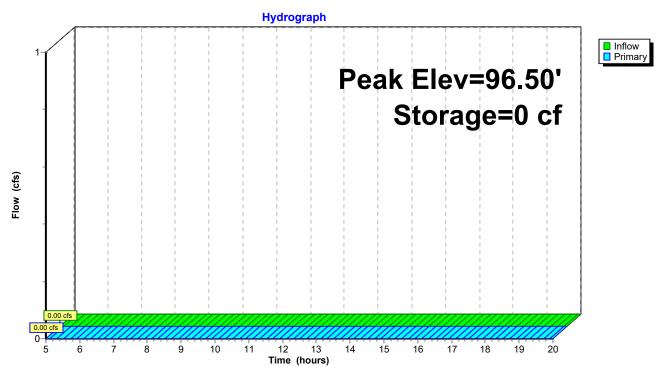
Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.50' (Free Discharge) 1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 9P: North Pond



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Summary for Link 2L: Outfall

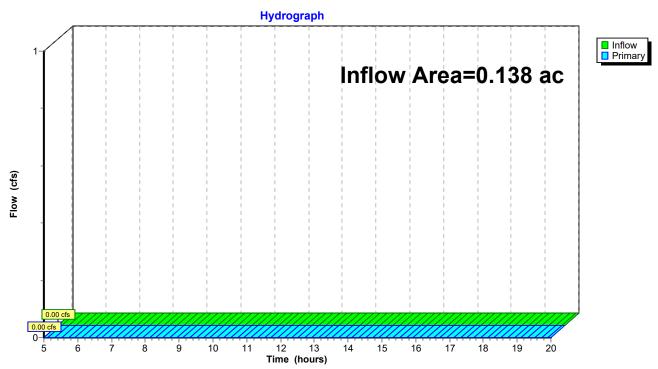
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth = 0.00" for 100-YR - 4HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 4HR. event

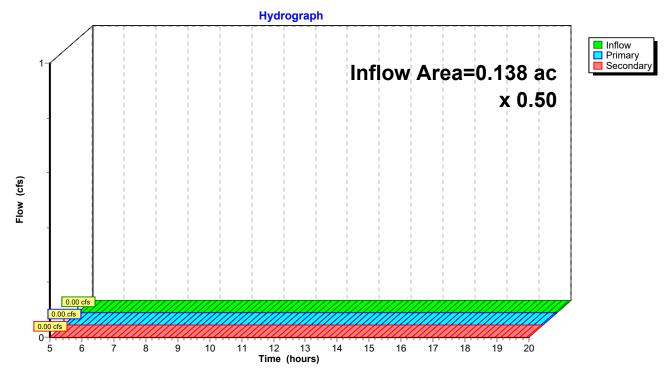
Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

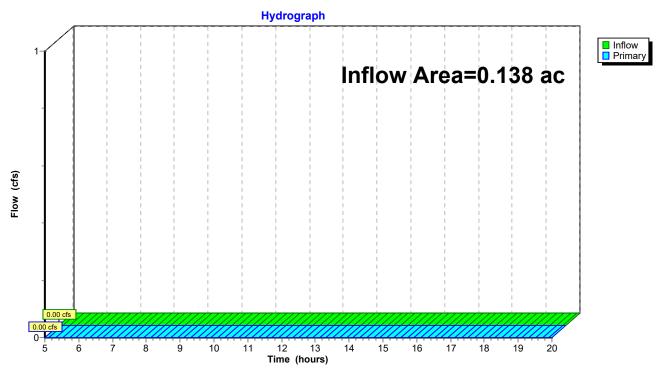
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.00" for 100-YR - 4HR. event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: Pre-DevelopedBasin I

Runoff Area=6,026 sf 0.00% Impervious Runoff Depth>0.82"

Flow Length=103' Slope=0.0147 '/' Tc=7.4 min CN=60 Runoff=0.07 cfs 0.009 af

Subcatchment3S: Post Developed Basin I

Runoff Area=6,026 sf 6.59% Impervious Runoff Depth>1.02"

Flow Length=150' Slope=0.0083'/' Tc=9.4 min CN=73 Runoff=0.09 cfs 0.012 af

Pond 4P: Rock Void

Peak Elev=98.00' Storage=170 cf Inflow=0.04 cfs 0.006 af

Outflow=0.03 cfs 0.002 af

Pond 5P: South Pond

Peak Elev=96.00' Storage=0.006 af Inflow=0.04 cfs 0.006 af

Outflow=0.00 cfs 0.000 af

Pond 9P: North Pond

Peak Elev=96.91' Storage=42 cf Inflow=0.03 cfs 0.002 af

Outflow=0.02 cfs 0.001 af

Link 2L: Outfall

Inflow=0.07 cfs 0.009 af

Primary=0.07 cfs 0.009 af

Link 6L: Split

x 0.50 Inflow=0.09 cfs 0.012 af

Primary=0.04 cfs 0.006 af Secondary=0.04 cfs 0.006 af

Link 10L: Combined Outflow

Inflow=0.02 cfs 0.001 af Primary=0.02 cfs 0.001 af

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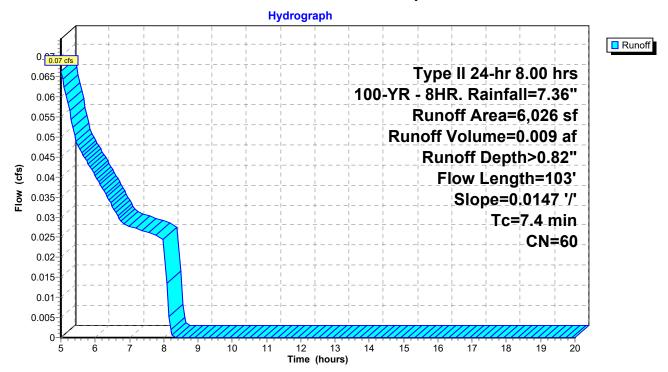
Summary for Subcatchment 1S: Pre-Developed Basin I

Runoff = 0.07 cfs @ 5.00 hrs, Volume= 0.009 af, Depth> 0.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

	Α	rea (sf)	CN [Description								
*		6,026	60 V	Woods/grass comb., Poor, HSG B								
		6,026	1	00.00% Pe	ervious Are	a						
	Tc	Length	Slope	,	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	7.4	103	0.0147	0.23		Lag/CN Method, Woods						

Subcatchment 1S: Pre-Developed Basin I



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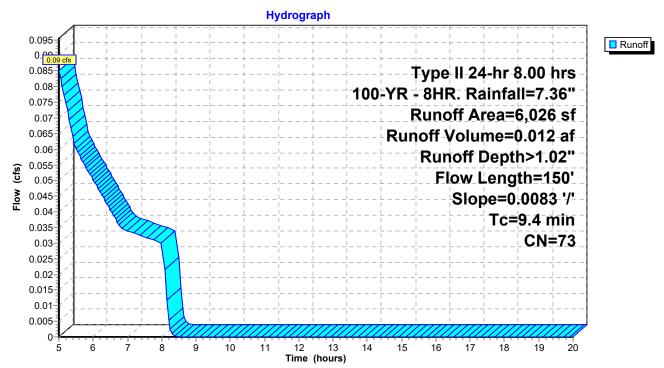
Summary for Subcatchment 3S: Post Developed Basin I

Runoff = 0.09 cfs @ 5.00 hrs, Volume= 0.012 af, Depth> 1.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

	Α	rea (sf)	CN I	Description								
		300	98 I	Roofs, HSC	Roofs, HSG B							
		97	98 I	Paved parking, HSG B								
*		973	65 l	Jncompact	ncompacted Gravel 35% Void							
		1,283	85 (ravel roads, HSG B								
		3,373	67 I	Brush, Poo	sh, Poor, HSG B							
		6,026	73 \	Neighted A	verage							
		5,629	(93.41% Pei	rvious Area							
		397	(6.59% Impe	ervious Area	a						
	Tc	Length	Slope	Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	9.4	150	0.0083	0.27		Lag/CN Method,						

Subcatchment 3S: Post Developed Basin I



Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

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Summary for Pond 4P: Rock Void

Inflow = 0.04 cfs @ 5.00 hrs, Volume= 0.006 af

Outflow = 0.03 cfs @ 6.70 hrs, Volume= 0.002 af, Atten= 27%, Lag= 102.0 min

Primary = 0.03 cfs @ 6.70 hrs, Volume= 0.002 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 98.00' @ 6.70 hrs Surf.Area= 973 sf Storage= 170 cf

Plug-Flow detention time= 128.0 min calculated for 0.002 af (33% of inflow)

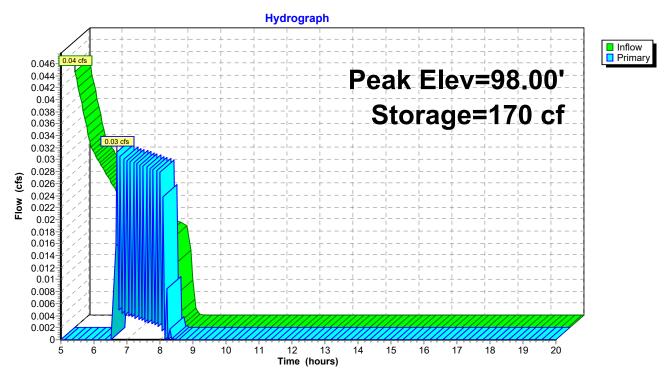
Center-of-Mass det. time= 67.1 min (443.4 - 376.3)

Volume	Inv	ert Avail.S	Storage	Storage D	escription	
#1	97.	50'	170 cf		Stage Data (Perall x 35.0%	rismatic)Listed below (Recalc) Voids
Elevation (fee		Surf.Area (sq-ft)		Store c-feet)	Cum.Store (cubic-feet)	
97.5	50	973		0	0	
98.0	00	973		487	487	
Device	Routing	Inve	rt Outl	et Devices		
#1	Primary	98.0	Hea	d (feet) 0.2	0.40 0.60	road-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32

Primary OutFlow Max=0.03 cfs @ 6.70 hrs HW=98.00' (Free Discharge)
1=Broad-Crested Rectangular Weir (Weir Controls 0.03 cfs @ 0.17 fps)

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Pond 4P: Rock Void



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Summary for Pond 5P: South Pond

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 0.51" for 100-YR - 8HR. event

Inflow = 0.04 cfs @ 5.00 hrs, Volume= 0.006 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.00' @ 8.55 hrs Surf.Area= 60.979 ac Storage= 0.006 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

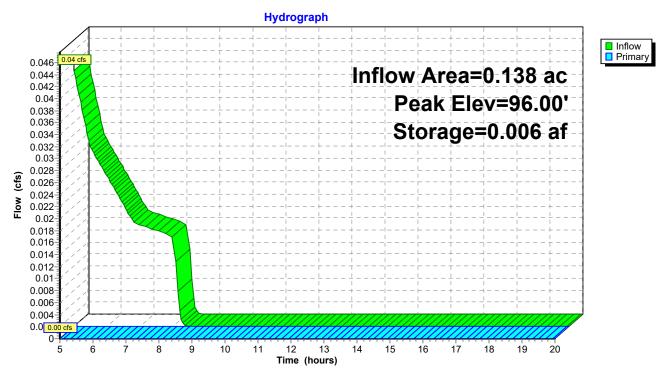
Volume	Invert A	vail.Storage	Storage Description
#1	96.00'	356.830 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee		Inc.S (acre-	
96.0	0 60.960	0	.000 0.000
97.0	0 265.600	163	.280 163.280
98.0	0 121.500	193	.550 356.830
Device	Routing	Invert O	utlet Devices
#1	Primary		00.0 deg x 8.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir v= 2.49 (C= 3.11)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

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Pond 5P: South Pond



Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

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Summary for Pond 9P: North Pond

Inflow = 0.03 cfs @ 6.70 hrs, Volume= 0.002 af

Outflow = 0.02 cfs @ 7.41 hrs, Volume= 0.001 af, Atten= 41%, Lag= 42.7 min

Primary = 0.02 cfs @ 7.41 hrs, Volume= 0.001 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.91' @ 7.40 hrs Surf.Area= 133 sf Storage= 42 cf

Plug-Flow detention time= 43.3 min calculated for 0.001 af (54% of inflow)

Center-of-Mass det. time= 22.2 min (465.6 - 443.4)

Invert /	Avail.Stor	age Stora	age Description	
96.50'	20	9 cf Cust	tom Stage Data (Prismatic)Listed below (Recalc)	
_				
	72	0	0	
1	47	55	5 55	
1	62	155	5 209	
	Invert 96.90'	100.0 deg	x 6.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir	
	96.50' Surf.Ar (sq	96.50' 20 Surf.Area (sq-ft) 72 147 162 uting Invert	96.50' 209 cf Cust Surf.Area Inc.Store (sq-ft) (cubic-feet) 72 (2) 147 55 162 155 uting Invert Outlet Deven	96.50' 209 cf Custom Stage Data (Prismatic)Listed below (Recalc) Surf.Area Inc.Store Cum.Store (sq-ft) (cubic-feet) (cubic-feet) 72 0 0 147 55 55 162 155 209 uting Invert Outlet Devices

Primary OutFlow Max=0.01 cfs @ 7.41 hrs HW=96.91' (Free Discharge)
1=Sharp-Crested Vee/Trap Weir (Weir Controls 0.01 cfs @ 0.29 fps)

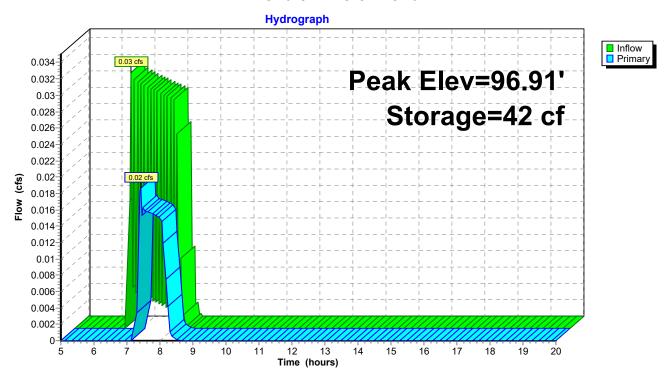
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Pond 9P: North Pond



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Summary for Link 2L: Outfall

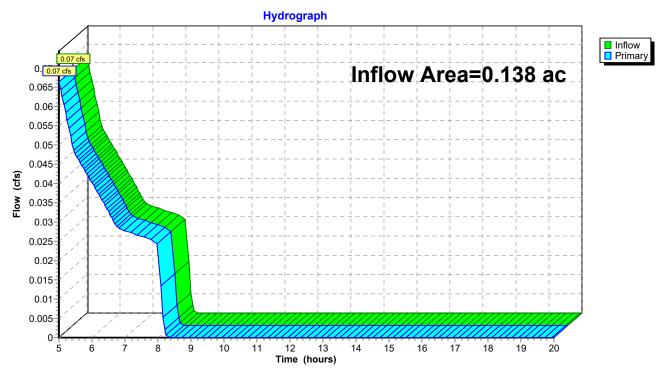
Inflow Area = 0.138 ac, 0.00% Impervious, Inflow Depth > 0.82" for 100-YR - 8HR. event

Inflow = 0.07 cfs @ 5.00 hrs, Volume= 0.009 af

Primary = 0.07 cfs @ 5.00 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 2L: Outfall



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Summary for Link 6L: Split

Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth > 1.02" for 100-YR - 8HR. event

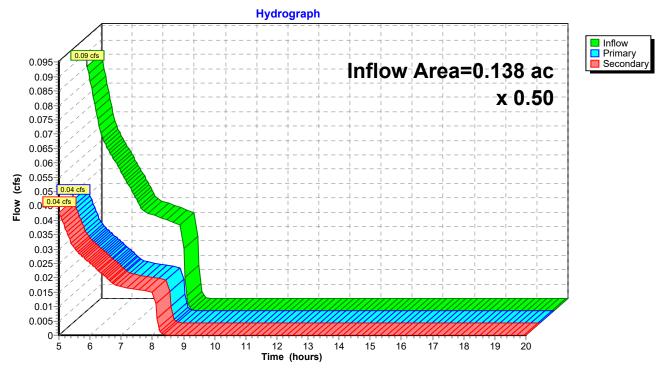
Inflow = 0.09 cfs @ 5.00 hrs, Volume= 0.012 af

Primary = 0.04 cfs @ 5.00 hrs, Volume= 0.006 af, Atten= 50%, Lag= 0.0 min

Secondary = 0.04 cfs @ 5.00 hrs, Volume= 0.006 af

Primary outflow = Inflow x 0.50, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 6L: Split



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Summary for Link 10L: Combined Outflow

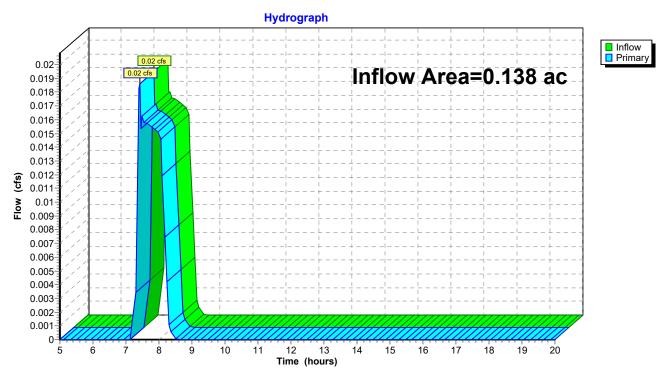
Inflow Area = 0.138 ac, 6.59% Impervious, Inflow Depth = 0.09" for 100-YR - 8HR. event

Inflow = 0.02 cfs @ 7.41 hrs, Volume= 0.001 af

Primary = 0.02 cfs @ 7.41 hrs, Volume= 0.001 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 10L: Combined Outflow



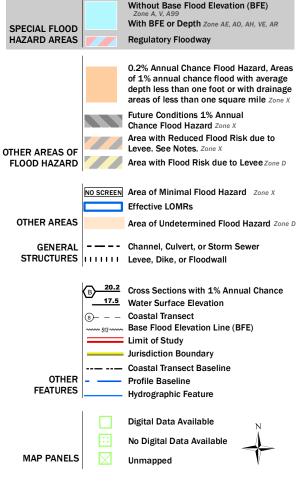
Appendix C – FEMA Firm Map

National Flood Hazard Layer FIRMette





SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT





The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 3/13/2020 at 2:51:02 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Appendix D – Rainfall Distribution Data

Appendix D

District Rainfall Distribution Data

Values for P_{total} (inches)¹

For the counties of Madison, Hamilton, Suwannee, Columbia, Baker and Union.

Frequency	Duration (hours)									
(years)	1	2	4	8	24	72	168	240		
3	2.50	2.64	3.08	3.52	4.56	5.80	7.30	8.00		
10	3.05	3.70	4.40	5.12	6.72	8.30	10.10	11.80		
25	3.45	4.30	5.12	6.00	7.92	10.00	12.30	14.00		
100	4.20	5.10	6.08	7.36	9.84	12.40	14.00	16.10		

For the counties of Taylor, Lafayette, Dixie, Gilchrist, Levy, Alachua and Bradford.

Frequency	Duratio	Duration (hours)										
(years)	1	2	4	8	24	72	168	240				
3	2.60	3.20	3.80	4.48	6.00	7.60	9.50	10.80				
10	3.20	4.00	4.80	5.84	7.92	8.90	11.00	12.50				
25	3.60	4.40	5.28	6.56	8.64	11.00	13.00	15.00				
100	4.40	5.40	6.72	8.00	11.04	13.80	16.00	18.00				

1-HOUR DURATION

T(hrs)	P/P _{total}	I/P _{total}
0	0	0
.1	.020	.200
.2	.080.	.600
.3	.200	1.200
.4	.410	2.100
.5	.625	2.150
.6	.805	1.800
.7	.915	1.100
.8	.985	0.700
.9	.995	0.100
1.0	1.000	0

¹ Values for durations through 24 hours were taken from Florida Department of Transportation intensity curves. Values for durations greater than 24 hours were taken from National Weather Service Technical Paper No. 49, 1964.



District Boundary

