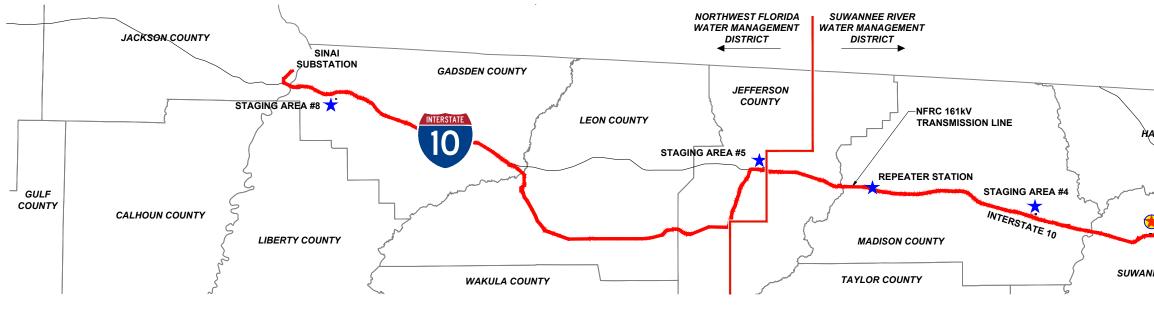
## **GULF POWER COMPANY** NFRC TRANSMISSION LINE PROJECT **TEMPORARY STAGING AREA NO. 3** SITE PLAN EXHIBIT

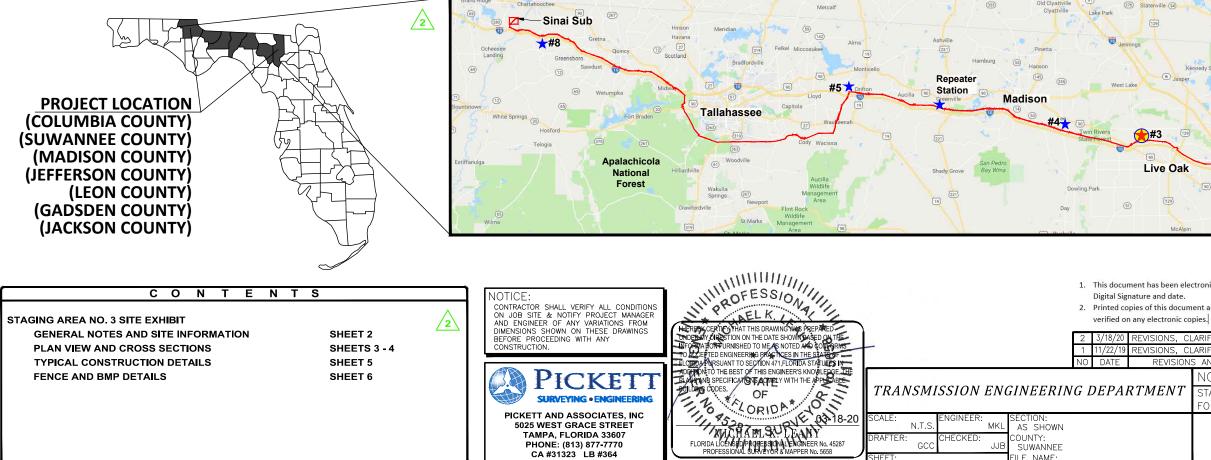
GC

1 OF 6

SUWANNEE

TILE NAME: NFRC EXH SA02 R02.dwg





CA #31323 LB #364



### **GULF POWER COMPANY** NFRC TRANSMISSION LINE PROJECT **TEMPORARY STAGING AREA NO. 3** SITE PLAN EXHIBIT

G CODES STATE

20

OF LORIDA'

CONTRACTOR SHALL VERIFY ALL CONDITIONS ON JOB SITE & NOTIFY PROJECT MANAGER AND ENGINEER OF ANY VARIATIONS FROM

PICKETT AND ASSOCIATES. INC.

5025 WEST GRACE STREET TAMPA, FLORIDA 33607 PHONE: (813) 877-7770 CA #31323 LB #364

ICKET

SURVEYING + ENGINEERING

DIMENSIONS SHOWN ON THESE DRAWINGS BEFORE PROCEEDING WITH AN' CONSTRUCTION.

ROFESSION

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AND SRECIFICATIONS COMPLY WITH THE APPLICABLE

PROFESSIONAL ENGINEER NO. 45287 PROFESSIONAL ENGINEER NO. 45287 PROFESSIONAL ENGINEER NO. 5658

03-18-20

#### SURVEYOR'S NOTES:

- 2. ELEVATIONS ARE TO NORTH AMERICAN VERTICAL DATUM OF 1988 AND ARE FOR REFERENCE AND GRAPHICAL DISPLAY PURPOSES ONLY. TEMPORARY BENCHMARKS WILL BE SET AT EACH CROSSING SITE LOCATION AS REQUIRED.
- 3. SURVEY INFORMATION SHOWN HEREON PERTAINING TO RIGHT-OF-WAY AND EASEMENTS IS BASED ON A SURVEYS PROVIDED BY GULF POWER.
- 4. NO UNDERGROUND UTILITIES AND/OR IMPROVEMENTS SHOWN HEREON A SUBSURFACE INVESTIGATION WAS NOT PERFORMED AS PART OF THIS SURVEY.
- 5. THE AERIAL IMAGERY SHOWN HEREIN ARE A COMBINATION OF 2015/2016/2017 ORTHOGRAPHIC IMAGES OBTAINED FROM THE FLORIDA DEPARTMENT OF TRANSPORTATION A+PLUS WEBSITE.
- EASEMENT TO GULF POWER.

#### CONSTRUCTION NOTES:

- ESTABLISHED.
- THE WORK.
- ON SHEET 5.
- **GENERAL GRADING CHARACTERISTICS.**
- OF RECORD.

#### FLOOD ZONE NOTES

FLOOD INSURANCE RATE MAPS:

#### MAP NUMBER 12023C0167D (DATED 11-02-18)

- Digital Signature and date.
  - verified on any electronic copies.

SCALE:     ENGINEER:     SECTION:       N.T.S.     MKL     AS       SHEET:     GCC     JJB       2     0F     6	SA02 R02.c	wa	Guif Power*	STAGING AREA I SITE PLAN EXHI		3			
TRANSMISSION ENGINEERIN	IG DEPA	RTMENT	STAGING AREA NO. 3 SITE PLAN EXHIBIT FOR TEMPORARY LAYDOWN YARDS						
			NORTH FLORIDA RESILIE	NCY CONNECTION (NFR	C)				
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	2 3/18/2	REVISIONS, CI	LARIFICATIONS FOR RAI#2 RESPONSE	12-20-19	GCC .	JJB I	MKL		

E: N.T.S. ENGINEER: MKL TTER: GCC CHECKED: JJB T: CHECKED: JJB T: FILE NAME:				STAGING AREA NO. 3 SITE PLAN EXHIBIT FOR TEMPORARY LAYDOWN YARDS STAGING AREA NO. 3 SITE PLAN EXHIBIT					
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	1	11/22/19	REVISIONS, CL	ONS, CLARIFICATIONS FOR RAI RESPONSE 11-22-19 GCC JJB MKL					
	2	3/18/20	REVISIONS, CL	ARIFICATIONS FOR RAI#2 RESPONSE	12-20-19	GCC	JJB	MKL	

SITE DATA:

#### STAGING AREA #3 - SUWANNEE COUNTY - SRWMD 153RD ROAD, LIVE OAK, FL PID 36-01S-12E-0981400.0000

#### PROJECT NARRATIVE:

TEMPORARY STAGING AREA NO. 3 IS REQUIRED TO STAGE AND STORE CONSTRUCTION MATERIALS (POLES, CONDUCTOR, INSULATORS, ETC.) AND EQUIPMENT (DRILL RIGS, LINE TRUCKS, CRANES, ETC.) FOR THE NORTH FLORIDA RESILIENCY CONNECTION (NFRC) PROJECT. THE NFRC PROJECT IS A 176 MILE LENGTH CORRIDOR THAT IS BROKEN UP INTO APPROXIMATELY 20 MILE SEGMENTS RESULTING IN THE NEED FOR FIVE (5) TOTAL TEMPORARY STAGING AREAS. EACH STAGING AREA IS SIZED TO BE ABLE TO STORE ITS PRO-RATA SHARE OF THE MATERIAL. THE AVERAGE SITE SELECTION CRITERIA IS FOR EACH STAGING AREA TO BE APPROXIMATELY 16.0 ACRES TOTAL WITH APPROXIMATELY 12.6 ACRES OF DEVELOPED AREA. THE DEVELOPED AREA WILL CONSIST OF AN AT GRADE #57 CRUSHED LIMEROCK SURFACE ON UNCOMPACTED SUBBASE TO FACILITATE THE STORAGE OF POLES AND EQUIPMENT ALONG WITH A GEOWEB SEDIMENT CONTAINMENT CELL PERIMETER ROAD OF #57 CRUSHED LIMEROCK FILL TO FACILITATE ACCESS.

TEMPORARY STAGING AREA NO. 3 SITE PLAN STORMWATER DESIGN HAS BEEN REVIEWED TO ENSURE THAT EXISTING SURFACE WATER FLOW WILL FLOW SIMILAR TO IT'S PREDEVELOPED CONDITION. THE DIFFERENCE BETWEEN PRE AND POST-DEVELOPED RUNOFF WILL BE STORED ON SITE WITH DRY RETENTION PONDS AND/OR THE ROCK VOIDS. DISCHARGE WILL NOT EXCEED THE PRE-DEVELOPED CONDITION FOR WATER TREATMENT AND RECOVERY. THIS SITE WILL USE A COMBINATION OF THE VOID SPACE BETWEEN THE #57 CRUSHED LIMEROCK AND A SERIES OF CHECK DAMN SYSTEMS MADE WITH WATER AND ROOT BARRIER SYSTEMS FOR STORAGE FOR THE FIRST 1" OR THE FIRST 1/2" OF RUNOFF, WHICH EVER IS GREATER, AS DIRECTED BY THE GOVERNING SUWANNEE RIVER WATER MANAGEMENT DISTRICT STORMWATER DESIGN MANUAL REQUIREMENTS. GULF POWER HAS DONE EXTENSIVE TESTING ON THIS VOID RATIO AND HAS DETERMINED THAT A 35% VOID RATIO PROVIDES A GOOD CONSERVATIVE VALUE. ANY TREATMENT VOLUMES NOT ABLE TO RECOVER IN THE ROCK VOIDS WILL UTILIZE DRY RETENTION PONDS FOR THE REMAINING VOLUME. THE TREATMENT VOLUMES ARE DESIGNED TO RECOVER WITHIN THE 72 HOUR REQUIREMENT. SOIL BORINGS AND DOUBLE RING INFILTROMETER TESTING WAS PERFORMED AT EACH SITE TO FACILITATE THE DESIGN OF EACH DRY POND AND ROCK VOID STORAGE AREA. REFER TO GEOGRAPHICAL REPORT FOR DETAILS.

TEMPORARY STAGING ARE NO. 3 WILL REMAIN IN PLACE FOR THE DURATION OF THE PROJECT. AT THE CONCLUSION OF THE PROJECT, THIS SITE WILL BE RETURNED TO ITS PRE-CONSTRUCTION STATE BY THE CONTRACTOR. THE ANTICIPATED DURATION IS APPROXIMATELY 12 - 18 MONTHS.

#### GENERAL SITE NOTES:

- CONSTRUCTION AND MAINTENANCE ACCESS TO TEMPORARY STAGING AREA NO. 3 WILL BE GAINED VIA EXISTING ROAD RIGHT-OF-WAY OF 153RD ROAD. CONNECTOR APRONS WILL BE CONSTRUCTED IN ACCORDANCE WITH COUNTY / STATE REQUIREMENTS.
- TEMPORARY STAGING AREA NO. 3 EXISTS ON EASEMENTS MADE THRU LAND NEGOTIATIONS WITH CURRENT LANDOWNERS. THIS SITE HAS 2 UNDERGONE A FULL EVALUATION / VETTING RELATIVE TO AVOIDANCE OF ENVIRONMENTAL, CULTURAL, AND WILDLIFE HABITAT IMPACT. NO TREE REMOVAL WILL BE NECESSARY TO FACILITATE CONSTRUCTION OF THIS SITE.
- TEMPORARY STAGING AREA NO. 3 WILL CONFORM WITH ALL FEDERAL, STATE, AND LOCAL ORDINANCES AND REGULATIONS FOR LONG 3. TERM STORAGE MATERIALS
- DELIVERIES AND ACTIVE USE OF THIS SITE WILL BE CONSISTENT WITH CONSTRUCTION HOURS. 4
- ALL PROPOSED SEMI-PERVIOUS MATERIAL WILL BE INSTALLED AT THE EXISTING NATURAL GROUND ELEVATION THROUGHOUT THE SITE TO 5. MINIMIZE IMPEDANCE OF THE EXISTING WATERSHED.
- WHEN THE PROPOSED ACTIVITIES OCCUR ADJACENT TO WETLANDS, APPROPRIATE SEDIMENT CONTROL METHODS WILL BE USED, AS REQUIRED. SEDIMENT CONTROLS INCLUDE THE INSTALLATION OF STAKED SILT FENCES ALONG PROPOSED FILL ADJACENT WETLANDS. NO FILL OR GRADING WORK WILL OCCUR IN WETLAND AREAS.

1. NORTH, THE BEARINGS AND THE COORDINATES SHOWN HEREON ARE REFERENCE TO THE WEST ZONE OF THE FLORIDA STATE PLANE COORDINATE SYSTEM, NORTH AMERICAN DATUM OF 1983 (NAD 83/ FLW-83) CORS 2011...

6. PROPERTY THE PROPOSED STAGING AREA IS LOCATED ON IS THERE BY GRANTED

1. CONTRACTOR SHALL INSTALL AND MAINTAIN BMP'S PER THE APPROVED SWPPP (STORM WATER POLLUTION PREVENTION PLAN, I.E. SILT FENCE, TURBIDITY BARRIER) AND WWACCM MANUAL AROUND THE PERIMETER TO THE WORK ZONES DURING CONSTRUCTION. BMP'S SHALL ONLY BE REMOVED AFTER ALL CONSTRUCTION HAS BEEN COMPLETED AND

2. CONTRACTOR SHALL CONSTRUCT PONDS AND/OR SWALES AS SHOWN IN THE DRAWINGS. CONTRACTOR SHALL SOD THE SIDE SLOPES AFTER GRADING TO STABILIZE THE DISTURBED SOIL AND EMBANKMENTS AND TO CONTROL EROSION. SEEDING AND SODDING SHALL BE PERFORMED IN ACCORDANCE WITH THE LATEST FDOT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION. THE SIDES OF POND/SWALE AREAS SHALL BE SODDED AND THE BOTTOMS SHALL BE SEEDED AND MULCHED.CONTRACTOR SHALL DISC THE AREAS TO EMBED THE SEED AND MULCH AND SHALL THEN RE-COMPACT THE SURFACE.CONTRACTOR SHALL MAINTAIN THE SOD AND SEED UNTIL FINAL ACCEPTANCE OF

3. CONTRACTOR SHALL INSTALL CHECK DAMS ALONG THE EXISTING (1) ONE FOOT CONTOUR ELEVATIONS AS SHOWN ON THE PLANS AND ALONG THE INTERIOR OF THE ROADWAYS BETWEEN THE ROCK LAYDOWN AREAS AND THE EDGE OF GEOWEB ROAD. SEE DETAIL 3

4. CONTRACTOR SHALL REMOVE THE TOP LAYER OF VEGETATION ON THE SITE BEFORE BEGINNING ANY GRADING OR SITE WORK. SITE SHALL MAINTAIN EXISTING SLOPES AND

5. IF ANY OBSTRUCTIONS OR VARIANCES EXIST, CONTRACTOR MUST NOTIFY THE ENGINEER

## 1. FLOOD ZONE INFORMATION BASED ON THE COLUMBIA COUNTY, FLORIDA

#### 2. APPLICABLE FLOOD ZONE DELINEATIONS PER THE ABOVE REFERENCED FLOOD INSURANCE RATE MAP ARE AS FOLLOWS:

#### ZONE X AREA OUTSIDE THE 100-YEAR FLOOD PLAIN

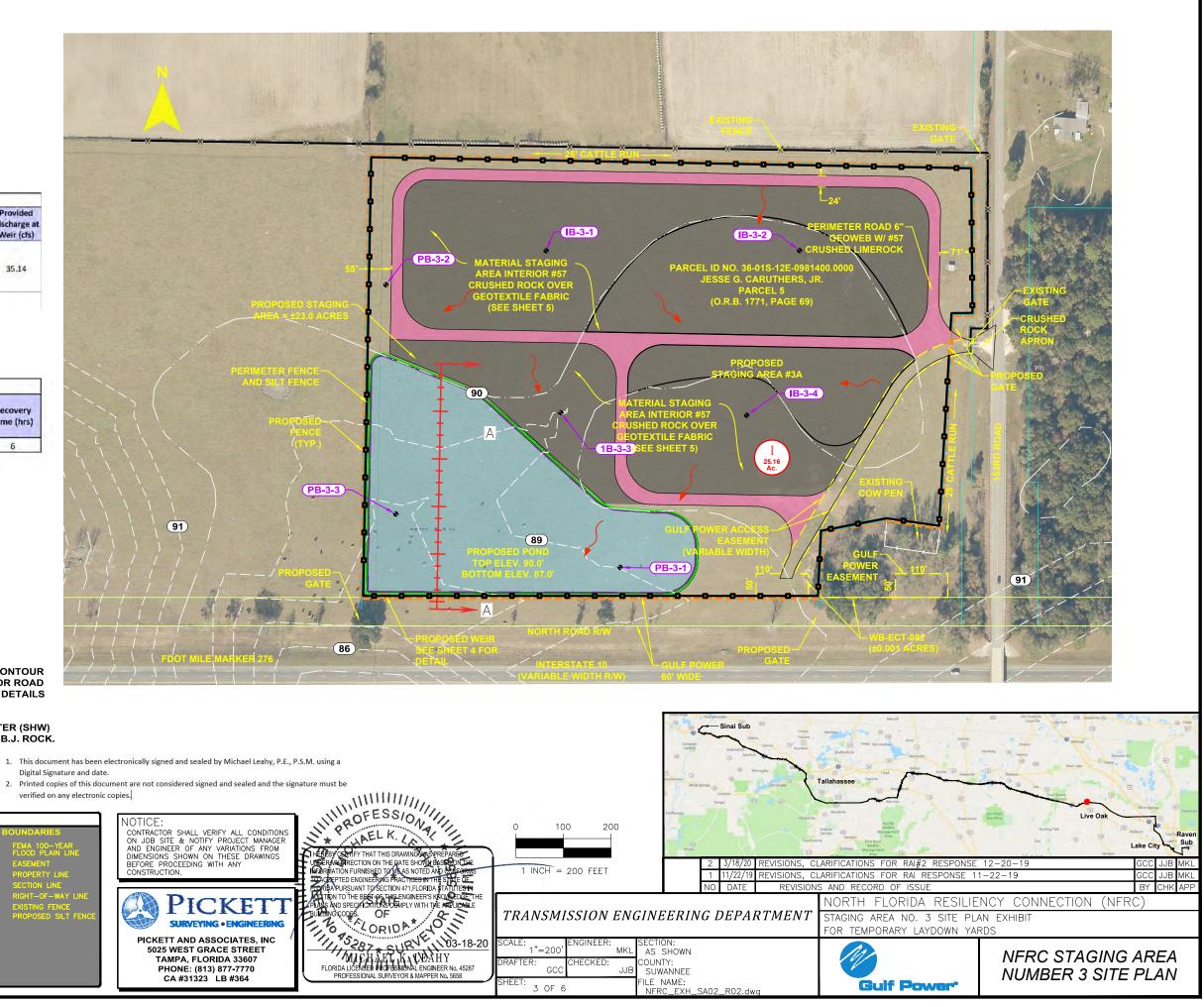
1. This document has been electronically signed and sealed by Michael Leahy, P.E., P.S.M. using a

2. Printed copies of this document are not considered signed and sealed and the signature must be

#### Staging Area #3 - Suwannee County - SRWMD 153rd Road, Live Oak, FL PID 36-01S-12E-0981400.0000

		Table 3:	Pond Storage Da	ata			
Basin No.	Elevation (ft, NAVD 88)		Area (ac)	Provided Volume (acft)	Required Volume (acft)	Provided Discharge at Weir (cfs)	
	Top of Pond	op of Pond 90.0					
20.0	Peak Water Elev.	88.9		12.13	7.45	35.14	
ň.	Weir Elev.	88.5					
	Bottom of Pond	87.5	4.85	$1 \rightarrow 1$			

	Table 4: Sumr	nary of Treatme	nt Volume and Recovery	
Basin No.	Treatment	Treatmen	Recovery	
	Volume Required (acft)	Rock Voids	Water Quality Basins	Time (hrs)
r	1.17	2.32	Not Required for Treatment	6

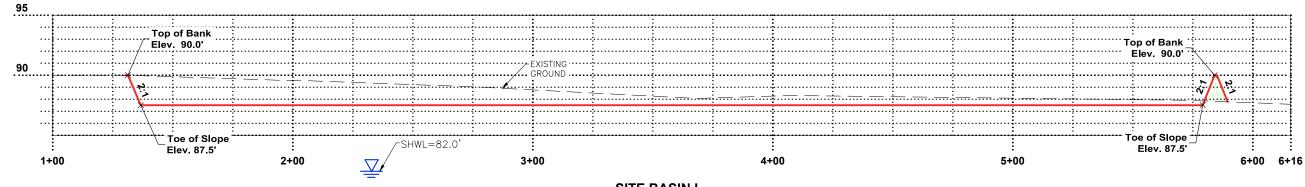


#### GENERAL NOTES:

- CHECK DAMS WILL BE INSTALLED ALONG EXISTING (1) ONE FOOT CONTOUR ELEVATIONS AS SHOWN, AND AS A BARRIER BETWEEN THE INTERIOR ROAD EDGE AND GRAVEL LAYDOWN AREA. SEE NOTES ON SHEET 2 AND DETAILS ON SHEET 5.
- INFORMATION OF WATER TABLE DEPTHS FOR SEASONAL HIGH WATER (SHW) 2 ELEVATIONS IS BASED ON GEOTECHNICAL REPORTS PROVIDED BY B.J. ROCK.
- INTERIOR CRUSHED ROCK SHALL NOT BE COMPACTED (TYP.).
- FILL SHALL NOT BE PLACED IN WETLAND AREAS (TYP.).
- Digital Signature and date.
- 2. Printed copies of this document are not considered signed and sealed and the signature must be
- verified on any electronic copies.

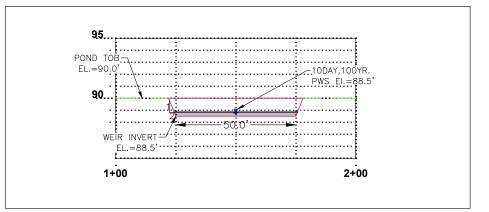


#### Staging Area #3 - Suwannee County - SRWMD 153rd Road, Live Oak, FL PID 36-01S-12E-0981400.0000

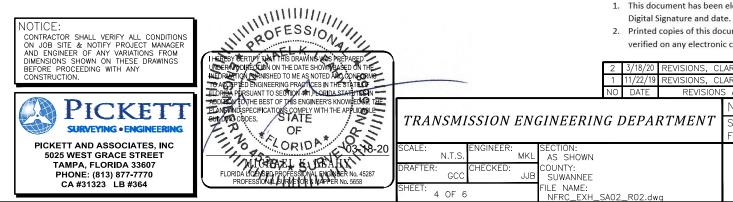


SITE BASIN I CROSS SECTION VEIW A-A

> LOOKING EAST HORZ. SCALE = 1" = 40' VERT. SCALE = 1" = 8'



SITE BASIN I WEIR CROSS SECTION HORZ. SCALE = 1" = 40' VERT. SCALE = 1" = 8'



LEGEND

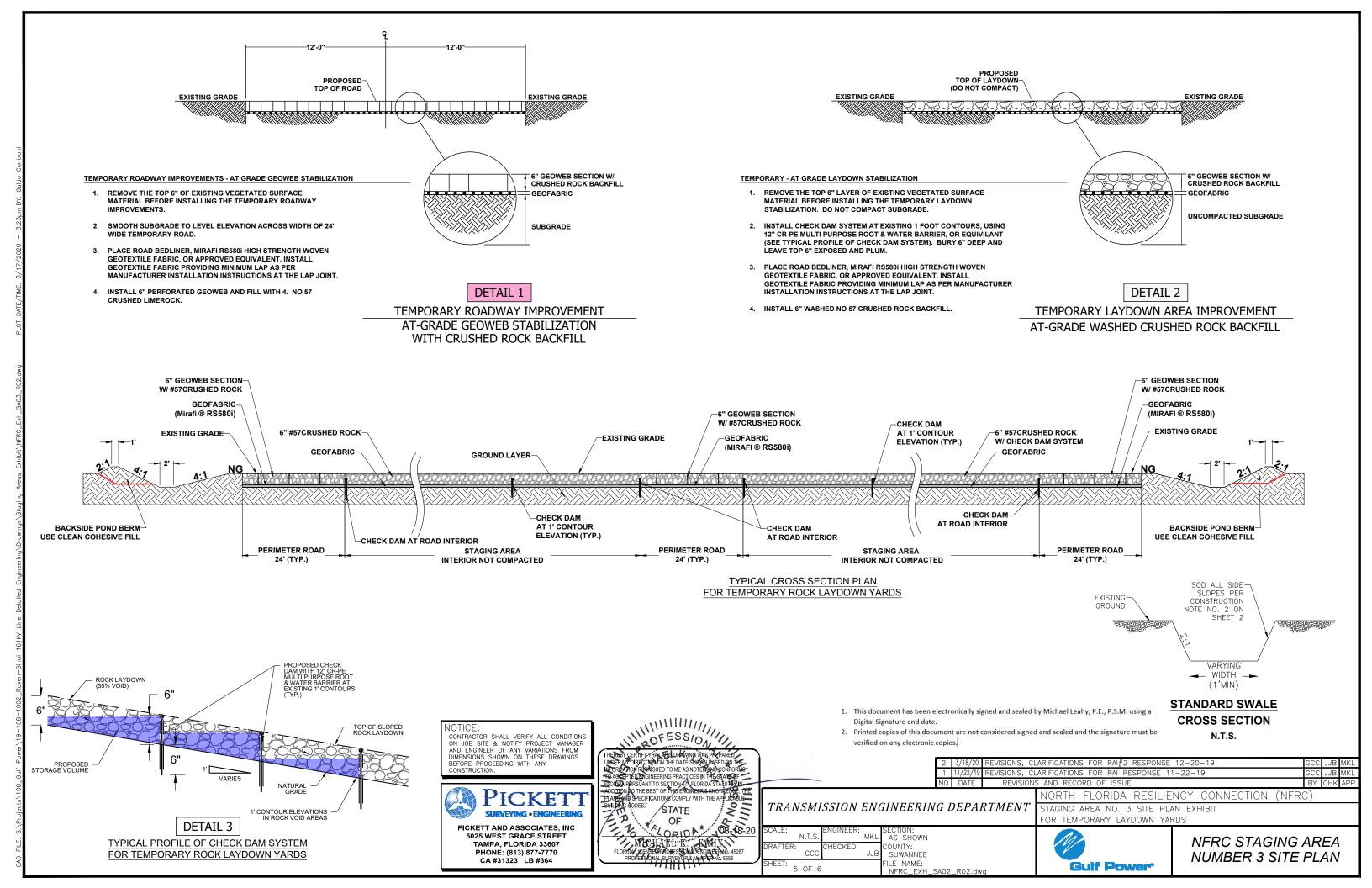
EXISTING GROUND
 PROPOSED GROUND

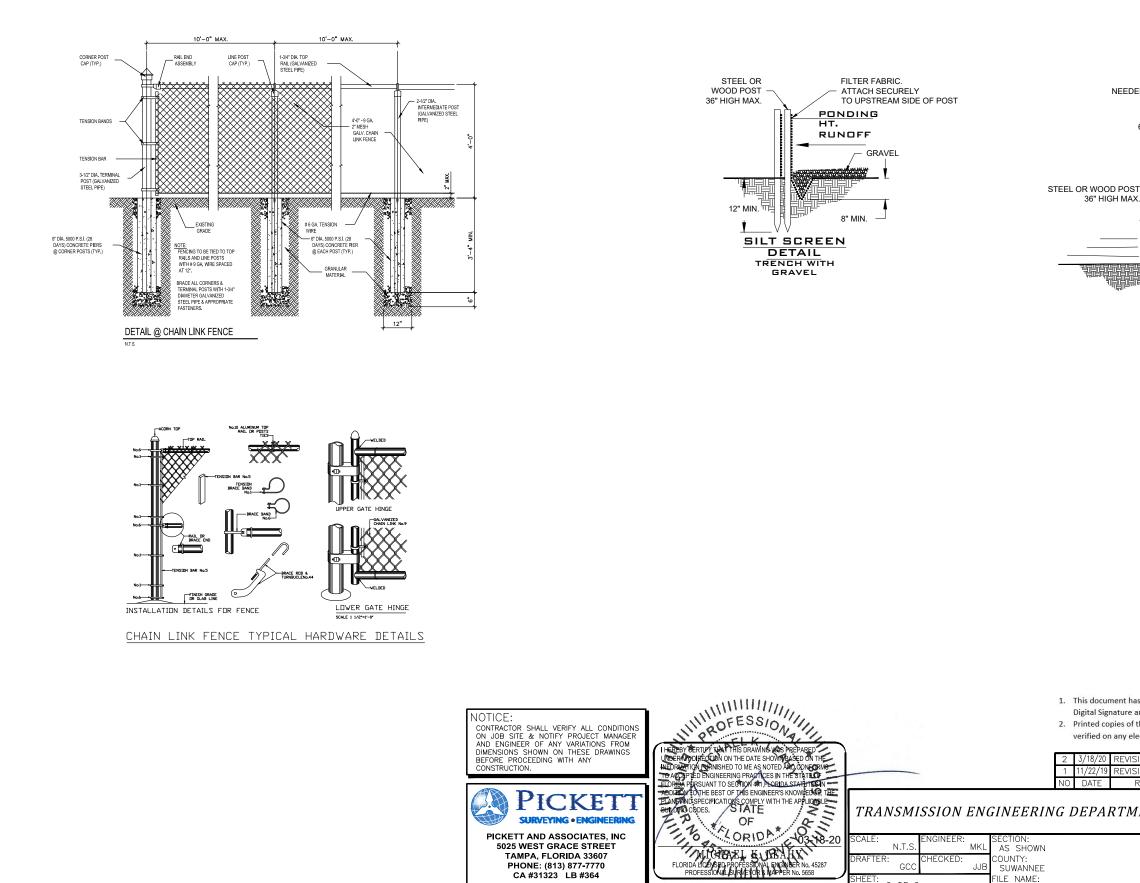
#### SEE SHEET 2 FOR NOTES & SITE DETAILS SEE SHEET 5 FOR TYPICAL CONSTRUCTION DETAILS

 This document has been electronically signed and sealed by Michael Leahy, P.E., P.S.M. using a Digital Signature and date.

2. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

ONS, CL	ARIFICATIONS FOR RAI#2 RESPONSE	12-20-19	GCC	JJB	MKL					
ONS, CL	NS, CLARIFICATIONS FOR RAI RESPONSE 11-22-19 GCC JJB MI									
EVISIONS	S AND RECORD OF ISSUE		BY	CHK	APP					
	NORTH FLORIDA RESILIENCY CONNECTION (NFRC)									
ENT	STAGING AREA NO. 3 SITE PLAN EXHIBIT FOR TEMPORARY LAYDOWN YARDS									
	Gulf Power*	NFRC STAGING NUMBER 3 SITE								

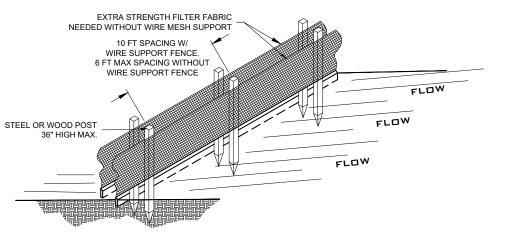




CA #31323 LB #364

## PERIMETER FENCE DETAILS

## **EROSION CONTROL DETAILS**



1. This document has been electronically signed and sealed by Michael Leahy, P.E., P.S.M. using a Digital Signature and date.

2. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

2 3/18/20 REVIS 1 11/22/19

NO DATE

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6 OF 6

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6

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	NORTH FLORIDA RESILIENCY CONNECTION (NFRC)									
ENT	STAGING AREA NO. 3 SITE PLA FOR TEMPORARY LAYDOWN YAR									
	Gulf Power*	NFRC STAGING NUMBER 3 SITE								

**Temporary Staging Area #3** 

#### **Stormwater Calculations**

for the

#### North Florida Resiliency Connection Project



Gulf Power 15430 Endeavor Drive Jupiter, FL 33478

Prepared by:



Pickett and Associates, Inc. 5025 W. Grace Street Tampa, FL 33607

#### **Table of Contents**

1.0	Site Data3
2.0	Project Narrative
3.0	Stormwater Calculations4
	Appendix A – Geotechnical Report (includes recovery analysis)
	Appendix B - HydroCAD Report
	Appendix C – Firm Map
	Appendix D – SRWMD Rainfall Distribution Data
	Appendix E – SRWMD Boundary Map

#### 1.0 Site Data

Columbia County – SRWMD 153<sup>rd</sup> Road, Live Oak, FL PID 36-01S-12E-0981400.0000 Basin Area = 25.16 acres Developed Area = 13.62 acres Flood Zone X per FIRM Map 12121C0130B effective 09-28-07 Design Storm, Non Ag: 100 year, SCS Type II Distribution. 1-, 2-, 4-, 8-, 24-hour and 3-, 7-, and 10-day duration. Recovery (Attenuation)

1. Provide treatment volumes within 72 hours following the end of the design storm event.

#### 2.0 Project Narrative

Temporary Staging Area #3 will stage and store construction materials (poles, conductor, insulators, etc.) and equipment (drill rigs, line trucks, cranes, etc.). The developed area will consist of an at grade #57 crushed limerock surface to facilitate the storage of poles and equipment along with a perimeter road to facilitate access. The site has been reviewed to ensure that existing surface water flow will not be impeded and existing water quality will not be adversely impacted. All proposed semi-pervious material will be installed at the existing natural ground elevation throughout the site to prevent impedance of the existing watershed.

The staging area will use the void space between the #57 crushed limerock for storage for the first 1" of runoff. Gulf Power has done extensive testing on this void ratio and has determined that a 35% void ratio provides a good conservative value. In addition to utilizing the voids for storage, each site will have a swale / berm constructed on the low side(s) of each to ensure no stormwater runoff escapes to adjacent properties. Each site will also have a dry retention pond to account for attenuation. The ponds will be designed to recover within 72 hours. Soil Borings and Double Ring Infiltrometer Testing have been performed at each site to facilitate the design of each dry pond. The site will use the interior uncompacted gravel as additional area for recovery by incorporating the use of a check dam system. Since the site has a slight grade change, an impervious, flexible water barrier (CR-PE12-20) will be installed along each contour line to slow the progression of water over the site to allow recovery within 72 hours. This is detailed in the construction drawings.

The staging area will remain in place for the duration of the project. At the conclusion of the project, each staging area will be returned to its pre-construction state. The anticipated duration is approximately 12 - 18 months.

Construction and maintenance access to each staging area will be gained via existing road right-of-way. Connector aprons will be constructed in accordance with county / state requirements.

Deliveries and active use of staging areas will be consistent with construction hours.

No tree removal will be necessary to facilitate construction of staging area #3.

#### 3.0 Stormwater Calculations

The SCS TR-20 method was used to calculate the pre and post-development peak runoff. The time of concentration was generated from the sheet, shallow concentrated flow and Lag/CN method. A complete list of the procedure follows.

#### Assumptions and Methodology

The SRWMD requires that the difference between the 100-year pre-developed and post-developed storm volume be stored on-site with the maximum release rate not exceed the pre-developed flow, Q. Per the SRWMD Handbook, the 100-year storm shall be evaluated for the greatest of the 1, 2, 4, 8, and 24 hour, 3, 7, and 10 days storms.

- Storm Frequency Type II 100 Year, 1, 2, 4, 8, and 24 hour, 3, 7, and 10 day storms
- Runoff Curve Number Weighted Curve Numbers were calculated for each area
  - Existing Conditions Curve Number Range: 58
  - o Post-Developed Condition Curve Number Range: 58-85
- Calculation of Time of Concentrations
  - Lag/CN Method Which is used for areas of 2000 acres or less. The formula is provided below:
    - $T_c = 0.00526 \times L^{0.8} (1000/CN-9)^{0.7} \times S^{-0.5}$
- Peak Flow Rate Calculations HydroCAD Version 10.0
- Pond Recovery Calculations PONDS Version 3.3

#### Pre-Development Summary

Staging Area 3 has mild slopes of up to 1% and generally consists of grass. Table 1 below includes the results of the pre-development drainage area runoff calculations for the peak flow. These were developed using the topography which can be seen on the plan set and HydroCAD (Appendix B). Table 1 summarizes the peak flows for the various 100-year design storm in the pre-developed condition. The storm with the greatest runoff volume was used in the calculations. In this case, the 100-year, 10-day storm generated the greatest runoff and thus was used as the design storm.

Table 1: Pre-Developed Peak Discharge											
Sub- Basin	Area		Time of Concentration	Type II, 100-Year Storm, Q <sub>100</sub> (CFS)							
DdSIII	(Acre)		(Min.)	1 HR	2 HR	4 HR	8 HR	24 HR	3 DAY	7 DAY	10 DAY
Ι	25.16	58	222.3	3.06	5.67	8.97	11.56	15.68	23.38	28.42	35.22

#### Post-Development Summary

Upon completion of construction, Staging Area 3 will consist of uncompacted gravel laydown yard with compacted gravel drives. The water quality basin will be located at the low point within the site. Table 2 below includes the results of the post- development calculations for the 100-year, 1, 2, 4, 8, and 24 hour, 3, 7, and 10 day peak flows. These were developed using the topography which can be seen on the plan set and HydroCAD (Appendix B). The difference between the pre-development and post-development storm will be contained within the pond, and anything greater will be conveyed through the outflow weir per the Suwannee River Management District Design Requirement. The storm with the

greatest runoff volume was used in the calculations. Again, in this case, the 100-year, 10-day storm generated the greatest runoff and thus was used as the design storm.

	Table 2: Post-Developed Peak Discharge										
Sub-		Weighted ) CN	Time of Concentration	Type II, 100-Year Storm, Q <sub>100</sub> (CFS)							
Basir	(Acre)		(Min.)	1 HR	2 HR	4 HR	8 HR	24 HR	3 DAY	7 DAY	10 DAY
I	25.16	64	193.3	4.09	7.52	12.88	16.18	21.01	30.19	36.12	44.01

Table 3 below summarizes the stormwater quality basin design and key pond elevations with required and provided volumes. It shows that the basin provides the required amount of freeboard (1-foot) and storage required to retain the peak runoff. Peak water surface elevation calculations for detention ponds were developed using HydroCAD (Appendix B).

	Table 3: Pond Storage Data									
Basin No.	Elevation (ft, NAVD 88)		VD 88) Area (ac)		Required Volume (acft)	Provided Discharge at Weir (cfs)				
	Top of Pond	90.0	5.09							
	Peak Water Elev.	88.9		12.13						
Ι	Weir Elev.	88.5			7.45	35.14				
	Bottom of Pond	87.5	4.85							

#### Water Quality/Treatment Methodology

The NWFWMD Handbook requires that all stormwater management systems provide the minimum state water quality treatment requirements. The method utilized for this project consists of one or a combination of percolation in the existing soils within the rock voids of the laydown storage and/or percolation within the stormwater quality basin. To determine the treatment runoff volume, the first 1.0-inch of rainfall was used along with the composite runoff coefficient for each sub-basin. This was compared with the volume from the first 0.5-inch rainfall without the coefficient. The greater volume was used for treatment evaluation and recovery. The calculations can be found starting on Page 6.

Recovery was calculated utilizing the PONDS software, as approved by the district. The rate of recovery was calculated within both the rock voids and if needed, the water quality basins. To model the rock voids, we calculated the available void space within the laydown area using a 35% uncompacted void ratio. An adjusted stage-storage table was input into the PONDS model utilizing a one-half foot increment stage, which corresponds to the height of the check dam. All treatment volumes must recover within 72-hours. See Table 4 for a summary of treatment volumes and recovery times for each sub-basin within the staging area.

Table 4: Summary of Treatment Volume and Recovery								
	Treatment	Treatmen	Recovery					
Basin No.	Volume Required (acft)	Rock Voids	Water Quality Basins	Time (hrs)				
I	1.17	2.32	Not Required for Treatment	6				

## Water Quality Recovery Volume Calculations Areas:

$$(1,096,103 . .) \times \left(\frac{1 .}{43,560 . .}\right) = 25.16 .$$

$$h = (576,632 . .) \times \left(\frac{1 .}{43,560 . .}\right) = 13.24 .$$

$$h = (98,135 . .) \times \left(\frac{1 .}{43,560 . .}\right) = 2.25 .$$

$$= (221,654 . .) \times \left(\frac{1 .}{43,560 . .}\right) = 5.09 .$$

$$= 25.16 . -13.24 . -2.25 . -5.09 . = 4.58 .$$

#### **Composite Runoff Coefficient:**

$$= \frac{\left[\left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area \end{array}\right) + pond \ area }{\left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ laydown \ area \end{array}\right) + rock \ road \ area } \left(\begin{array}{cc} rock \ area \ area \end{array}\right) + rock \ area \ area \end{array}\right) + rock \ area \ a$$

$$=\frac{[(0.5 \quad 13.24 \quad .) + (0.7 \quad 2.25 \quad .) + (1.0 \quad 5.09 \quad .) + (0.17 \quad 4.58)]}{25.16} = .56$$

#### Total Treatment Volume from 1 inch of Rainfall:

$$= () \times (1 h) \times )$$

$$= (.56) \times (1 ) \times (25.16) \times (\frac{1}{12}) = 1.17 . .$$

Total Treatment Volume from ½ inch of Rainfall:

$$= (0.5 h) \times$$
)  
= (0.5 .) × (25.16 .) ×  $\left(\frac{1}{12}\right) = 1.05$  . .

The treatment volume for the project is the larger value, **1.17 Ac.-Ft**.

Appendix A – Geotechnical Investigation

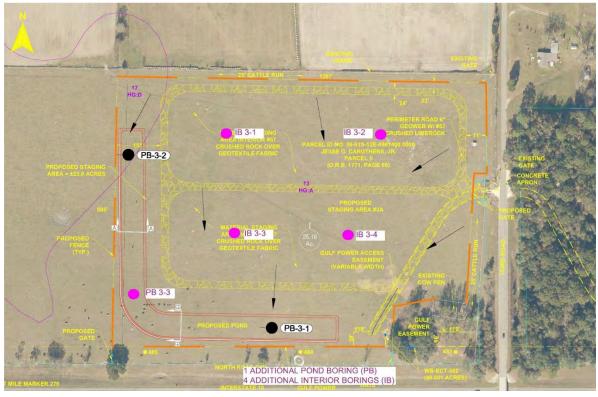


# **GEOTECHNICAL REPORT**





## NFRC STAGING AREA NO. 3



## SUWANNEE COUNTY, FLORIDA

MARCH 2020 BJR 19-198B





March 13, 2020

Mike Leahy, P.E. **Pickett & Associates** 5025 W. Grace Street Tampa, FL 33607

Geotechnical Exploration Report NFRC Staging Area No. 3 Suwannee County, Florida BJR No. 19-198B

Dear Mr. Leahy:

**BJ Rock, LLC (BJR)** has completed the geotechnical exploration for the referenced project as authorized by Pickett & Associates for Gulf Power. The purposes of this study were to explore general subsurface conditions for the proposed staging areas and to use the data obtained to develop engineering recommendations to guide the design of the planned ponds/swales. This report describes our exploration procedure, presents the data obtained, and presents our conclusions and recommendations regarding the geotechnical engineering aspects of the design.

BJR appreciates the opportunity to participate in this project and we trust that the information included in this report is sufficient for your design. If you have any questions or comments concerning the contents of this report, please contact us.

Sincerely,

BJ Rock, LLC BJR FL Certificate of Authorization No. 29100

> John C. Peak, P.E. Sr. Geotechnical Engineer FL P.E. License No. 57018

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#### ATTACHMENTS

Field Test Location Plan (Figure 1) Soil Boring Logs (Figure 2) Stormwater Pond Recovery Analysis Results NRCS Soil Survey Data Field Testing Standards and Procedures



#### PROJECT INFORMATION

#### Existing Site

Based on the information provided for our review from Pickett & Associates, we understand a staging area is planned off on 153<sup>rd</sup> Road in Live Oak in Suwannee County, Florida (Figure 1).

#### Project Approach

The objective of the geotechnical investigation for the proposed project was to obtain information concerning the subsurface conditions in order to make geotechnical engineering estimates and recommendations in each of the following areas:

- Soil stratigraphy at the boring locations and the development of the approximate soil profile.
- General location and description of potentially deleterious materials which may interfere with construction or new structure performance, including buried or surficial existing fills, organics, construction debris, etc.
- Identification of some critical design or construction details, including present groundwater levels, estimated wet season levels, and seasonal fluctuations in the specified areas.

#### Scope of Work

In order to address the above objectives, our scope of work for this project included the following:

- Reviewed available published information on the site, including the United States Department of Agriculture (USDA) National Resources Conservation Service (NRCS) soil survey data for Suwannee County.
- Conducted a subsurface exploration program consisting of the advancement of auger borings with DRI / field permeability testing for the pond/swales, subsurface sampling, and field testing.
- Measured the stabilized groundwater levels at the boring locations.
- Reviewed and visually classified the recovered soils in the laboratory using the Unified Soil Classification System (ASTM D 2487). Developed the general soil stratigraphy at the boring locations.
- Performed geotechnical engineering studies and analyses in order to develop geotechnical engineering recommendations for each of the objectives previously discussed for the proposed project.
- Performed stormwater pond recovery analysis per referenced staging area. Analysis performed by our subconsultant, Native GeoSciences, Inc.
- Prepared a geotechnical report that summarizes the course of our study, the field and laboratory data generated, the subsurface conditions encountered, stormwater pond recovery analysis results and our geotechnical engineering recommendations for the proposed project.



#### **Soil Survey Review**

According to the USDA NRCS "Soil Survey of Suwannee County", the soil types generally present on the site are attached in the appendix and are generalized as follows: *Blanton-Alpin-Bonneau complex and Falmouth-Bonneau-Blanton complex.* 

#### SUBSURFACE EXPLORATION

#### Field Exploration Procedures

The procedures used by BJ Rock, LLC for field sampling and testing are in general accordance with industry standards of care and established geotechnical engineering practice. BJR performed 7 auger borings to approximate depths of up to 10 feet each with 7 field permeability tests at the proposed locations.

Our staff located the staked borings in the field per the plans and field information provided by Pickett & Associates. The approximate testing locations are noted on the provided Field Test Location Plan (Figure 1) in the Appendix. The standards and procedures for the Standard Penetration Test (SPT) Boring and soil sample handling and classification are described in our Field Testing Standards and Procedures in the Appendix.

#### Field Exploration Results

#### Subsurface Conditions

The auger borings generally encountered fine to slightly silty fine sands, clayey fine sands and sandy clays to an approximate depth of 10 feet below existing grade. The soil testing results are shown on the attached Soil Boring Logs (Figure 2) in the Appendix.

#### Field Permeability Test

The field permeability falling head tests were performed at the specified location on the site as shown on Figure 2 in the Appendix. The tests were performed at approximate depths of 1.5 and  $3^{+/-}$  feet below existing grade. The tests were performed utilizing slotted casing seated in a uniform soil condition. The results of the tests are as follows:

Recommended Existing Groundwater Parameters for Pond Design				
	STA	GING AREA 3 - NFR	C TRANSMISSION LI	NE FPL
PB Test	Test Depth (ft)	Vertical Infiltration (ft/day)	Estimated Horizontal Infiltration (ft/day)*	Recommended SHGWL Depth (ft)
IB-3-1	1.5	0.08	0.16	3
IB-3-2	3	2	4	6
IB-3-3	3	2	4	6
IB-3-4	3	1	2	5
PB 3-1	3	2.6	5.2	6
PB 3-2	2	0.2	0.4	3
PB-3-3	3	1	2	6
*	Estimated horizontal permeability rate is 2x the vertical permeability test result.			
Note:	Horizontal and vertical permeability rates do not include a factor of safety.			



#### Groundwater

Groundwater was not encountered to an approximate depth of 10 feet below existing ground surface in the soil test borings performed in November 2019 and February 2020. Based on our past site experience, the results of our investigation, and our review of the NRCS soil survey, it is our opinion that the seasonal high groundwater table will be encountered at an approximate depth of 3 to  $6^{+/-}$  feet below existing ground surface in the areas of borings performed. Significant fluctuations in the groundwater levels should be expected due to seasonal variations in rainfall, runoff, and other site-specific factors across the site such as shallow perched conditions due to encountered clayey soils.

#### Stormwater Pond Recovery Analysis

Native GeoSciences (NGS) completed the stormwater pond recovery analysis for the staging area(s). NGS utilized the commercially available software PONDS (version 3.3) to perform the stormwater pond recovery analysis. The analysis included recovery of the treatment volume within 30 days. The description of the input parameters and a Copy of the PONDS software outputs are included in the Attachments in the Appendix.

#### SITE PREPARATION RECOMMENDATIONS

#### Site Stripping

Prior to any construction, the site must be properly prepared. To prepare the site for construction, all existing topsoil, muck, debris, vegetation, and large roots down to finger-size should be removed, including a 5-foot margin in a horizontal direction away from the footprints of the structures. The resulting excavations should be backfilled with soils as discussed in the structural fill section of this report.

#### Proofrolling

Following site stripping and any related excavation activity, and prior to any fill placement, proofrolling of the on-site soils should be performed. We recommend using a vibratory roller having a static weight of at least ten tons. Placement of fill materials may then proceed. Compaction of the fill materials should continue until the roller has made at least ten passes over all areas of the site and the soils appear to be relatively firm and unyielding. Half of the roller passes should be perpendicular to the direction of travel of the other passes. Proofrolling should be closely monitored by our engineering technician to look for unusual deflection of the soils beneath the compacting equipment. If unusual or excessive deflection is observed, the areas should be undercut to firm soils and backfilled with structural fill placed in maximum one-foot thick lifts. Backfill soils should be of the same composition and should be compacted to the same criteria as structural fill soils.

#### Structural Fill

#### Definition

Soil used for structural fill can be defined as clean fine sand containing less than twelve percent material by weight that is finer than a number 200 sieve (fines) (material conforming to SP to SP-SM in the Unified Soil Classification System) and less than 5 percent organics by weight. However, materials containing up to 25 percent fines (materials conforming to SC or SM in the Unified Soil Classification System) may be utilized as structural fill, if their plasticity index is less than 20 and the working subgrade is at least 2 feet above water or groundwater level.



If fill material with higher fines content is used (< 25 percent fines), the material will require the use of compaction equipment designed for clayey soils. This includes a sheeps foot or vibratory pad foot roller. In addition, a disk could be required to assist with drying the clayey soils in order to place them at or near their optimum moisture content. These materials must be placed in 6-inch thick maximum lifts so that they can be effectively compacted with a vibratory pad foot roller.

#### Soil Suitability Recommendations

Based on the results of the auger borings in Figure 3, the soil materials encountered in the borings appear to be acceptable general and/or structural fill from ground surface to 1 to 10<sup>+</sup> feet below existing grade excluding any organic material, clays and unsuitable rock/shell/limestone, etc. Stratum 1 (SP/SP-SM) can be utilized as structural fill material. Stratum 2 (SM/SC) can be utilized as general fill material.

#### Placement

Fill should be placed in lifts not to exceed one foot thick. The fill material should be compacted to at least 95 percent of its modified Proctor maximum dry density (ASTM D 1557). Confined areas, such as utility trenches, should be compacted with manually operated vibratory compaction equipment.

#### TESTING AND MONITORING

Construction monitoring and testing are essential to proper site construction and performance. Compliance with the recommended foundation specification must be verified by our engineering technician familiar with the project construction. Observation of site preparation work is an integral part of the engineering recommendations contained in this report.

Safe working conditions are necessary. Temporary excavations should be sloped and/or braced as required by applicable local, state, and federal safety regulations, as well as the current Occupational Safety and Health Organization (OSHA) Excavation and Trench Safety Standards. Generally, the grading contractor is responsible for constructing stable, temporary excavations that are dewatered, shored, sloped and/or benched to maintain stability of the sides and bottom of the trench.

#### LIMITATIONS

This report has been prepared for the exclusive use of **Pickett & Associates and Gulf Power** for the specific application to the project previously discussed. Our conclusions and recommendations have been rendered using generally accepted standards of geotechnical engineering geology practice in the state of Florida. No other warranty is expressed or implied.

Our conclusions and recommendations are based on the design information furnished to us, the data obtained from the previously described subsurface exploration, and our experience. They do not reflect variations in the subsurface conditions that are likely to exist in the region of our boring and in unexplored areas of the site. These variations are due to the inherent variability of the subsurface conditions in this geologic region. Should variations become apparent during construction, it will be necessary to re-evaluate our conclusions and recommendations based upon our on-site observations of the conditions.

The site is underlain by limestone bedrock that is susceptible to dissolution and the subsequent development of karst features such as voids and sinkholes in the natural soil overburden. Construction in a sinkhole prone area is therefore accompanied by some risk that internal soil

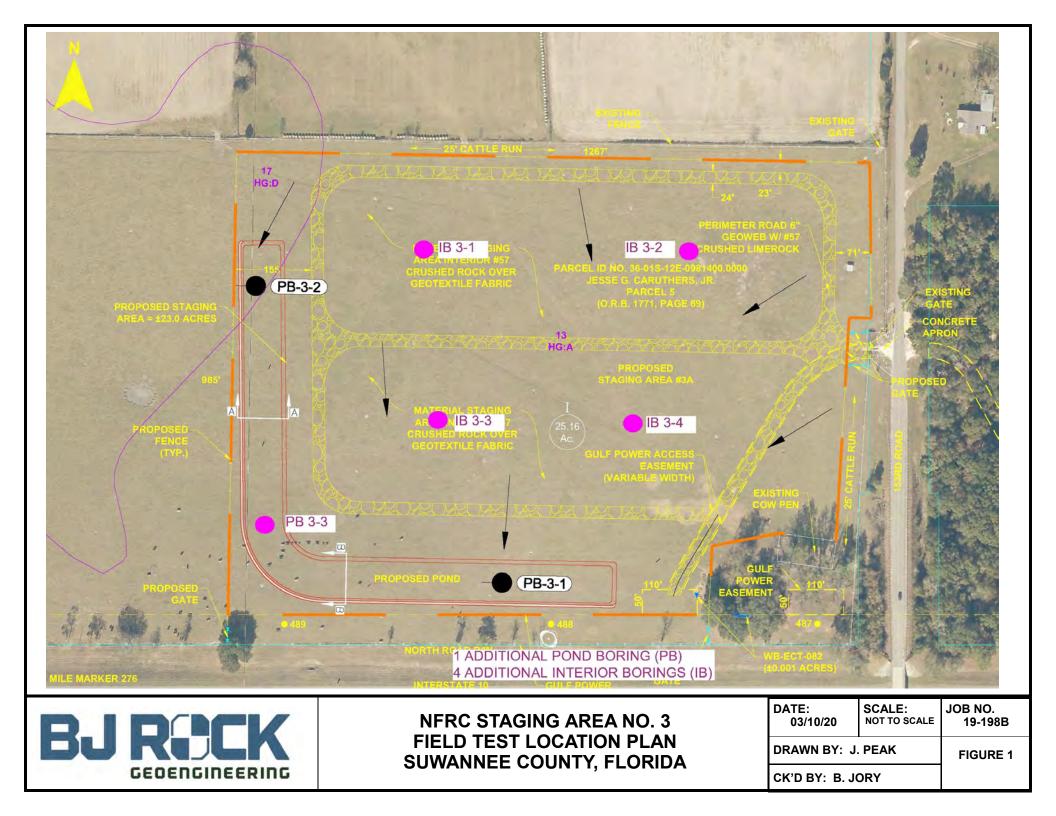


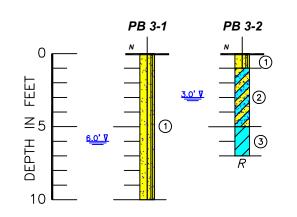
erosion and ground subsidence could affect new structures in the future. It is not possible to investigate or design to completely eliminate the possibility of future sinkhole-related problems. In any event, the Owner must understand and accept this risk.

The scope of our services does not include any environmental assessments or investigations for the possible presence of hazardous or toxic substances in the soil, groundwater, or surface water within or in the general vicinity of the site studied. Any statements made in this report or shown on the test boring log regarding unusual subsurface conditions and/or composition, odor, staining, origin, or other characteristics of the surface and/or subsurface materials are strictly for the information of our client and may or may not be indicative of an environmental problem.

If changes are made in the overall design or the location of the proposed structure(s), the recommendations presented in this report must not be considered valid unless the changes are reviewed by our firm and recommendations modified or verified in writing. We should be given the opportunity to review the foundation plan and the applicable portions of the project specifications when the design is finalized. This review will allow us to check whether these documents are consistent with the intent of our recommendations.

APPENDIX





#### LEGEND

- GRAY, TAN, BROWN FINE TO SLIGHTLY SILTY FINE SANDS (SP)/(SP-SM)
- (2) = ORANGE, TAN CLAYEY FINE SAND (SC)
- (3) = GRAY, BROWN, TAN SANDY CLAY (CL)
  - (SP) = UNIFIED SOIL CLASSIFICATION GROUP SYMBOL
    - N = STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT
  - 0.017 = ESTIMATED SEASONAL HIGH GROUNDWATER LEVEL

R = REFUSAL MATERIAL ENCOUNTERED

NOTES: HAND AUGER BORINGS PERFORMED NOVEMBER 14, 2019.

EXISTING GROUNDWATER LEVEL NOT ENCOUNTERED TO 7 TO 10 FEET.



NFRC STAGING AREA 3 SOIL BORING LOGS COLUMBIA COUNTY, FL

DATE:	SCALE:		JOB NO.
11/17/19	AS SHOWN		19-198A
DRAWN BY: E. COLO'N		FI	GURE 2
CK'D BY: J. PEAK			

## LEGEND

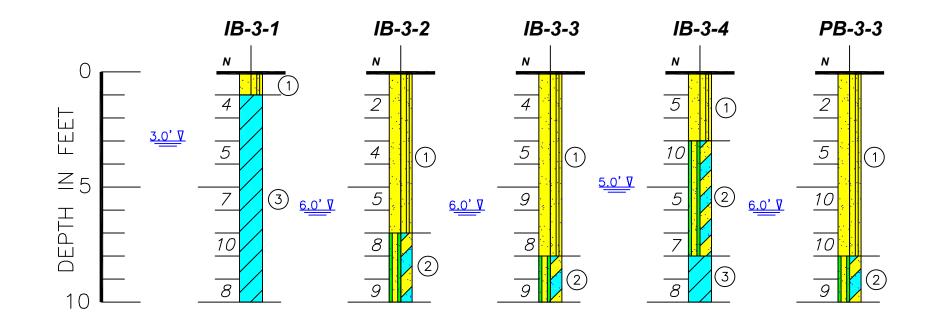
- () = GRAY, TAN, ORANGE, BROWN, DARK BROWN, DARK GRAY FINE TO SLIGHTLY SILTY FINE SANDS (SP)/(SP-SM)
- (2) = GRAY, TAN, BROWN, ORANGE SILTY TO CLAYEY FINE SANDS (SM)/(SC)
- (3) = BROWN, ORANGE/BROWN SANDY CLAY (CL)
  - (SP) = UNIFIED SOIL CLASSIFICATION GROUP SYMBOL
    - N = STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT CORRELATED FROM CPT READINGS
  - Q.Q. = EXISTING GROUNDWATER LEVEL (IF ENCOUNTERED)
  - 0.0'V = ESTIMATED SEASONAL HIGH GROUNDWATER LEVEL

NOTE: TESTING PERFORMED FEBRUARY 13, 2020.



NFRC STAGING AREA 3 SOIL BORING LOGS SUWANNEE COUNTY, FL

DATE:	SCALE:		JOB NO.
2-20-20	AS SF	IOWN	19-198B
DRAWN BY: E. COLO'N		FI	GURE 2
CK'D BY: J. PEAK		SHE	ET 1 OF 2



B.I.R. CK	NFRC STAGING AREA 3	date: <b>2-20-20</b>	<sup>SCALE:</sup> AS SHOWN	јов <i>по.</i> <b>19-198В</b>
GEDENGINEERING	SUWANNEE COUNTY, FL	DRAWN BY: E. C CK'D BY: J. PEA		GURE 2 EET 2 OF 2

March 13, 2020

#### Re: Stormwater Pond Recovery Analysis NFRC Staging Areas Staging Area No. 3 – Basin I Suwanee County, Florida

BJR Job No: 19-198(B)

As authorized, BJ Rock, LLC (BJR) has completed the stormwater pond recovery analysis for the above-referenced staging area. The project site is located on 153<sup>rd</sup> Road in Live Oak, Suwanee County, Florida.

We understand that two crushed rock material laydown areas will be constructed along with one dry stormwater management pond within the proposed project. The pond will be constructed within the southwest corner of the project. The Staging Area consists of one drainage basin (I).

We used soil and groundwater information collected during the geotechnical exploration on the site and provided in the BJR Geotechnical data provided. In addition, we used site survey data, crushed rock laydown area design, and stormwater pond design information provided by Pickett Surveying and Engineering. We utilized the commercially available software PONDS (version 3.3) to perform the stormwater pond recovery analysis. Copies of the PONDS software outputs are included in the Attachments.

The PONDS software is generally limited to analyzing flat bottom stormwater ponds. Since the rock laydown areas are planned to be constructed at existing grade and will be sloping, it was necessary to analyze each area as flat basins using average soil and groundwater parameters. We understand that you plan to utilize CR-PE Multi-Purpose Root & Water Barrier Molded Rolls by Century Products (or similar) to retain water within the laydown areas for recharge before discharging excess water to the ponds. Based on this plan, it is our opinion that using average soil and groundwater parameters for this analysis is appropriate. Please note that the treatment volume was recovered within the rock laydown basin area within 72 hours. Therefore, discharge and recovery within the stormwater pond was not needed.

Below are Average Soil and Groundwater Calculations and Model Input Parameters for each basin. We assumed a Base of Aquifer depth below the Seasonal High Water Table (SHWT) of 2 feet or less. This depth is generally conservative based on our experience with similar projects in soils with relatively high silt/clay content. The actual Base of Aquifer is likely deeper.

Lastly, we assumed a porosity of 35% for the crushed rock for void space storage.

#### Stormwater Recovery Analysis – Staging Area No. 3 – Basin I

#### Average Soil and Groundwater Calculations

Below are the average soil and groundwater calculations for the stormwater pond recovery analysis.

Staging Area No. 3			
	Basin I		
	Rock Laydown Eleva	tion	
Low El. (ft)	High El. (ft)	Average El. (ft.)	
90	90	90	
	Horizontal Saturated Hydraulic		
Boring	Conductivity (ft/day)*	Depth to SHWT (ft)	
PB-3-1	2.6	6	
PB-3-2	0.2	3	
PB-3-3	1	6	
IB-3-1	0.08	3	
IB-3-2	2	6	
IB-3-3	2	6	
IB-3-4	1	5	
AVG.	1.27	5	
Average SHWT Elev. (ft) 85			
* Hydraulic conductivity values include a factor of safety of 2 based on the field			
test results.	test results.		

#### Model Input Parameters

Below are the input parameters used for the stormwater pond recovery analysis.

#### Aquifer and Geometry Data

Input Parameter	STAGING AREA NO.3 - BASIN I
Base of Aquifer Elevation (feet)	84
Water Table Elevation (feet)	85
Horizontal Saturated Hydraulic Conductivity (ft/day)*	1.27
Fillable Porosity (%)	25
Unsaturated Vertical Infiltration Rate (ft/day)*,**	0.635
Maximum Area for Unsaturated Infiltration (ft <sup>2</sup> )	201821.2
Equivalent Pond Length (ft)	1000
Equivalent Pond Width (ft)	576
* Hydraulic conductivity values include a factor of safety of 2 based on the	he field test results.
** Unsaturated vertical Infiltration rate is 1/2 the field tested Horizontal Saturated Hydraulic Conductivity rate.	

#### Stage vs Area Data for STAGING AREA 3 – BASIN I

Stage (ft)	Area (ft <sup>2</sup> )
90	201821.2
90.5	201821.2

Stormwater Input Data

Stormwater Pond Recovery Analysis NFRC – Staging Area No. 3 March 13, 2020 Page 3 of 3

STAGING AREA NO. 3	Hydrograph Type	slug load
BASIN I	Treatment Volume (ft <sup>3</sup> )	50965.2

#### **Results**

Based on the results of this analysis, the proposed crushed rock laydown area recovers the associated treatment volume within 72 hours.

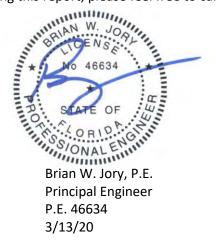
#### **Closing**

We appreciate the opportunity to be of service to you on this project and look forward to a continued relationship. Should you have any questions or concerns regarding this report, please feel free to call us at (407) 342-1443.

Sincerely, **Native Geoscience, Inc.** Certificate of Authorization No. 30474

1

John C. Diehl, P.G. Principal Geologist P.G. 2460



#### Attachments:

• PONDS Output – Staging Area No. 3 – Basin I – Rock Voids (7 pages)

#### Project Data

Project Name:	NFRC Staging Areas
Simulation Description:	Staging Area No. 3 - Basin I - Rock Voids
Project Number:	BJR19-198A
Engineer :	CW
Supervising Engineer:	JCD
Date:	03-11-2020

#### Aquifer Data

Base Of Aquifer Elevation, [B] (ft datum):	84.00
Water Table Elevation, [WT] (ft datum):	85.00
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day):	1.27
Fillable Porosity, [n] (%):	25.00
Unsaturated Vertical Infiltration Rate, [lv] (ft/day):	0.635
Maximum Area For Unsaturated Infiltration, [Av] (ft <sup>2</sup> ):	201821.2

#### **Geometry Data**

Equivalent Pond Length, [L] (ft):	1000.0
Equivalent Pond Width, [W] (ft):	576.0

Ground water mound is expected to intersect the pond bottom

#### Stage vs Area Data

Stage	Area
(ft datum)	(ft²)
90.00	201821.2
90.50	201821.2

#### Ditch Data

Ditch (or interceptor trench) parallel to length axis is inactive

Ditch (or interceptor trench) parallel to width axis is inactive

#### **Discharge Structures**

**Discharge Structure #1 is inactive** 

**Discharge Structure #2 is inactive** 

#### Discharge Structures (cont'd.)

**Discharge Structure #3 is inactive** 

#### Scenario Input Data

Scenario 1 :: 50965.2 ft<sup>3</sup> slug load

Hydrograph Type:	Slug Load
Modflow Routing:	Routed with infiltration

Treatment Volume (ft<sup>3</sup>) 50965.2

Initial ground water level (ft datum) 85.00 (default)

Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)	Time After Storm Event (days)
3.500	11.000	19.000	27.000
4.000	12.000	20.000	28.000
5.000	13.000	21.000	29.000
6.000	14.000	22.000	30.000
7.000	15.000	23.000	
8.000	16.000	24.000	
9.000	17.000	25.000	
10.000	18.000	26.000	
	Storm Event (days) 3.500 4.000 5.000 6.000 7.000 8.000 9.000	Storm Event (days)         Storm Event (days)           3.500         11.000           4.000         12.000           5.000         13.000           6.000         14.000           7.000         15.000           8.000         16.000           9.000         17.000	Storm Event (days)         Storm Event (days)         Storm Event (days)         Storm Event (days)           3.500         11.000         19.000           4.000         12.000         20.000           5.000         13.000         21.000           6.000         14.000         22.000           7.000         15.000         23.000           8.000         16.000         24.000           9.000         17.000         25.000

#### PONDS Version 3.3.0278 Retention Pond Recovery - Refined Method Copyright 2012 Devo Seereeram, Ph.D., P.E.

Detailed Results :: Scenario 1 :: 50965.2 ft<sup>3</sup> slug load

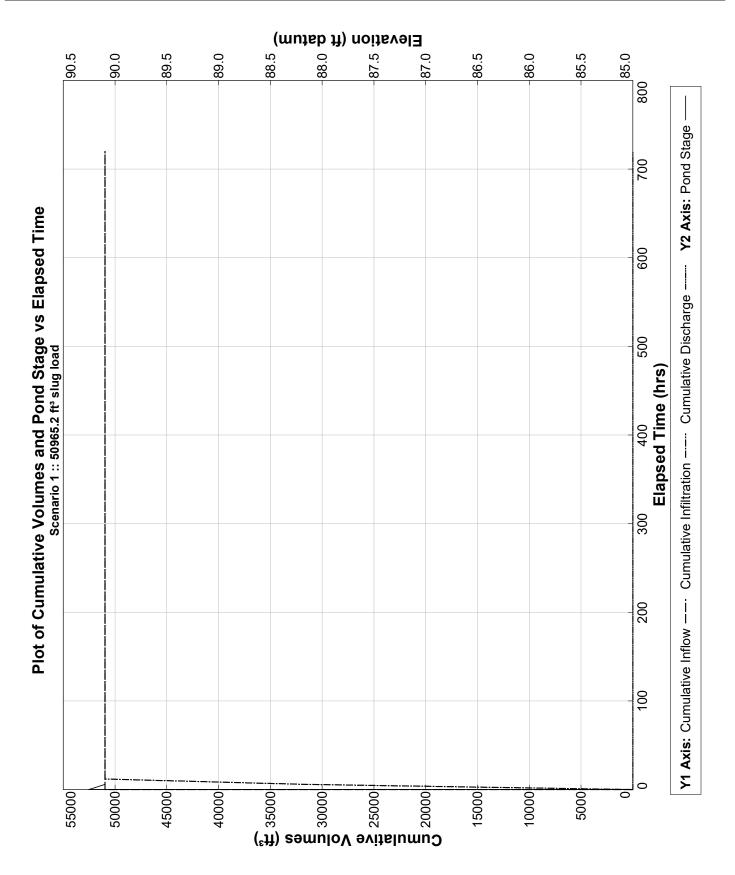
Elapsed Time (hours)	Instantaneous Inflow Rate (ft³/s)	Outside Recharge (ff/day)	Stage Elevation (ft datum)	Infiltration Rate (ft³/s)	Combined Instantaneous Discharge Rate (ft³/s)	Cumulative Inflow Volume (ft³)	Cumulative Infiltration Volume (ft <sup>3</sup> )	Combined Cumulative Discharge (ft <sup>3</sup> )	Flow Type
0.000	8494,2000	0.00000	85.00000	0.00000	0	0.000	0.0	0	N.A.
0.002	8494.2000	0.00000	90.25248	1.48329	0	50965,200	8.9	0	U/P
2.400	0.0000	0.00000	90,18903	1.48329	0	50965.200	12815.7	0	U/P
6.000	0.0000	0.00000	90.09377	0.92706	0	50965.200	32039.1	0	U/P
12.000	0.0000	0.00000				50965.200	50965.2	0	dry
24.000	0.0000	0.00000				50965,200	50965.2	0	dry
36.000	0.0000	0.00000				50965,200	50965.2	0	dry
48.000	0.0000	0.00000				50965.200	50965.2	0	dry
60.000	0.0000	0.00000				50965.200	50965.2	0	dry
72.000	0.0000	0.00000				50965.200	50965.2	0	dry
84.000	0.0000	0.00000				50965.200	50965.2	0	dry
96.000	0.0000	0.00000				50965.200	50965.2	0	dry
120.000	0.0000	0.00000				50965.200	50965.2	0	dry
144.000	0.0000	0.00000				50965.200	50965.2	0	dry
168.000	0.0000	0.00000				50965.200	50965.2	0	dry
192.000	0.0000	0.00000				50965.200	50965.2	0	dry
216.000	0.0000	0.00000				50965.200	50965.2	0	dry
240.000	0.0000	0.00000				50965.200	50965.2	0	dry
264.000	0.0000	0.00000				50965.200	50965.2	0	dry
288.000	0.0000	0.00000				50965.200	50965.2	0	dry
312.000	0.0000	0.00000				50965.200	50965.2	0	dry
336.000	0.0000	0.00000				50965.200	50965.2	0	dry
360.000	0.0000	0.00000				50965.200	50965.2	0	dry
384.000	0.0000	0.00000				50965.200	50965.2	0	dry
408.000	0.0000	0.00000				50965.200	50965.2	0	dry
432.000	0.0000	0.00000				50965.200	50965.2	0	dry
456.000	0.0000	0.00000				50965.200	50965.2	0	dry
480.000	0.0000	0.00000				50965.200	50965.2	0	dry
504.000	0.0000	0.00000				50965.200	50965.2	0	dry
528.000	0.0000	0.00000				50965.200	50965.2	0	dry
552.000	0.0000	0.00000				50965.200	50965.2	0	dry
576.000	0.0000	0.00000				50965.200	50965.2	0	dry
600.000	0.0000	0.00000				50965.200	50965.2	0	dry
624.000	0.0000	0.00000				50965.200	50965.2	0	dry
648.000	0.0000	0.00000				50965.200	50965.2	0	dry
672.000	0.0000	0.00000				50965.200	50965.2	0	dry
696.000	0.0000	0.00000				50965.200	50965.2	0	dry
720.000	0.0000	0.00000				50965.200	50965.2	0	dry

#### PONDS Version 3.3.0278 Retention Pond Recovery - Refined Method Copyright 2012 Devo Seereeram, Ph.D., P.E.

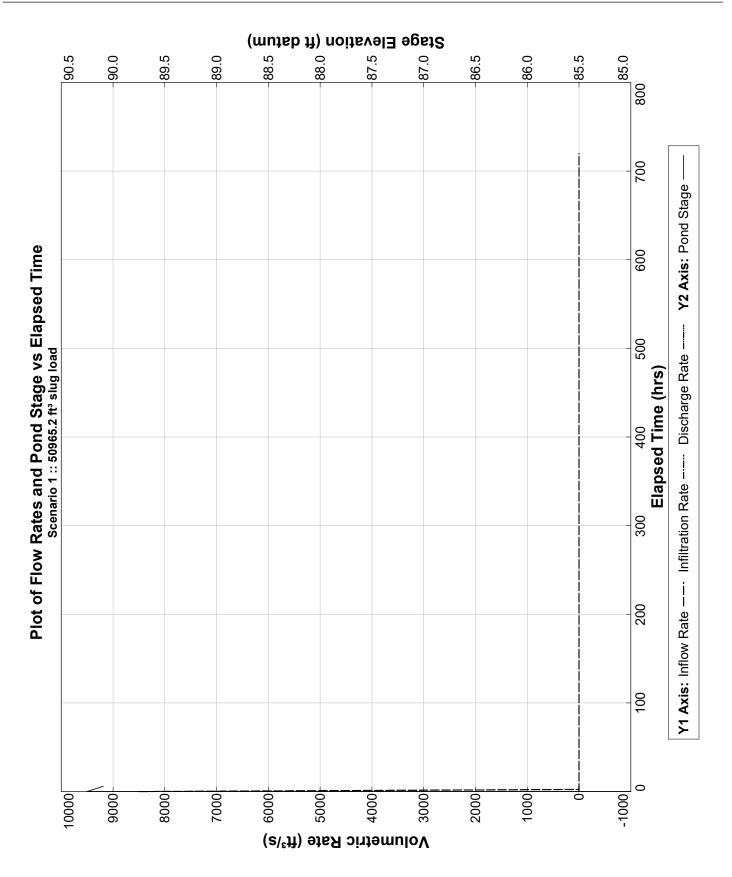
#### Summary of Results :: Scenario 1 :: 50965.2 ft<sup>3</sup> slug load

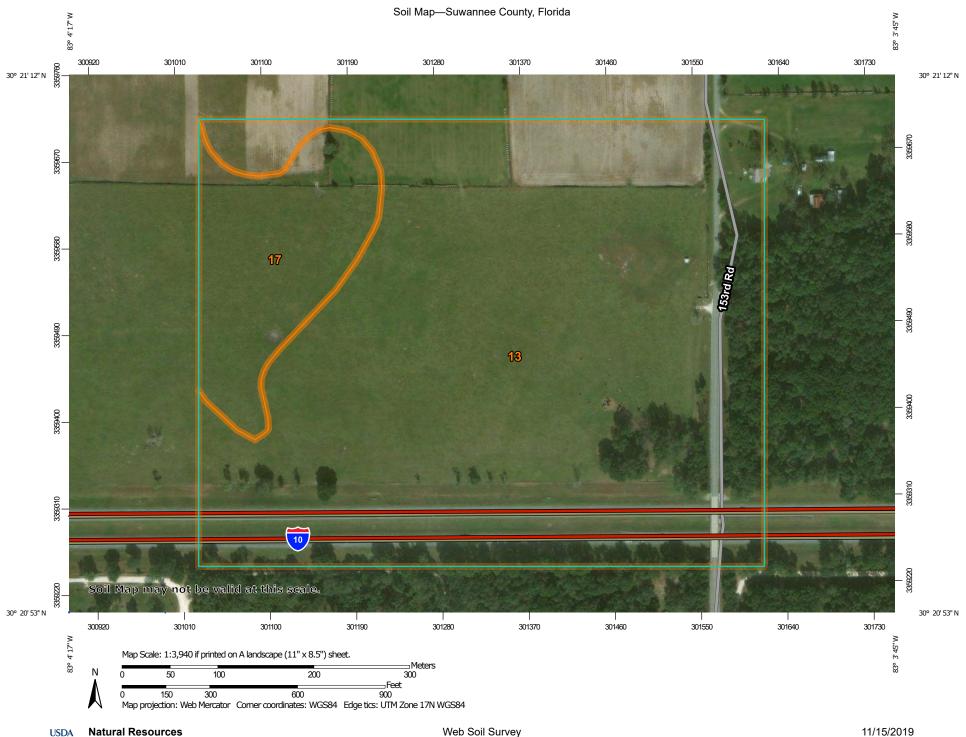
	Time (hours)	Stage (ft datum)	Rate (ft³/s)	Volume (ft³)
Stage				
Minimum	0.000	85.00		
Maximum	0.002	90.25		
Inflow				
Rate - Maximum - Positive	0.002		8494.2000	
Rate - Maximum - Negative	None		None	
Cumulative Volume - Maximum Positive	0.002			50965.2
Cumulative Volume - Maximum Negative	None			None
Cumulative Volume - End of Simulation	720.000			50965.2
Infiltration				
Rate - Maximum - Positive	0.002		1.4833	
Rate - Maximum - Negative	None		None	
Cumulative Volume - Maximum Positive	6.000		Hono	32039.1
Cumulative Volume - Maximum Negative	None			None
Cumulative Volume - End of Simulation	720.000			50965.2
	0.000			
Combined Discharge				
Rate - Maximum - Positive	None		None	
Rate - Maximum - Negative	None		None	
Cumulative Volume - Maximum Positive	None			None
Cumulative Volume - Maximum Negative	None			None
Cumulative Volume - End of Simulation	720.000			0.0
Discharge Structure 1 - inactive				
Rate - Maximum - Positive	disabled		disabled	
Rate - Maximum - Negative	disabled		disabled	
Cumulative Volume - Maximum Positive	disabled		disabled	disabled
Cumulative Volume - Maximum Negative	disabled			disabled
Cumulative Volume - End of Simulation	disabled			disabled
Discharge Structure 2 - inactive				
Rate - Maximum - Positive	disabled		disabled	
Rate - Maximum - Negative	disabled		disabled	
Cumulative Volume - Maximum Positive	disabled			disabled
Cumulative Volume - Maximum Negative	disabled			disabled
Cumulative Volume - End of Simulation	disabled			disabled
Discharge Structure 3 - inactive				
Rate - Maximum - Positive	disabled		disabled	
Rate - Maximum - Negative	disabled		disabled	
Cumulative Volume - Maximum Positive	disabled		usabieu	disabled
Cumulative Volume - Maximum Volume	disabled			disabled
Cumulative Volume - End of Simulation	disabled			disabled
Pollution Abatement:	00.000	5		50005 C
36 Hour Stage and Infiltration Volume	36.000	Dry		50965.2
72 Hour Stage and Infiltration Volume	72.000	Dry		50965.2

#### PONDS Version 3.3.0278 Retention Pond Recovery - Refined Method Copyright 2012 Devo Seereeram, Ph.D., P.E.



#### PONDS Version 3.3.0278 Retention Pond Recovery - Refined Method Copyright 2012 Devo Seereeram, Ph.D., P.E.





Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey 11/15/2019 Page 1 of 3

Area of Interest (AOI		D	MAP INFORMATION
Area of Interest (AOI) 🗃 Spoil Area			The soil surveys that comprise your AOI were mapped at
Area of I	nterest (AOI)		1:24,000.
Soils			Warning: Soil Map may not be valid at this scale.
Soil Map	Unit Polygons		Enlargement of maps beyond the scale of mapping can cause
🛹 🛛 Soil Map	Unit Lines		misunderstanding of the detail of mapping and accuracy of soil
Soil Map	Unit Points		line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed
Special Point Feat		Special Line Features	scale.
Blowout	Water F	eatures	Please rely on the bar scale on each map sheet for map
🔀 🛛 Borrow P		Streams and Canals	measurements.
💥 🛛 Clay Spo		ortation Rails	Source of Map: Natural Resources Conservation Service
Closed D	epression	Interstate Highways	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)
💥 🛛 Gravel Pi	t 🖌	US Routes	Maps from the Web Soil Survey are based on the Web Mercato
Gravelly		Major Roads	projection, which preserves direction and shape but distorts
🙆 Landfill	~	Local Roads	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more
Lava Flov			accurate calculations of distance or area are required.
Marsh or		Aerial Photography	This product is generated from the USDA-NRCS certified data a of the version date(s) listed below.
🙊 Mine or C	Quarry		Soil Survey Area: Suwannee County, Florida
Miscellar	eous Water		Survey Area Data: Version 18, Sep 17, 2019
Perennia	Water		Soil map units are labeled (as space allows) for map scales
🤝 🛛 Rock Out	crop		1:50,000 or larger.
+ Saline Sp	pot		Date(s) aerial images were photographed: Jun 5, 2006—Feb 2017
Sandy Sp	pot		The orthophoto or other base map on which the soil lines were
Severely	Eroded Spot		compiled and digitized probably differs from the background
Sinkhole			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.
b Slide or S	Slip		5 - · · · · · · · · · · · · · · · · · ·
🧭 Sodic Sp	ot		



# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
13	Blanton-Alpin-Bonneau complex, 0 to 5 percent slopes	58.7	86.2%
17	Falmouth-Bonneau-Blanton complex, 0 to 5 percent slopes	9.4	13.8%
Totals for Area of Interest	1	68.0	100.0%



# Suwannee County, Florida

### 13—Blanton-Alpin-Bonneau complex, 0 to 5 percent slopes

#### Map Unit Setting

National map unit symbol: 2w4gj Elevation: 50 to 350 feet Mean annual precipitation: 49 to 57 inches Mean annual air temperature: 66 to 73 degrees F Frost-free period: 239 to 269 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Blanton and similar soils: 42 percent
Alpin and similar soils: 33 percent
Bonneau and similar soils: 16 percent
Minor components: 9 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Blanton**

#### Setting

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Summit Landform position (three-dimensional): Side slope, interfluve Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 5 inches: fine sand E - 5 to 41 inches: fine sand Bt - 41 to 48 inches: sandy loam Btg - 48 to 80 inches: sandy clay loam

#### Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 42 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 4.5 inches)

USDA

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Forage suitability group: Sandy soils on rises, knolls, and ridges of mesic uplands (G138XA121FL) Hydric soil rating: No

#### **Description of Alpin**

#### Setting

Landform: Knolls on marine terraces, ridges on marine terraces, flats on marine terraces
 Landform position (two-dimensional): Summit
 Landform position (three-dimensional): Interfluve, talf
 Down-slope shape: Convex
 Across-slope shape: Linear
 Parent material: Eolian deposits or sandy marine deposits

#### **Typical profile**

A - 0 to 6 inches: fine sand E - 6 to 65 inches: fine sand E and Bt - 65 to 80 inches: fine sand

#### Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 20.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 3.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4s Hydrologic Soil Group: A Forage suitability group: Sandy soils on ridges and dunes of xeric uplands (G138XA111FL)

Hydric soil rating: No

#### **Description of Bonneau**

#### Setting

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

JSDA

*Down-slope shape:* Convex *Across-slope shape:* Convex *Parent material:* Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 7 inches: fine sand E - 7 to 27 inches: fine sand Bt - 27 to 58 inches: fine sandy loam Btg - 58 to 80 inches: sandy clay loam

#### Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: About 42 to 60 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Forage suitability group: Sandy over loamy soils on rises, knolls, and ridges of mesic uplands (G138XA221FL) Hydric soil rating: No

#### **Minor Components**

#### Albany

Percent of map unit: 5 percent Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Chipley

Percent of map unit: 4 percent
Landform: Knolls on marine terraces, rises on marine terraces, flats on marine terraces
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Interfluve, talf
Down-slope shape: Convex
Across-slope shape: Linear

USDA

Hydric soil rating: No

# **Data Source Information**

Soil Survey Area: Suwannee County, Florida Survey Area Data: Version 18, Sep 17, 2019



# Suwannee County, Florida

# 17—Falmouth-Bonneau-Blanton complex, 0 to 5 percent slopes

#### Map Unit Setting

National map unit symbol: 13bvp Elevation: 20 to 350 feet Mean annual precipitation: 49 to 57 inches Mean annual air temperature: 66 to 73 degrees F Frost-free period: 239 to 269 days Farmland classification: Not prime farmland

#### Map Unit Composition

Falmouth and similar soils: 36 percent
Bonneau and similar soils: 30 percent
Blanton and similar soils: 22 percent
Minor components: 12 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Falmouth**

#### Setting

Landform: Ridges on marine terraces, hills on marine terraces Landform position (three-dimensional): Interfluve Down-slope shape: Linear Across-slope shape: Linear Parent material: Clayey marine deposits

#### **Typical profile**

Ap - 0 to 3 inches: fine sand E - 3 to 10 inches: fine sand Bt - 10 to 17 inches: sandy clay loam B/Cg - 17 to 80 inches: sandy clay

#### **Properties and qualities**

Slope: 2 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 18 to 36 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 8.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: D Forage suitability group: Loamy and clayey soils on flats and rises of mesic lowlands (G138XA331FL) Hydric soil rating: No

#### **Description of Bonneau**

#### Setting

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Parent material: Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 7 inches: fine sand E - 7 to 27 inches: fine sand Bt - 27 to 36 inches: fine sandy loam Btg - 36 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: About 42 to 60 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Forage suitability group: Sandy over loamy soils on rises, knolls, and ridges of mesic uplands (G138XA221FL) Hydric soil rating: No

#### **Description of Blanton**

#### Setting

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (three-dimensional): Interfluve, side slope Down-slope shape: Convex Across-slope shape: Linear

JSDA

#### Parent material: Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 5 inches: fine sand E - 5 to 41 inches: fine sand Bt - 41 to 48 inches: sandy loam Btg - 48 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 42 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 4.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Forage suitability group: Sandy soils on rises, knolls, and ridges of mesic uplands (G138XA121FL) Hydric soil rating: No

#### **Minor Components**

#### Alpin

Percent of map unit: 7 percent Landform: Knolls on marine terraces, ridges on marine terraces, flats on marine terraces Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Albany

Percent of map unit: 5 percent Landform: Knolls on marine terraces, ridges on marine terraces Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear

USDA

Hydric soil rating: No

# **Data Source Information**

Soil Survey Area: Suwannee County, Florida Survey Area Data: Version 18, Sep 17, 2019



#### FIELD TESTING STANDARDS AND PROCEDURES

#### Standard Penetration Test (SPT) Boring

The SPT borings were advanced by means of a truck or track mounted drill rig employing wet rotary drilling techniques. The SPT testing was performed continuously in the upper ten feet and at five-foot intervals thereafter. The soil samples were obtained at the depths where the SPT testing was performed. The soil samples were then classified in the field, placed in sealed containers, and returned to our laboratory for further evaluation by a geotechnical engineer.

The SPT borings were performed in general compliance with standard field penetration test procedures (ASTM D 1586-99). After drilling to the sampling depth and flushing the borehole, the standard two-inch O.D. split-barrel sampler was seated by driving it six inches into the undisturbed soil at the bottom of the borehole. The sampler was then driven an additional 12 inches by a 140-pound hammer falling 30 inches. The number of blows required to produce the 12 inches of penetration is recorded as the standard penetration test value (N). These values are plotted on the left side of the boring log Figure 3.

In the upper ten feet sampling was performed by driving the split-barrel sampler 24 inches and the blows required to drive the sampler the middle two 6-inch increments were recorded as the "N" value. Through this technique, the upper ten feet of the soil was sampled continuously. Detailed descriptions of the soils encountered during the advancement of the SPT boring are presented in the Boring Logs.

#### Soil Sample Handling and Classification

The soil samples obtained from the SPT borings were placed in sealed containers to retain moisture and returned to our laboratory. The samples were then reviewed by a geotechnical engineer to confirm classifications, visually estimate the relative percentages of the soil's constituents (sand, clay, etc.), and identify pertinent structural features. We visually classified the soils according to the Unified Soil Classification System (ASTM D 2487). The stratification lines shown on the boring logs in Figure 3 represent our interpretation of approximate boundaries between soil types. The transition between strata may be gradual. Our classifications are based on a visual estimation of the soil properties and our engineering experience with the soils found in this geologic area.

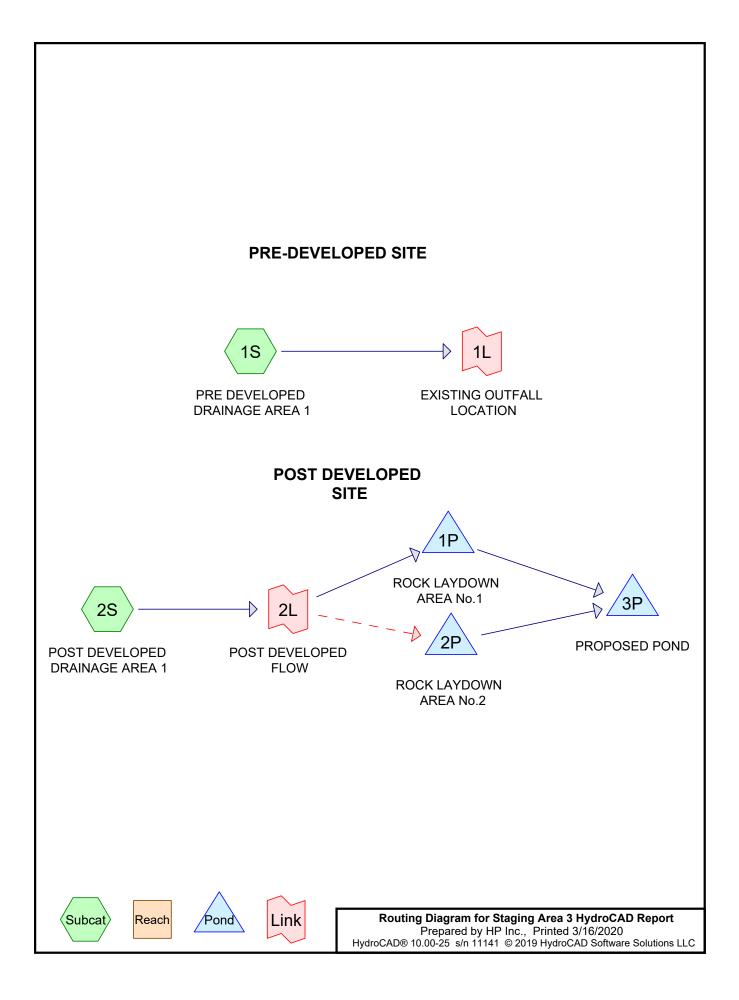
The SPT "N" values are presented adjacent along the left side of the boring logs. The correlation of the SPT "N" values with relative density, unconfined compressive strength, and consistency are provided in the following table:

Coarse-Gra	ined Soils	Fine Grained Soils			
Penetration Resistance N (blows/ft)	Relative Density of Sand	Penetration Resistance N (blows/ft)	Unconfined Compressive Strength of Clay (tons/ft <sup>2</sup> )	Consistency of Clay	
0-4	Very Loose	<2	<0.25	Very Soft	
4-10	Loose	2-4	0.25-0.50	Soft	
10-30	Medium-Dense	4-8	0.50-1.00	Medium	
30-50	Dense	8-15	1.00-2.00	Stiff	
>50	Very Dense	15-30	2.00-4.00	Very Stiff	
		>30	>4.00	Hard	

#### Hand Auger Borings

The auger borings were performed with a manually advanced hand auger. The auger was advanced by rotating it into the ground in approximate 6-inch increments. After each incremental penetration, the auger was retracted, and the soils collected in the auger bucket were placed in sealed containers. The samples were then reviewed by a geotechnical engineer and classified as described above. Detailed descriptions of the soils encountered in the auger borings are presented in the Auger Boring Logs.

Appendix B – HydroCAD Report



Staging Area 3 HydroCAD Report Type II 24-hr 3 DAY-100YR. Rainfall=12.40" Prepared by HP Inc. Printed 3/16/2020 HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC Page 3 Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method Subcatchment1S: PRE DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>5.06" Flow Length=1,711' Slope=0.0016 '/' Tc=222.3 min CN=58 Runoff=23.38 cfs 10.620 af Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>6.15" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=30.19 cfs 12.892 af Peak Elev=90.37' Storage=21,675 cf Inflow=13.28 cfs 5.672 af Pond 1P: ROCK LAYDOWN AREANo.1 Discarded=1.00 cfs 0.768 af Primary=15.29 cfs 4.417 af Outflow=16.29 cfs 5.185 af Pond 2P: ROCK LAYDOWN AREANo.2 Peak Elev=90.46' Storage=13,418 cf Inflow=16.91 cfs 7.220 af Discarded=0.62 cfs 0.514 af Primary=20.38 cfs 6.376 af Outflow=21.00 cfs 6.891 af Pond 3P: PROPOSED POND Peak Elev=88.72' Storage=260,592 cf Inflow=29.63 cfs 10.793 af Discarded=1.75 cfs 1.035 af Primary=16.42 cfs 4.287 af Outflow=18.18 cfs 5.322 af Link 1L: EXISTING OUTFALL LOCATION Inflow=23.38 cfs 10.620 af Primary=23.38 cfs 10.620 af Link 2L: POST DEVELOPED FLOW

x 0.44 Inflow=30.19 cfs 12.892 af Primary=13.28 cfs 5.672 af Secondary=16.91 cfs 7.220 af

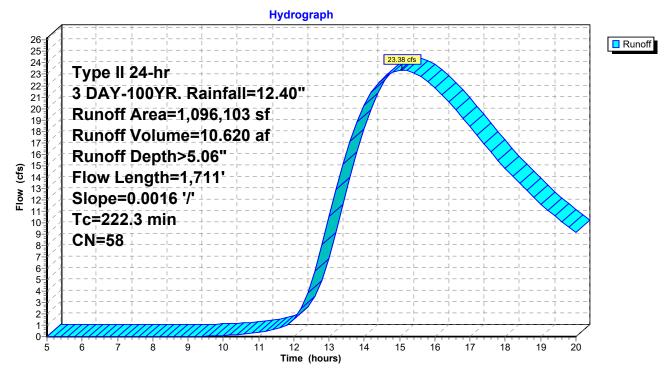
### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 23.38 cfs @ 15.06 hrs, Volume= 10.620 af, Depth> 5.06"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 3 DAY-100YR. Rainfall=12.40"

Are	ea (sf)	CN D	escription		
1,09	6,103	58 N	3 Meadow, non-grazed, HSG B		
1,09	6,103	1	00.00% Pe	ervious Are	ea
Tc I (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
222.3	1,711	0.0016	0.13		Lag/CN Method,

### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



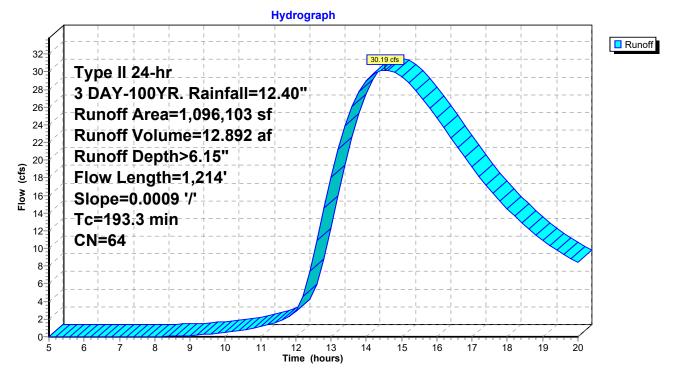
### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff 30.19 cfs @ 14.52 hrs, Volume= = 12.892 af, Depth> 6.15"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 3 DAY-100YR. Rainfall=12.40"

_	A	rea (sf)	CN E	Description		
k	5	76,632	65 L	Incompact	ed Gravel(	( 35% Void Ratio)
	4	21,336	58 N	Meadow, non-grazed, HSG B		
_		98,135	85 C	Gravel roads, HSG B		
	1,0	96,103	64 V	Weighted Average		
	1,0	96,103	1	100.00% Pervious Area		ea
	Та	l a sa aith	Clana	Valasity	Conseitu	Description
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	193.3	1,214	0.0009	0.10		Lag/CN Method,

### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

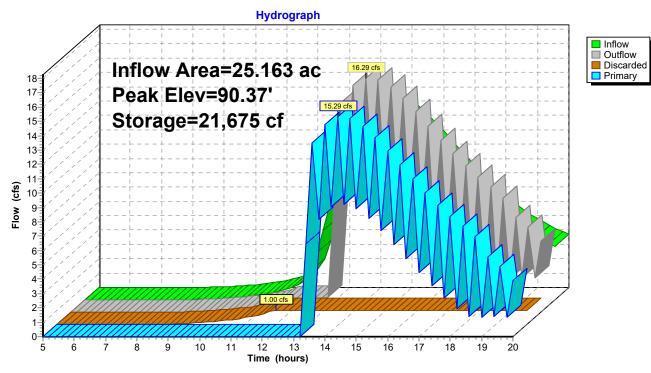


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# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	13.28 cfs @ 16.29 cfs @ 1.00 cfs @	0.00% Impervious, Inflow Depth > 2.71" for 3 DAY-100YR. event         14.52 hrs, Volume=       5.672 af         14.40 hrs, Volume=       5.185 af, Atten= 0%, Lag= 0.0 min         12.00 hrs, Volume=       0.768 af         14.40 hrs, Volume=       4.417 af			
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.37' @ 14.40 hrs Surf.Area= 123,855 sf Storage= 21,675 cf					
Center-of-Mas	Plug-Flow detention time= 37.0 min calculated for 5.117 af (90% of inflow) Center-of-Mass det. time= 16.3 min ( 952.1 - 935.8 )				
Volume		torage Storage Description			
#1	#189.50'21,675 cfCustom Stage Data (Prismatic)Listed below (Recalc) 61,928 cf Overall x 35.0% Voids				
Elevation	Surf.Area	Inc.Store Cum.Store			
(feet)	(sq-ft)	(cubic-feet) (cubic-feet)			
89.50	123,855				
90.00	123,855	61,928 61,928			
00.00	120,000	01,020			
Device Rout	ing Inve	rt Outlet Devices			
#1 Prim	0				
#2 Disc	arded 89.5				
<b>Discarded OutFlow</b> Max=1.00 cfs @ 12.00 hrs HW=89.51' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 1.00 cfs)					

**Primary OutFlow** Max=15.24 cfs @ 14.40 hrs HW=90.37' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 15.24 cfs @ 2.03 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

Inflow =	16.91 cfs @	14.52 hrs, Volume=	7.220 af
Outflow =	21.00 cfs @	14.60 hrs, Volume=	6.891 af, Atten= 0%, Lag= 4.7 min
Discarded =	0.62 cfs @	11.20 hrs, Volume=	0.514 af
Primary =	20.38 cfs @	14.60 hrs, Volume=	6.376 af

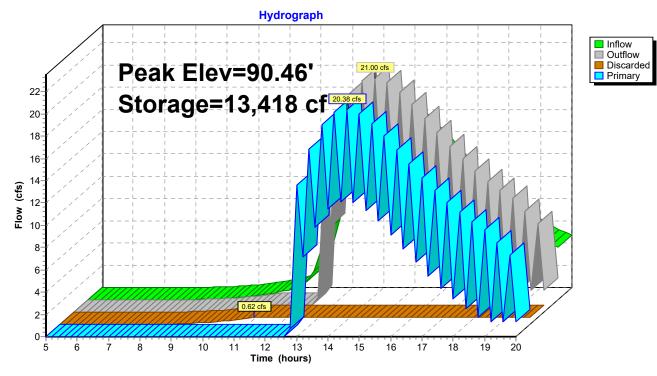
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.46' @ 14.60 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 19.4 min calculated for 6.891 af (95% of inflow) Center-of-Mass det. time= 7.8 min (943.6 - 935.8)

Volume	Invert	Avail.Stor	rage Storage	Description			
#1	89.50'	13,41		<b>Stage Data (Pr</b> of Overall x 35.0		below (Recalc)	
Elevatio (fee		.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
89.5	50 7	6,672	0	0			
90.0	00 7	6,672	38,336	38,336			
Device	Routing	Invert	Outlet Devices	S			
#1	Primary	89.90'	Head (feet) 0	0.5' breadth Bro .20 0.40 0.60 ( a) 2.80 2.92 3.0	0.80 1.00	Rectangular Weir	
#2	Discarded	89.50'				Phase-In= 0.01'	
Discarded OutFlow Max=0.62 cfs @ 11.20 hrs HW=89.51' (Free Discharge) ▲ 2=Exfiltration (Exfiltration Controls 0.62 cfs)							

Primary OutFlow Max=20.35 cfs @ 14.60 hrs HW=90.46' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 20.35 cfs @ 2.28 fps) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

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# Pond 2P: ROCK LAYDOWN AREA No.2

### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow	Depth > 5.15" for 3 DAY-100YR. event
Inflow =	29.63 cfs @	14.60 hrs, Volume=	10.793 af
Outflow =	18.18 cfs @	16.91 hrs, Volume=	5.322 af, Atten= 39%, Lag= 138.6 min
Discarded =	1.75 cfs @	16.91 hrs, Volume=	1.035 af
Primary =	16.42 cfs @	16.91 hrs, Volume=	4.287 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 88.72' @ 16.91 hrs Surf.Area= 216,318 sf Storage= 260,592 cf

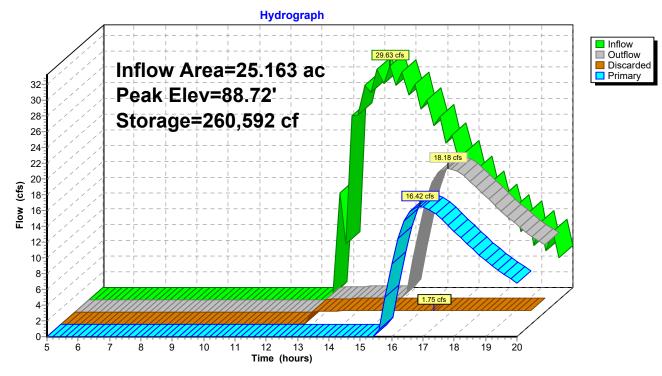
Plug-Flow detention time= 187.0 min calculated for 5.252 af (49% of inflow) Center-of-Mass det. time= 98.2 min (1,049.1 - 950.9)

Volume	Invert	Avail.Stor	rage Storage	e Description	
#1	87.50'	541,13	32 cf Custon	n Stage Data (Pr	ismatic)Listed below (Recalc)
Elevatio	et)	f.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
87.5 88.0		11,274 13,338	0 106,153	0 106,153	
89.0 90.0		17,483 21,654	215,411 219,569	321,564 541,132	
Device	Routing	Invert	Outlet Device		
#1	Discarded	87.50'	0.350 in/hr E	Exfiltration over	Surface area Phase-In= 0.01'
#2	Primary	88.50'	<b>43.6 deg x 5</b> Cv= 2.56 (C=		rise Sharp-Crested Vee/Trap Weir
Discourd	Disconded OutFlow May 1 75 of a 16 04 bra LIV/-00 701 (Free Discharge)				

**Discarded OutFlow** Max=1.75 cfs @ 16.91 hrs HW=88.72' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.75 cfs)

Primary OutFlow Max=16.37 cfs @ 16.91 hrs HW=88.72' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir (Weir Controls 16.37 cfs @ 1.50 fps) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

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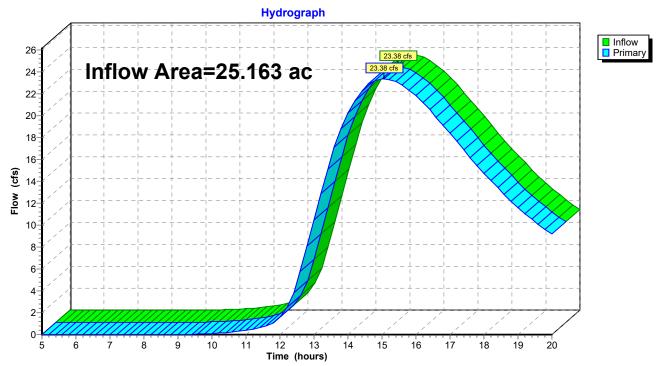


# Pond 3P: PROPOSED POND

# Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Are	a =	25.163 ac,	0.00% Impervious, Inflow Depth > 5.06" for 3 DAY	-100YR. event
Inflow	=	23.38 cfs @	15.06 hrs, Volume= 10.620 af	
Primary	=	23.38 cfs @	15.06 hrs, Volume= 10.620 af, Atten= 0%, La	g= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

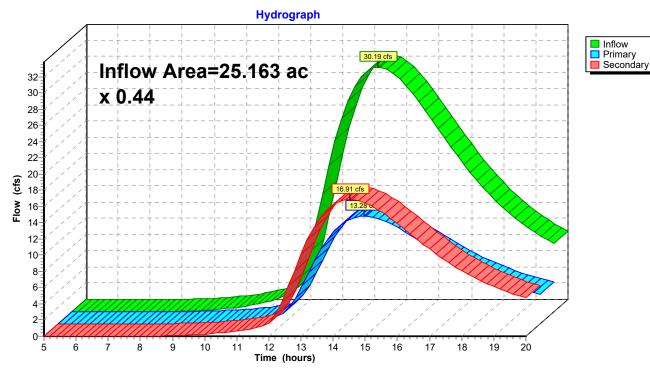


# Link 1L: EXISTING OUTFALL LOCATION

# Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow [	Depth > 6.15" for 3 DAY-100YR. event
Inflow =	30.19 cfs @	14.52 hrs, Volume=	12.892 af
Primary =	13.28 cfs @	14.52 hrs, Volume=	5.672 af, Atten= 56%, Lag= 0.0 min
Secondary =	16.91 cfs @	14.52 hrs, Volume=	7.220 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



# Link 2L: POST DEVELOPED FLOW

Printed 3/16/2020

Staging Area 3 HydroCAD ReportType II 24-hr 7 DAY-100YR Rainfall=14.00"Prepared by HP Inc.Printed 3/16/2020
HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC Page 14
Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method . Pond routing by Stor-Ind method
Subcatchment1S: PRE DEVELOPEDRunoff Area=1,096,103 sf0.00% ImperviousRunoff Depth>6.17"Flow Length=1,711'Slope=0.0016 '/'Tc=222.3 minCN=58Runoff=28.42 cfs12.932 af
Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>7.37" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=36.12 cfs 15.451 af
Pond 1P: ROCK LAYDOWN AREANO.1         Peak Elev=90.47'         Storage=21,675 cf         Inflow=15.89 cfs         6.798 af           Discarded=1.00 cfs         0.812 af         Primary=21.09 cfs         5.474 af         Outflow=22.09 cfs         6.286 af
Pond 2P: ROCK LAYDOWN AREANO.2         Peak Elev=90.48' Storage=13,418 cf         Inflow=20.23 cfs         8.652 af           Discarded=0.62 cfs         0.545 af         Primary=21.51 cfs         7.816 af         Outflow=22.13 cfs         8.360 af
Pond 3P: PROPOSED POND         Peak Elev=88.78' Storage=273,940 cf         Inflow=38.73 cfs         13.290 af           Discarded=1.75 cfs         1.059 af         Primary=23.83 cfs         6.658 af         Outflow=25.59 cfs         7.717 af
Link 1L: EXISTING OUTFALL LOCATIONInflow=28.42 cfs12.932 afPrimary=28.42 cfs12.932 af
Link 2L: POST DEVELOPED FLOW x 0.44 Inflow=36.12 cfs 15.451 af

x 0.44 Inflow=36.12 cfs 15.451 at Primary=15.89 cfs 6.798 af Secondary=20.23 cfs 8.652 af

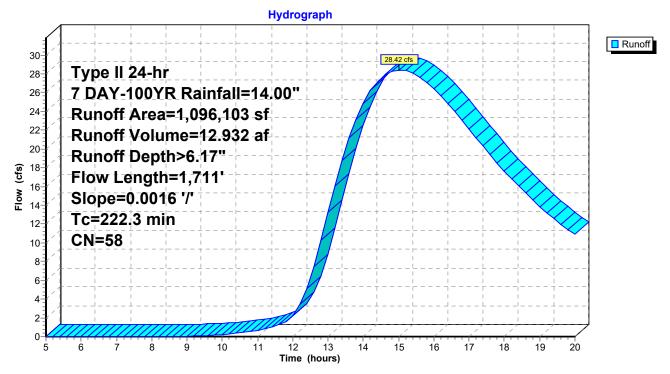
### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 28.42 cfs @ 15.02 hrs, Volume= 12.932 af, Depth> 6.17"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 7 DAY-100YR Rainfall=14.00"

	A	rea (sf)	CN I	Description				
	1,0	96,103	58 I	58 Meadow, non-grazed, HSG B				
	1,096,103 100.00% Pervious Area				28			
(I	Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
2	22.3	1,711	0.0016	0.13		Lag/CN Method,		

### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



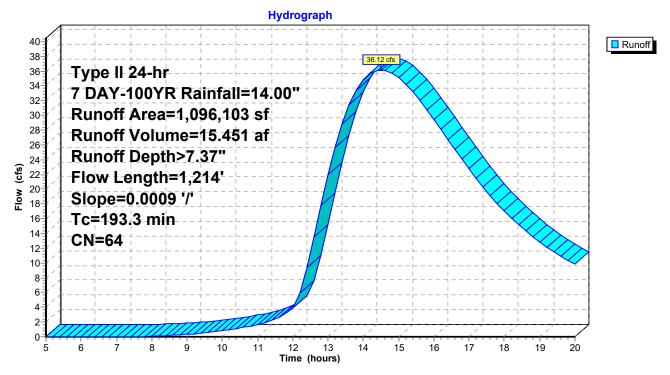
# Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff = 36.12 cfs @ 14.50 hrs, Volume= 15.451 af, Depth> 7.37"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 7 DAY-100YR Rainfall=14.00"

_	A	rea (sf)	CN E	Description				
*	5	76,632	65 L	Uncompacted Gravel( 35% Void Ratio)				
	4	21,336	58 N	Meadow, non-grazed, HSG B				
_		98,135	85 0	Gravel roads, HSG B				
	1,096,103 64 Weighted Average				verage			
	1,096,103 100.00% Pervious Area			00.00% Pe	ervious Are	ea		
	_		<u>.</u>		<b>•</b> •	<b>-</b>		
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	193.3	1,214	0.0009	0.10		Lag/CN Method,		

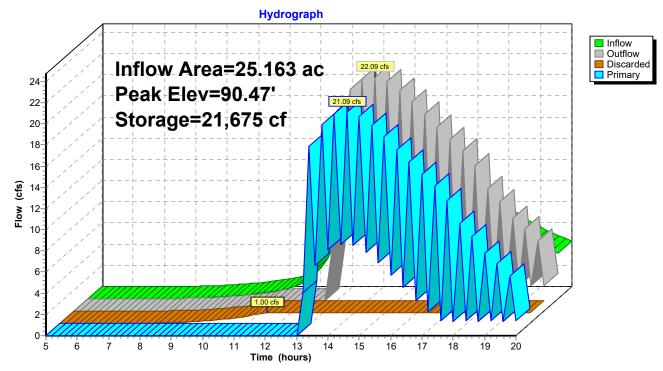
### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	15.89 cfs @ 1 22.09 cfs @ 1 1.00 cfs @ 1	0.00% Impervious, Inflow Depth > 3.24" for 7 DAY-100YR event         14.50 hrs, Volume=       6.798 af         14.60 hrs, Volume=       6.286 af, Atten= 0%, Lag= 6.2 min         11.60 hrs, Volume=       0.812 af         14.60 hrs, Volume=       5.474 af			
		e Span= 5.00-20.00 hrs, dt= 0.20 hrs Surf.Area= 123,855 sf   Storage= 21,675 cf			
Center-of-Mass of	let. time= 12.9 n	nin calculated for 6.286 af (92% of inflow) nin ( 945.6 - 932.8 ) orage Storage Description			
		675 cf Custom Stage Data (Prismatic)Listed below (Recalc)			
#1 09.	.50 21,0	61,928 cf Overall x 35.0% Voids			
Elevation	Surf.Area	Inc.Store Cum.Store			
(feet)	(sq-ft)	(cubic-feet) (cubic-feet)			
89.50	123,855	0 0			
90.00	123,855	61,928 61,928			
Device Routing	Invert	Outlet Devices			
#1 Primary	•	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00			
#2 Discard	ed 89.50'	Coef. (English) 2.80 2.92 3.08 3.30 3.32 0.350 in/hr Exfiltration over Surface area Phase-In= 0.01			
<b>Discarded OutFlow</b> Max=1.00 cfs @ 11.60 hrs HW=89.51' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 1.00 cfs)					

**Primary OutFlow** Max=21.04 cfs @ 14.60 hrs HW=90.47' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 21.04 cfs @ 2.31 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

Inflow =	20.23 cfs @	14.50 hrs, Volume=	8.652 af
Outflow =	22.13 cfs @	14.40 hrs, Volume=	8.360 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.62 cfs @	10.60 hrs, Volume=	0.545 af
Primary =	21.51 cfs @	14.40 hrs, Volume=	7.816 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.48' @ 14.40 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 16.9 min calculated for 8.360 af (97% of inflow) Center-of-Mass det. time= 8.0 min (940.8 - 932.8)

Volume	Invert	Avail.Stor	rage Storage	Description				
#1	89.50'	13,41		<b>Stage Data (Pr</b> of Overall x 35.0		below (Recalc)		
Elevatio (fee		.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
89.5	50 7	6,672	0	0				
90.0	00 7	6,672	38,336	38,336				
Device	Routing	Invert	Outlet Device	S				
#1	Primary	89.90'	Head (feet) 0	0.5' breadth Bro .20 0.40 0.60 ( a) 2.80 2.92 3.0	0.80 1.00	Rectangular Weir		
#2	Discarded	89.50'				Phase-In= 0.01'		
	<b>Discarded OutFlow</b> Max=0.62 cfs @ 10.60 hrs HW=89.51' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 0.62 cfs)							

Primary OutFlow Max=21.45 cfs @ 14.40 hrs HW=90.48' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 21.45 cfs @ 2.32 fps) 8-6 4-

2-0-

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Hydrograph Peak Elev=90.48' 24 Storage=13,418 cl 22 20-18-16 (cfs) 14 Flow 12-10

# Pond 2P: ROCK LAYDOWN AREA No.2

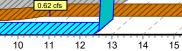
16

17

18

19

20



10 11 12 13 Time (hours)  Inflow
 Outflow Discarded Primary

### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow I	Depth > 6.34" for 7 DAY-100YR event
Inflow =	38.73 cfs @	14.60 hrs, Volume=	13.290 af
Outflow =	25.59 cfs @	16.35 hrs, Volume=	7.717 af, Atten= 34%, Lag= 104.8 min
Discarded =	1.75 cfs @	16.35 hrs, Volume=	1.059 af
Primary =	23.83 cfs @	16.35 hrs, Volume=	6.658 af

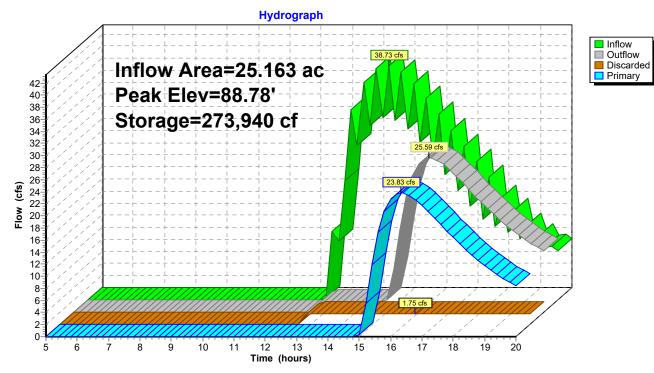
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 88.78' @ 16.35 hrs Surf.Area= 216,573 sf Storage= 273,940 cf

Plug-Flow detention time= 162.7 min calculated for 7.615 af (57% of inflow) Center-of-Mass det. time= 85.6 min (1,032.8 - 947.3)

Volume	Invert	Avail.Stor	rage Storage	Description			
#1	87.50'	541,13	32 cf Custom	n Stage Data (Pr	ismatic)Listed below (Recalc)		
Elevatio (fee 87.5 88.0 89.0 90.0	et) 50 21 00 21 00 21	f.Area (sq-ft) 1,274 3,338 7,483 21,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132			
Device	Routing	Invert	Outlet Device				
#1	Discarded	87.50'	0.350 in/hr E	xfiltration over	Surface area Phase-In= 0.01'		
#2	Primary	88.50'	<b>43.6 deg x 5</b> Cv= 2.56 (C=	•	rise Sharp-Crested Vee/Trap Weir		
Discord	Discorded OutElow May -1 75 of a 16 25 bra LIW-99 79' (Free Discharge)						

**Discarded OutFlow** Max=1.75 cfs @ 16.35 hrs HW=88.78' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.75 cfs)

Primary OutFlow Max=23.77 cfs @ 16.35 hrs HW=88.78' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir (Weir Controls 23.77 cfs @ 1.69 fps) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

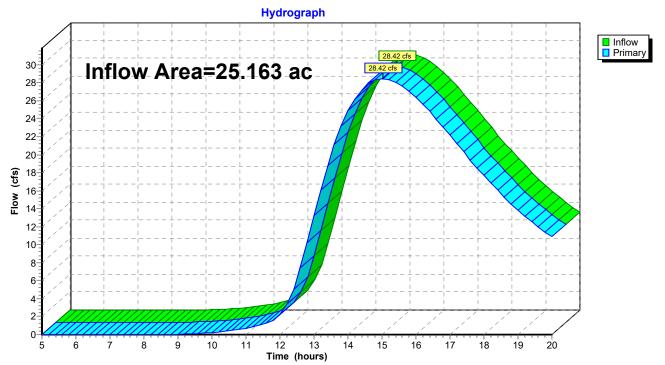


# Pond 3P: PROPOSED POND

# Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Are	a =	25.163 ac,	0.00% Impervious, Inflow I	Depth > 6.17" for 7 DAY-100YR event
Inflow	=	28.42 cfs @	15.02 hrs, Volume=	12.932 af
Primary	=	28.42 cfs @	15.02 hrs, Volume=	12.932 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

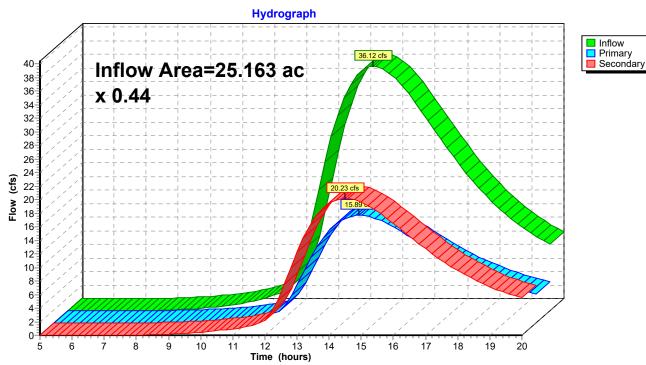


# Link 1L: EXISTING OUTFALL LOCATION

### Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow I	Depth > 7.37" for 7 DAY-100YR event
Inflow =	36.12 cfs @	14.50 hrs, Volume=	15.451 af
Primary =	15.89 cfs @	14.50 hrs, Volume=	6.798 af, Atten= 56%, Lag= 0.0 min
Secondary =	20.23 cfs @	14.50 hrs, Volume=	8.652 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



# Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD Report Prepared by HP Inc. HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Softwa	Type II 24-hr 10 DAY-100YR Rainfall=16.10" Printed 3/16/2020
	are Solutions LLC Page 25
Time span=5.00-20.00 hrs Runoff by SCS TR-20 method, UI Reach routing by Stor-Ind+Trans method	H=Georgia-323, Weighted-CN
	=1,096,103 sf 0.00% Impervious Runoff Depth>7.66" ' Tc=222.3 min CN=58 Runoff=35.22 cfs 16.072 af

Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>9.01" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=44.01 cfs 18.891 af

Pond 1P: ROCK LAYDOWN AREANO.1 Peak Elev=90.55' Storage=21,675 cf Inflow=19.36 cfs 8.312 af Discarded=1.00 cfs 0.866 af Primary=26.10 cfs 6.971 af Outflow=27.11 cfs 7.837 af

Pond 2P: ROCK LAYDOWN AREANO.2 Peak Elev=90.55' Storage=13,418 cf Inflow=24.64 cfs 10.579 af Discarded=0.62 cfs 0.580 af Primary=26.55 cfs 9.669 af Outflow=27.17 cfs 10.249 af

 Pond 3P: PROPOSED POND
 Peak Elev=88.85' Storage=289,266 cf
 Inflow=47.52 cfs
 16.640 af

 Discarded=1.76 cfs
 1.092 af
 Primary=33.39 cfs
 9.867 af
 Outflow=35.14 cfs
 10.958 af

Link 1L: EXISTING OUTFALL LOCATION

Inflow=35.22 cfs 16.072 af Primary=35.22 cfs 16.072 af

x 0.44 Inflow=44.01 cfs 18.891 af Primary=19.36 cfs 8.312 af Secondary=24.64 cfs 10.579 af

Link 2L: POST DEVELOPED FLOW

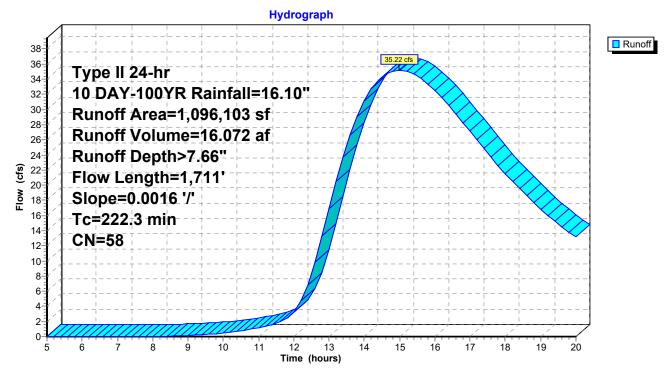
#### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 35.22 cfs @ 14.99 hrs, Volume= 16.072 af, Depth> 7.66"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 10 DAY-100YR Rainfall=16.10"

	A	rea (sf)	CN E	<b>Description</b>			
	1,0	96,103	58 N	58 Meadow, non-grazed, HSG B			
	1,0	96,103	1	00.00% Pe	ervious Are	а	
(m	Tc nin)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
22	2.3	1,711	0.0016	0.13		Lag/CN Method,	

### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



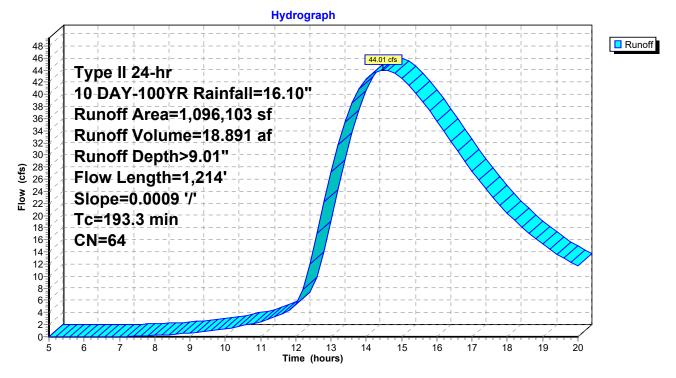
#### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff 44.01 cfs @ 14.47 hrs, Volume= 18.891 af, Depth> 9.01" =

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 10 DAY-100YR Rainfall=16.10"

_	A	rea (sf)	CN E	Description		
*	5	76,632	65 L	Incompact	ed Gravel(	35% Void Ratio)
	4	21,336	58 N	/leadow, no	on-grazed,	HSG B
_		98,135	85 C	Gravel road	ls, HSG B	
	1,0	96,103	64 V	Veighted A	verage	
	1,0	96,103	1	00.00% Pe	ervious Are	ea
	Та	l a sa aith	Clana	Valacity	Consister	Description
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	193.3	1,214	0.0009	0.10		Lag/CN Method,

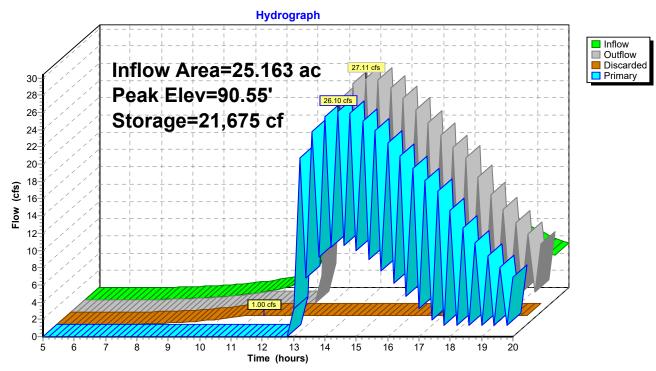
#### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	19.36 cfs @ 1 27.11 cfs @ 1 1.00 cfs @ 1	.00% Impervious 4.47 hrs, Volum 4.40 hrs, Volum 1.60 hrs, Volum 4.40 hrs, Volum	e= 8.312 e= 7.837 e= 0.866	2 af 7 af, Atten= 0' 5 af	10 DAY-100YR event %, Lag= 0.0 min
	-Ind method, Time 55' @ 14.40 hrs				
Center-of-Mass	ntion time= 27.2 m det. time= 12.3 m nvert Avail.Sto		2)	f inflow)	
				(* ) :	
#1 8	9.50' 21,6	75 cf <b>Custom</b> 61,928 cf	Overall x 35.0%		below (Recalc)
Elevation	Surf.Area	Inc.Store	Cum.Store		
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)		
89.50	123,855	0	0		
90.00	123,855	61,928	61,928		
	,	,	,		
Device Routir	ng Invert	Outlet Devices			
#1 Prima	ry 89.90'	16.0' long x 0	.5' breadth Bro	ad-Crested R	ectangular Weir
			20 0.40 0.60 0.		•
		Coef. (English)	2.80 2.92 3.08	8 3.30 3.32	
#2 Discai	rded 89.50'	0.350 in/hr Ex	filtration over S	urface area	Phase-In= 0.01'
	<b>Discarded OutFlow</b> Max=1.00 cfs @ 11.60 hrs HW=89.53' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 1.00 cfs)				

Primary OutFlow Max=26.05 cfs @ 14.40 hrs HW=90.55' (Free Discharge) —1=Broad-Crested Rectangular Weir (Weir Controls 26.05 cfs @ 2.52 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

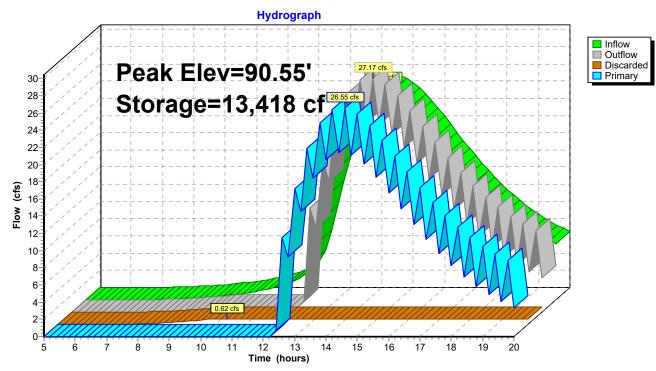
Inflow =	24.64 cfs @	14.47 hrs, Volume=	10.579 af
Outflow =	27.17 cfs @	14.60 hrs, Volume=	10.249 af, Atten= 0%, Lag= 7.4 min
Discarded =	0.62 cfs @	10.40 hrs, Volume=	0.580 af
Primary =	26.55 cfs @	14.60 hrs, Volume=	9.669 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.55' @ 14.60 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 14.4 min calculated for 10.249 af (97% of inflow) Center-of-Mass det. time= 6.2 min (935.4 - 929.2)

Volume	Invert	Avail.Stor	age Storage	Description	
#1	89.50'	13,41		<b>Stage Data (Prismatic)</b> Listed f Overall x 35.0% Voids	d below (Recalc)
Elevatio (fee		.Area /sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
89.5	1	6,672	0	0	
90.0		6,672	38,336	38,336	
Device	Routing	Invert	Outlet Device	3	
#1	Primary	89.90'	•	<b>0.5' breadth Broad-Crested</b> 20 0.40 0.60 0.80 1.00	Rectangular Weir
			· · ·	) 2.80 2.92 3.08 3.30 3.32	
#2	Discarded	89.50'		filtration over Surface area	
<b>Discarded OutFlow</b> Max=0.62 cfs @ 10.40 hrs HW=89.52' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 0.62 cfs)					

Primary OutFlow Max=26.47 cfs @ 14.60 hrs HW=90.55' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 26.47 cfs @ 2.54 fps)



# Pond 2P: ROCK LAYDOWN AREA No.2

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#### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow	Depth > 7.94" for 10 DAY-100YR event
Inflow =	47.52 cfs @	14.40 hrs, Volume=	16.640 af
Outflow =	35.14 cfs @	15.87 hrs, Volume=	10.958 af, Atten= 26%, Lag= 88.3 min
Discarded =	1.76 cfs @	15.87 hrs, Volume=	1.092 af
Primary =	33.39 cfs @	15.87 hrs, Volume=	9.867 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 88.85' @ 15.87 hrs Surf.Area= 216,867 sf Storage= 289,266 cf

Plug-Flow detention time= 140.7 min calculated for 10.958 af (66% of inflow) Center-of-Mass det. time= 73.5 min (1,016.6 - 943.1)

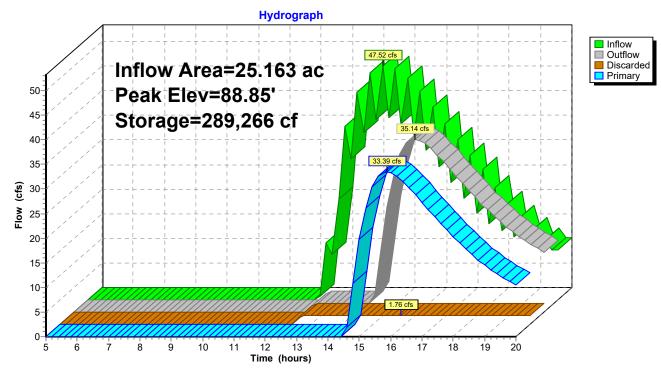
Volume	Invert	Avail.Stor	rage Storage	Description	
#1	87.50'	541,13	32 cf Custom	n Stage Data (Pr	ismatic)Listed below (Recalc)
Elevatio (fee 87.5 88.0 89.0 90.0	et) 50 21 00 21 00 21	f.Area (sq-ft) 1,274 3,338 7,483 21,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132	
Device	Routing	Invert	Outlet Device	es	
#1	Discarded	87.50'	0.350 in/hr E	xfiltration over	Surface area Phase-In= 0.01'
#2	Primary	88.50'	<b>43.6 deg x 5</b> Cv= 2.56 (C=	•	rise Sharp-Crested Vee/Trap Weir
Discord	ad OutFlow	Max=1.76 af	a @ 15 07 hra		

**Discarded OutFlow** Max=1.76 cfs @ 15.87 hrs HW=88.85' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.76 cfs)

Primary OutFlow Max=33.28 cfs @ 15.87 hrs HW=88.85' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir (Weir Controls 33.28 cfs @ 1.89 fps)

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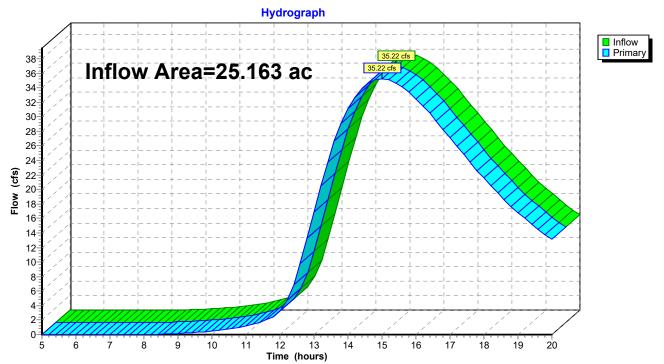


# Pond 3P: PROPOSED POND

### Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Are	a =	25.163 ac,	0.00% Impervious, Inflow De	epth > 7.66" for 10 DAY-100YR event
Inflow	=	35.22 cfs @	14.99 hrs, Volume=	16.072 af
Primary	=	35.22 cfs @	14.99 hrs, Volume=	16.072 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

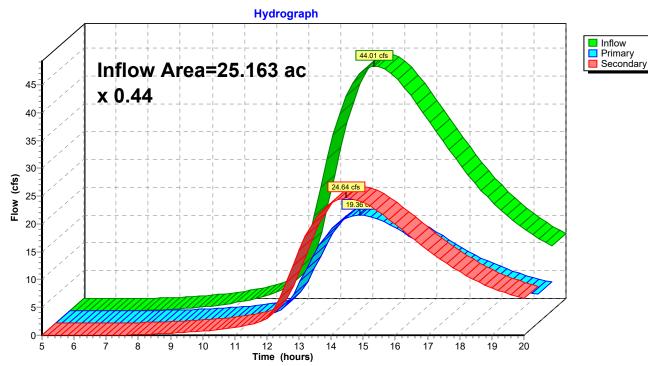


# Link 1L: EXISTING OUTFALL LOCATION

### Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow	Depth > 9.01" for 10 DAY-100YR event
Inflow =	44.01 cfs @	14.47 hrs, Volume=	18.891 af
Primary =	19.36 cfs @	14.47 hrs, Volume=	8.312 af, Atten= 56%, Lag= 0.0 min
Secondary =	24.64 cfs @	14.47 hrs, Volume=	10.579 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



# Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD ReportType II 24-hr10-YR - 24HR. Rainfall=6.72"Prepared by HP Inc.Printed 3/16/2020HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLCPage 36
Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment1S: PRE DEVELOPEDRunoff Area=1,096,103 sf0.00% ImperviousRunoff Depth>1.61"Flow Length=1,711'Slope=0.0016 '/'Tc=222.3 minCN=58Runoff=7.35 cfs3.370 af
Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>2.19" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=10.66 cfs 4.583 af
Pond 1P: ROCK LAYDOWN AREA No.1Peak Elev=90.10' Storage=21,675 cfInflow=4.69 cfs2.017 afDiscarded=1.00 cfs0.648 afPrimary=3.94 cfs0.905 afOutflow=4.94 cfs1.553 af
Pond 2P: ROCK LAYDOWN AREA No.2Peak Elev=90.21' Storage=13,418 cfInflow=5.97 cfs2.567 afDiscarded=0.62 cfs0.412 afPrimary=7.96 cfs1.848 afOutflow=8.58 cfs2.260 af
Pond 3P: PROPOSED POND         Peak Elev=87.88' Storage=81,577 cf         Inflow=11.07 cfs         2.753 af           Discarded=1.72 cfs         0.876 af         Primary=0.00 cfs         0.000 af         Outflow=1.72 cfs         0.876 af
Link 1L: EXISTING OUTFALL LOCATIONInflow=7.35 cfs3.370 afPrimary=7.35 cfs3.370 af
Link 2L: POST DEVELOPED FLOWx 0.44Inflow=10.66 cfs4.583 afPrimary=4.69 cfs2.017 afSecondary=5.97 cfs2.567 af

### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

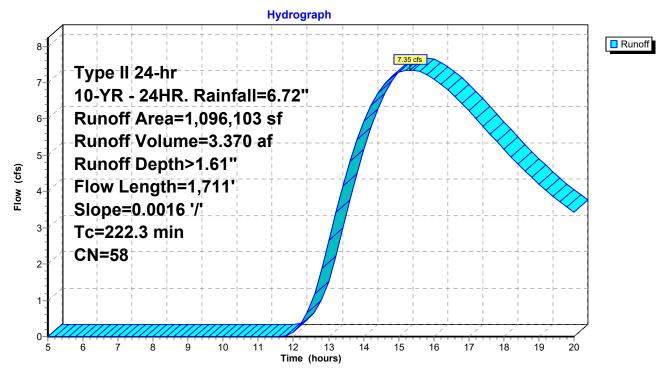
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Runoff 7.35 cfs @ 15.32 hrs, Volume= = 3.370 af, Depth> 1.61"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

Ar	ea (sf)	CN E	Description					
1,0	96,103	58 N	Meadow, non-grazed, HSG B					
1,09	96,103	1	00.00% Pe	ervious Are	ea			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
222.3	1,711	0.0016	0.13		Lag/CN Method,			

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



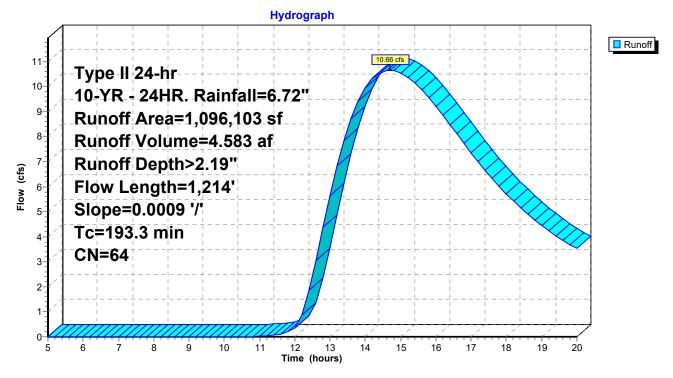
# Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff 10.66 cfs @ 14.69 hrs, Volume= = 4.583 af, Depth> 2.19"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 10-YR - 24HR. Rainfall=6.72"

	A	rea (sf)	CN [	Description					
*	5	76,632	65 l	Incompact	ed Gravel(	35% Void Ratio)			
	4	21,336	58 N	Meadow, non-grazed, HSG B					
		98,135	85 (	Gravel roads, HSG B					
	1,096,103 64 Weighted Average			Veighted A	verage				
	1,096,103		100.00% F		Pervious Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	193.3	1,214	0.0009	0.10		Lag/CN Method,			

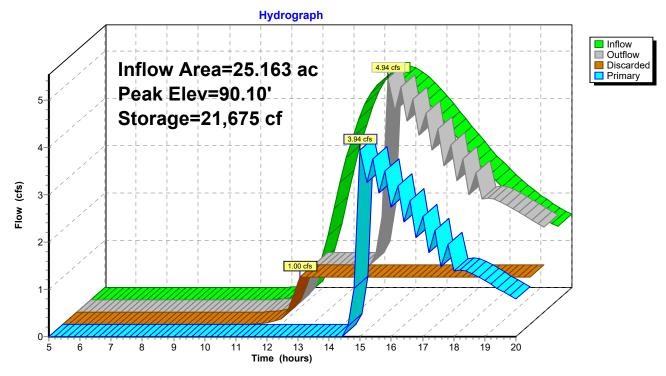
### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	4.69 cfs @ 1 4.94 cfs @ 1 1.00 cfs @ 1	.00% Impervious 4.69 hrs, Volum 5.00 hrs, Volum 2.60 hrs, Volum 5.00 hrs, Volum	e= 2.01 e= 1.55 e= 0.64	17 af	10-YR - 24HR. event %, Lag= 18.5 min		
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.10' @ 15.00 hrs Surf.Area= 123,855 sf Storage= 21,675 cf							
Plug-Flow detention time= 91.4 min calculated for 1.553 af (77% of inflow) Center-of-Mass det. time= 41.5 min(992.1 - 950.6) Volume Invert Avail.Storage Storage Description							
		75 cf <b>Custom</b>		rismatic) isted	below (Recalc)		
			Overall x 35.0				
Elevation	Surf.Area	Inc.Store	Cum.Store				
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)				
89.50	123,855	0	0				
90.00	123,855	61,928	61,928				
Device Routing	g Invert	Outlet Devices					
#1 Primar	y 89.90'	16.0' long x 0	.5' breadth Bro	oad-Crested R	ectangular Weir		
		Head (feet) 0.2	20 0.40 0.60 (	0.80 1.00	-		
		Coef. (English) 2.80 2.92 3.08 3.30 3.32					
#2 Discard	ded 89.50'	0.350 in/hr Ex	filtration over	Surface area	Phase-In= 0.01'		
<b>Discarded OutFlow</b> Max=1.00 cfs @ 12.60 hrs HW=89.51' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 1.00 cfs)							

**Primary OutFlow** Max=3.94 cfs @ 15.00 hrs HW=90.10' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 3.94 cfs @ 1.25 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

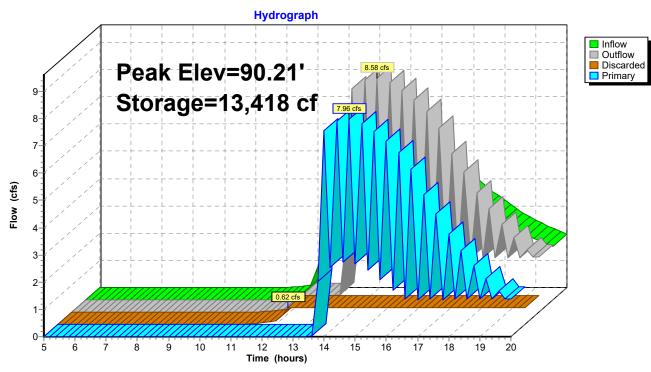
Inflow = Outflow =		14.69 hrs, Volume= 14.80 hrs, Volume=	2.567 af 2.260 af, Atten= 0%, Lag= 6.4 min
Discarded =	0.62 cfs @	12.40 hrs, Volume=	0.412 af
Primary =	7.90 CIS @	14.80 hrs, Volume=	1.848 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.21' @ 14.80 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 49.2 min calculated for 2.260 af (88% of inflow) Center-of-Mass det. time= 21.4 min (972.1 - 950.6)

Volume	Invert	Avail.Stor	rage Storage	Description			
#1	#1 89.50' 13,418			<b>Stage Data (Pr</b> of Overall x 35.0		below (Recalc)	
Elevation Surf.Area (feet) (sq-ft)			Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
89.5	50 7	6,672	0	0			
90.0	90.00 76,672		38,336	38,336			
Device	Routing	Invert	Outlet Device	S			
#1	Primary	Primary 89.90'		<b>0.5' breadth Br</b> 0.20 0.40 0.60 n) 2.80 2.92 3.0	0.80 1.00	Rectangular Weir	
#2	Discarded	89.50'				Phase-In= 0.01'	
<b>Discarded OutFlow</b> Max=0.62 cfs @ 12.40 hrs HW=89.51' (Free Discharge) <b>1 2=Exfiltration</b> (Exfiltration Controls 0.62 cfs)							

Primary OutFlow Max=7.94 cfs @ 14.80 hrs HW=90.21' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 7.94 cfs @ 1.60 fps) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC



# Pond 2P: ROCK LAYDOWN AREA No.2

### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	epth > 1.31" for 10-YR - 24HR. event
Inflow =	11.07 cfs @	15.20 hrs, Volume=	2.753 af
Outflow =	1.72 cfs @	20.00 hrs, Volume=	0.876 af, Atten= 84%, Lag= 288.3 min
Discarded =	1.72 cfs @	20.00 hrs, Volume=	0.876 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 87.88' @ 20.00 hrs Surf.Area= 212,862 sf Storage= 81,577 cf

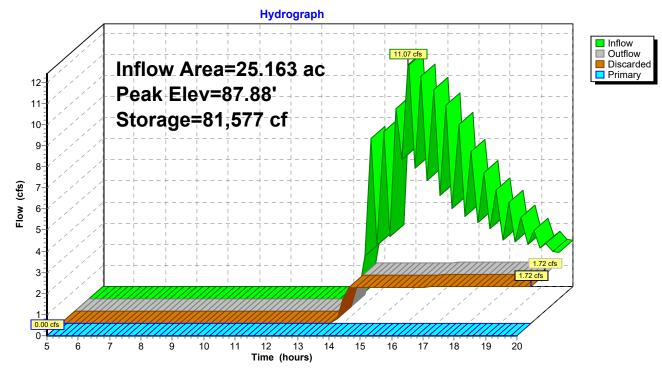
Plug-Flow detention time= 137.9 min calculated for 0.865 af (31% of inflow) Center-of-Mass det. time= 36.6 min (1,021.3 - 984.7)

Volume	Invert	Avail.Sto	rage Storage	e Description			
#1	87.50'	541,13	32 cf Custon	n Stage Data (Pi	<b>'ismatic)</b> Listed below (Recalc)		
Elevatio (fee 87.5 88.0 89.0 90.0	t) 50 2 00 2 00 2	urf.Area (sq-ft) 211,274 213,338 217,483 221,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132			
Device	Routing	Invert	Outlet Device	es			
#1 #2	Discarded Primary	87.50' 88.50'		0.0' long x 1.50'	Surface area Phase-In= 0.01' rise Sharp-Crested Vee/Trap Weir		
<b>Discarded OutFlow</b> Max=1 72 cfs @ 20 00 hrs HW=87 88' (Free Discharge)							

**Discarded OutFlow** Max=1.72 cfs @ 20.00 hrs HW=87.88' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.72 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC



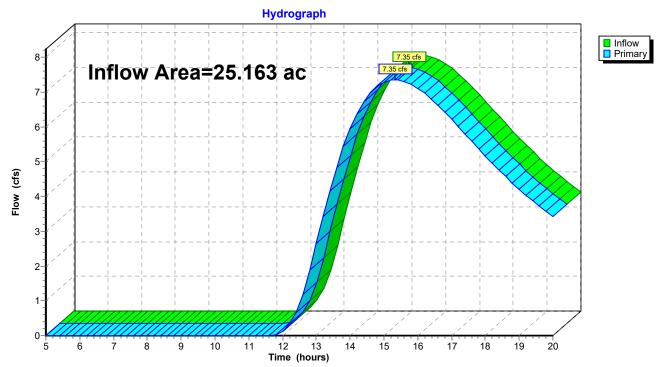


# Pond 3P: PROPOSED POND

### Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Area	=	25.163 ac,	0.00% Impervious, Inflow De	epth > 1.61" for 10-YR - 24HR. event
Inflow =	=	7.35 cfs @	15.32 hrs, Volume=	3.370 af
Primary =	=	7.35 cfs @	15.32 hrs, Volume=	3.370 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

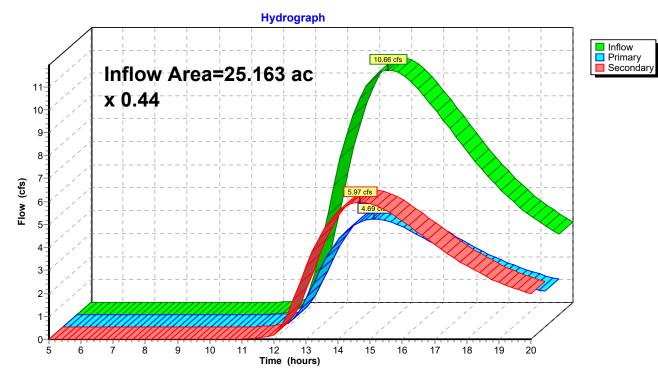


# Link 1L: EXISTING OUTFALL LOCATION

### Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow Depth	> 2.19" for 10-YR - 24HR. event
Inflow =	10.66 cfs @	14.69 hrs, Volume= 4.58	3 af
Primary =	4.69 cfs @	14.69 hrs, Volume= 2.01	7 af, Atten= 56%, Lag= 0.0 min
Secondary =	5.97 cfs @	14.69 hrs, Volume= 2.56	67 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



#### Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD ReportType II 24-hr25-YR - 24HR. Rainfall=7.92"Prepared by HP Inc.Printed 3/16/2020HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLCPage 47
Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method . Pond routing by Stor-Ind method
Subcatchment1S: PRE DEVELOPEDRunoff Area=1,096,103 sf0.00% ImperviousRunoff Depth>2.25"Flow Length=1,711'Slope=0.0016 '/'Tc=222.3 minCN=58Runoff=10.37 cfs4.726 af
Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>2.95" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=14.48 cfs 6.191 af
Pond 1P: ROCK LAYDOWN AREANO.1Peak Elev=90.19' Storage=21,675 cf Inflow=6.37 cfs 2.724 afDiscarded=1.00 cfs 0.666 af Primary=7.24 cfs 1.572 af Outflow=8.25 cfs 2.238 af
Pond 2P: ROCK LAYDOWN AREANo.2Peak Elev=90.24' Storage=13,418 cf Inflow=8.11 cfs 3.467 afDiscarded=0.62 cfs 0.427 af Primary=9.32 cfs 2.736 af Outflow=9.94 cfs 3.163 af
Pond 3P: PROPOSED POND         Peak Elev=88.19'         Storage=146,463 cf         Inflow=16.56 cfs         4.308 af           Discarded=1.73 cfs         0.930 af         Primary=0.00 cfs         0.000 af         Outflow=1.73 cfs         0.930 af
Link 1L: EXISTING OUTFALL LOCATIONInflow=10.37 cfs 4.726 af Primary=10.37 cfs 4.726 af
Link 2L: POST DEVELOPED FLOW x 0.44 Inflow=14.48 cfs 6.191 af

Primary=6.37 cfs 2.724 af Secondary=8.11 cfs 3.467 af

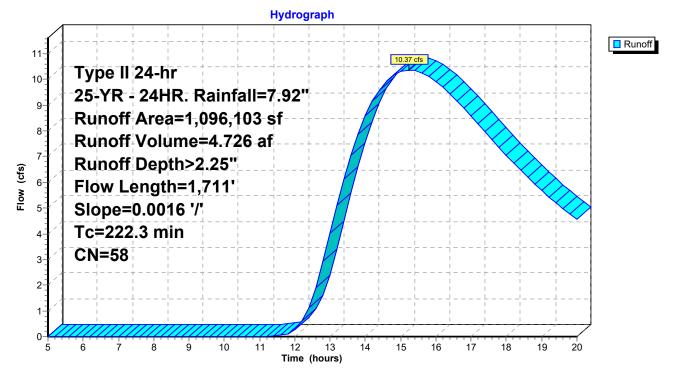
### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 10.37 cfs @ 15.23 hrs, Volume= 4.726 af, Depth> 2.25"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

A	rea (sf)	CN E	Description					
1,0	96,103	58 N	3 Meadow, non-grazed, HSG B					
1,0	96,103	100.00% Pervious Are			ea			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
222.3	1,711	0.0016	0.13		Lag/CN Method,			

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



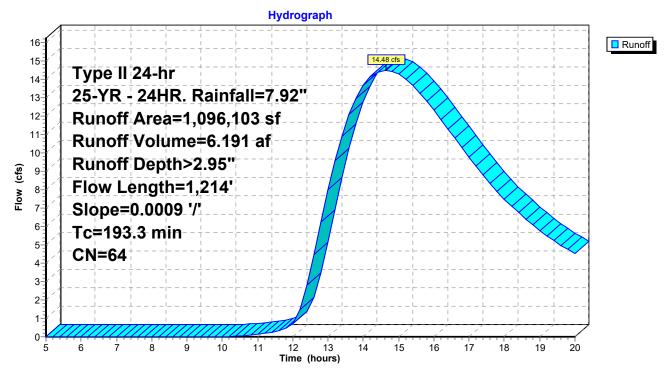
# Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff = 14.48 cfs @ 14.64 hrs, Volume= 6.191 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 25-YR - 24HR. Rainfall=7.92"

_	A	rea (sf)	CN [	Description					
*	5	76,632	65 l	Uncompacted Gravel( 35% Void Ratio)					
	4	21,336	58 N	/leadow, no	on-grazed,	HSG B			
_		98,135	85 (	Gravel roads, HSG B					
1,096,103 64 Weighted Average			Veighted A	verage					
	1,096,103		100.00%		Pervious Area				
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description			
_			. /		(013)				
	193.3	1,214	0.0009	0.10		Lag/CN Method,			

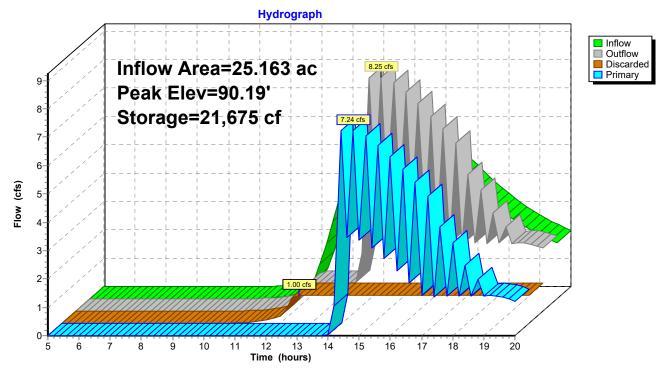
### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	6.37 cfs @ 14 8.25 cfs @ 14 1.00 cfs @ 12	00% Impervious, 1 4.64 hrs, Volume= 4.80 hrs, Volume= 2.60 hrs, Volume= 4.80 hrs, Volume=	= 2.724 ; = 2.238 ; = 0.666 ;	af, Atten= 0%, Lag= 9.6 min af	
		Span= 5.00-20.00 Surf.Area= 123,855			
	Plug-Flow detention time= 71.3 min calculated for 2.238 af (82% of inflow) Center-of-Mass det. time= 31.2 min (978.0 - 946.7) Volume Invert Avail.Storage Storage Description				
#1 89.				matic)Listed below (Recalc)	
#1 00.	21,01		verall x 35.0%		
		,			
Elevation	Surf.Area	Inc.Store	Cum.Store		
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)		
89.50	123,855	0	0		
90.00	123,855	61,928	61,928		
Device Routing	Invert	Outlet Devices			
#1 Primary	89.90'			d-Crested Rectangular Weir	
		Head (feet) 0.20			
Coef. (English) 2.80 2.92 3.08 3.30 3.32					
#2 Discard	ed 89.50'	0.350 in/hr Exfil	tration over Su	Irface area Phase-In= 0.01'	
<b>Discarded OutFlow</b> Max=1.00 cfs @ 12.60 hrs HW=89.52' (Free Discharge) <b>1 2=Exfiltration</b> (Exfiltration Controls 1.00 cfs)					

**Primary OutFlow** Max=7.22 cfs @ 14.80 hrs HW=90.19' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 7.22 cfs @ 1.54 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

Inflow	=	8.11 cfs @	14.64 hrs, Volume=	3.467 af
Outflow	=	9.94 cfs @	14.80 hrs, Volume=	3.163 af, Atten= 0%, Lag= 9.6 min
Discarded	=	0.62 cfs @	12.40 hrs, Volume=	0.427 af
Primary	=	9.32 cfs @	14.80 hrs, Volume=	2.736 af

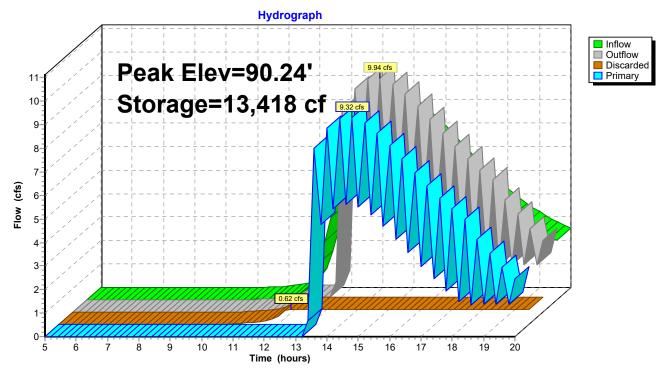
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.24' @ 14.80 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 37.6 min calculated for 3.163 af (91% of inflow) Center-of-Mass det. time= 16.6 min (963.3 - 946.7)

Volume	Invert	Avail.Stor	rage Storage	Description			
#1	89.50'	89.50' 13,418 cf		<b>Stage Data (Pr</b> of Overall x 35.0		below (Recalc)	
Elevatio (fee	vation Surf.Area (feet) (sq-ft)		Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
89.5	50 7	6,672	0	0			
90.0	,		38,336	38,336			
Device	Routing	Invert	Outlet Device	S			
#1	Primary 89.90'		Head (feet) C	<b>0.5' breadth Br</b> 0.20 0.40 0.60 n) 2.80 2.92 3.0	0.80 1.00	Rectangular Weir	
#2						Phase-In= 0.01'	
Discarded OutFlow Max=0.62 cfs @ 12.40 hrs HW=89.53' (Free Discharge)							

Primary OutFlow Max=9.28 cfs @ 14.80 hrs HW=90.24' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 9.28 cfs @ 1.69 fps) Prepared by HP Inc. HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

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# Pond 2P: ROCK LAYDOWN AREA No.2

### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	epth > 2.05" for 25-YR - 24HR. event
Inflow =	16.56 cfs @	14.80 hrs, Volume=	4.308 af
Outflow =	1.73 cfs @	20.00 hrs, Volume=	0.930 af, Atten= 90%, Lag= 312.1 min
Discarded =	1.73 cfs @	20.00 hrs, Volume=	0.930 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 88.19' @ 20.00 hrs Surf.Area= 214,120 sf Storage= 146,463 cf

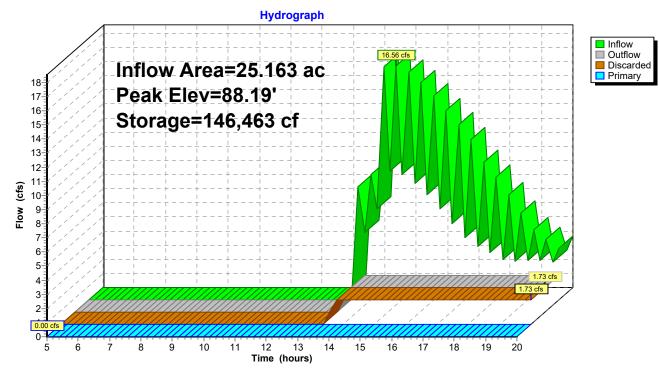
Plug-Flow detention time= 157.8 min calculated for 0.918 af (21% of inflow) Center-of-Mass det. time= 39.3 min (1,010.8 - 971.5)

Volume	Invert	Avail.Sto	rage Storage	e Description	
#1	87.50	541,13	32 cf Custor	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio (fee 87.5 88.0 89.0 90.0	t) 50	urf.Area (sq-ft) 211,274 213,338 217,483 221,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132	
Device	Routing	Invert	Outlet Device	es	
#1 Discarded 87.50' #2 Primary 88.50'			0.0' long x 1.50'	Surface area Phase-In= 0.01' rise Sharp-Crested Vee/Trap Weir	
<b>Discarded OutFlow</b> Max=1 73 cfs @ 20 00 hrs HW=88 19' (Free Discharge)					

**Discarded OutFlow** Max=1.73 cfs @ 20.00 hrs HW=88.19' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.73 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge) 2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

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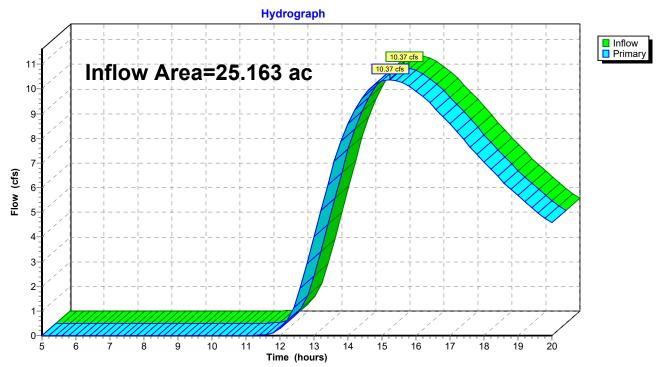
# Pond 3P: PROPOSED POND

# Summary for Link 1L: EXISTING OUTFALL LOCATION

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Inflow Are	a =	25.163 ac,	0.00% Impervious, Inflow D	epth > 2.25" for 25-YR - 24HR. event
Inflow	=	10.37 cfs @	15.23 hrs, Volume=	4.726 af
Primary	=	10.37 cfs @	15.23 hrs, Volume=	4.726 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

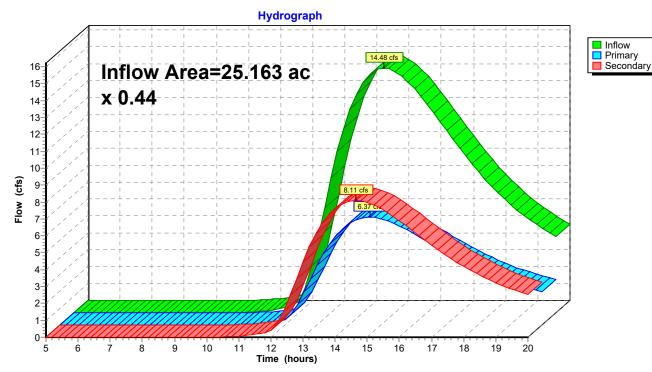


### Link 1L: EXISTING OUTFALL LOCATION

### Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	epth > 2.95" for 25-YR - 24HR. event
Inflow =	14.48 cfs @	14.64 hrs, Volume=	6.191 af
Primary =	6.37 cfs @	14.64 hrs, Volume=	2.724 af, Atten= 56%, Lag= 0.0 min
Secondary =	8.11 cfs @	14.64 hrs, Volume=	3.467 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



# Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD ReportType II 24-hr 1.00 hrs100-YR - 1HR. Rainfall=4.20"Prepared by HP Inc.Printed 3/16/2020HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLCPage 58

Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

	ea=1,096,103 sf 0.00% Impervious Runoff Depth>0.31" 016 '/' Tc=222.3 min CN=58 Runoff=3.06 cfs 0.644 af
	rea=1,096,103 sf 0.00% Impervious Runoff Depth>0.33" 0009 '/' Tc=193.3 min CN=64 Runoff=4.09 cfs 0.700 af
	k Elev=89.55' Storage=2,164 cf Inflow=1.80 cfs 0.308 af af Primary=0.00 cfs 0.000 af Outflow=1.00 cfs 0.308 af
	k Elev=89.77' Storage=7,301 cf Inflow=2.29 cfs 0.392 af af Primary=0.00 cfs 0.000 af Outflow=0.62 cfs 0.392 af
	Peak Elev=87.50' Storage=0 cf Inflow=0.00 cfs 0.000 af af Primary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Link 1L: EXISTING OUTFALL LOCATION	Inflow=3.06 cfs 0.644 af Primary=3.06 cfs 0.644 af
	x 0.44 Inflow=4.09 cfs. 0.700 af

x 0.44 Inflow=4.09 cfs 0.700 af Primary=1.80 cfs 0.308 af Secondary=2.29 cfs 0.392 af

Link 2L: POST DEVELOPED FLOW

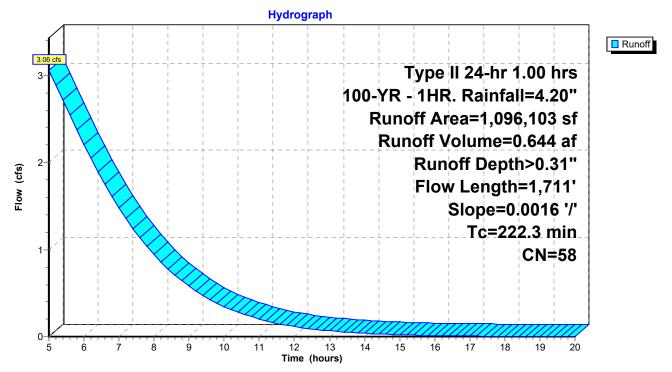
### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 3.06 cfs @ 5.00 hrs, Volume= 0.644 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

Ar	ea (sf)	CN [	Description			
1,09	96,103	58 N	Meadow, non-grazed, HSG B			
1,09	96,103		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
222.3	1,711	0.0016	0.13		Lag/CN Method,	

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



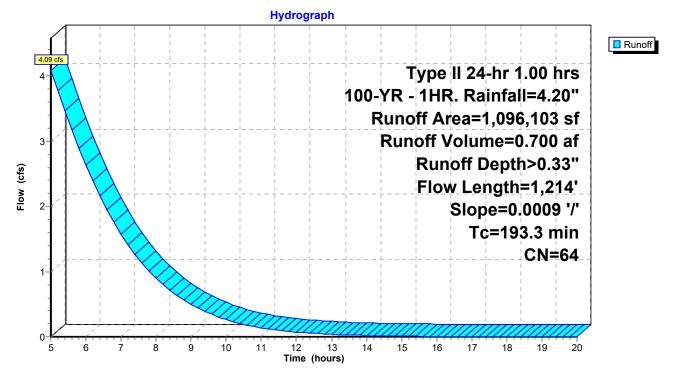
### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff = 4.09 cfs @ 5.00 hrs, Volume= 0.700 af, Depth> 0.33"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 1.00 hrs 100-YR - 1HR. Rainfall=4.20"

_	A	rea (sf)	CN E	Description				
*	5	76,632	65 Uncompacted Gravel( 35% Void Ratio)					
	4	421,336 58 Meadow, non-grazed, HSG B						
_		98,135	85 C	Gravel road	ls, HSG B			
	1,096,103 64 Weighted Average				verage			
	1,096,103 100.00% Pervious Area			00.00% Pe	ervious Are	ea		
			<b>•</b> •					
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	193.3	1,214	0.0009	0.10		Lag/CN Method,		
						-		

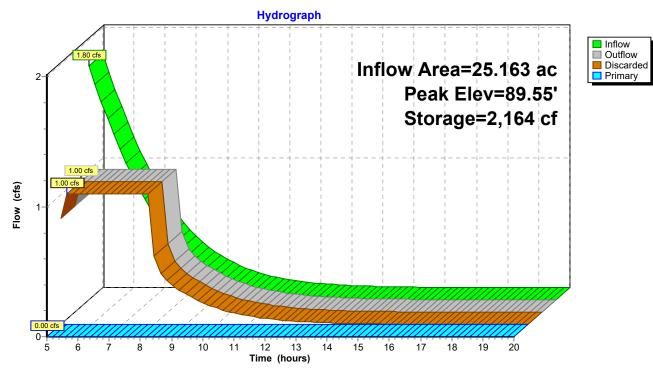
#### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



## Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	1.80 cfs @ 1.00 cfs @ 1.00 cfs @	00% Impervious, 5.00 hrs, Volum 5.20 hrs, Volum 5.20 hrs, Volum 5.00 hrs, Volum	e= 0.308 e= 0.308 e= 0.308	af af, Atten= 44 af	00-YR - 1HR. event %, Lag= 12.0 min			
	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 89.55' @ 6.29 hrs Surf.Area= 123,855 sf Storage= 2,164 cf							
Center-of-Mass	ntion time= 32.3 m det. time= 21.6 m nvert Avail.Sto		5)	inflow)				
			Stage Data (Pris	matic listed h	elow (Recalc)			
<i>π</i> ι 0.	21,0		Overall x 35.0%					
		• .,•=• •						
Elevation	Surf.Area	Inc.Store	Cum.Store					
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)					
89.50	123,855	0	0					
90.00	123,855	61,928	61,928					
Device Routin	g Invert	Outlet Devices						
#1 Primar	y 89.90'	16.0' long x 0	.5' breadth Broa	d-Crested Re	ctangular Weir			
	, ,		20 0.40 0.60 0.8		U			
		Coef. (English)	2.80 2.92 3.08	3.30 3.32				
#2 Discar	ded 89.50'	0.350 in/hr Ex	filtration over S	urface area F	Phase-In= 0.01'			
Discarded OutFlow Max=1.00 cfs @ 5.20 hrs HW=89.52' (Free Discharge) ←2=Exfiltration (Exfiltration Controls 1.00 cfs)								

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=89.51' (Free Discharge)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

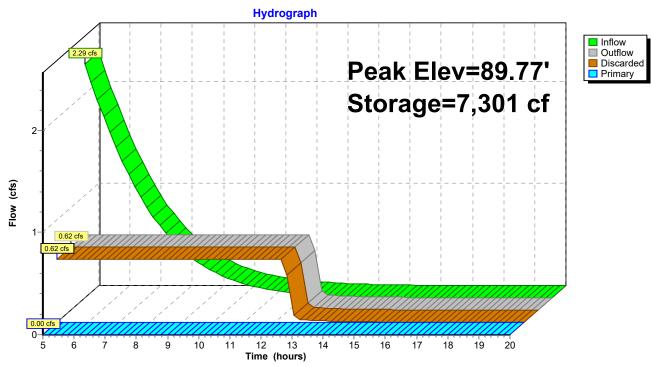
Inflow	=	2.29 cfs @	5.00 hrs, Volume=	0.392 af
Outflow	=	0.62 cfs @	5.00 hrs, Volume=	0.392 af, Atten= 73%, Lag= 0.0 min
Discarded	=	0.62 cfs @	5.00 hrs, Volume=	0.392 af
Primary	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 89.77' @ 7.64 hrs Surf.Area= 76,672 sf Storage= 7,301 cf

Plug-Flow detention time= 145.4 min calculated for 0.378 af (96% of inflow) Center-of-Mass det. time= 124.2 min ( 523.8 - 399.6 )

Volume	Invert	Avail.Stor	rage Storage	Description				
#1	89.50'	13,41	3 cf <b>Custom Stage Data (Prismatic)</b> Listed below (F 38,336 cf Overall x 35.0% Voids			below (Recalc)	_	
Elevatio (fee		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
89.5	50	76,672	0	0				
90.0	00	76,672	38,336	38,336				
Device	Routing	Invert	Outlet Device	S				
#1	Primary	89.90'		<b>0.5' breadth Br</b> 0.20 0.40 0.60		Rectangular Weir	-	
			Coef. (English) 2.80 2.92 3.08 3.30 3.32					
#2	Discarded	89.50'	0.350 in/hr Exfiltration over Surface area Phase-In= 0.01'					
Discarded OutFlow Max=0.62 cfs @ 5.00 hrs HW=89.52' (Free Discharge) ☐ 2=Exfiltration (Exfiltration Controls 0.62 cfs)								

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=89.52' (Free Discharge) ←1=Broad-Crested Rectangular Weir( Controls 0.00 cfs)



# Pond 2P: ROCK LAYDOWN AREA No.2

## Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	Pepth = 0.00" for 100-YR - 1HR. event
Inflow =	0.00 cfs @	5.00 hrs, Volume=	0.000 af
Outflow =	0.00 cfs @	5.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.00 cfs @	5.00 hrs, Volume=	0.000 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 87.50' @ 5.00 hrs Surf.Area= 211,274 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert	Avail.Sto	rage Storag	e Description			
#1	87.50'	541,13	32 cf Custor	n Stage Data (Prismatic)List	ed below (Recalc)		
Elevatio (fee 87.5	et)	urf.Area (sq-ft) 211,274	Inc.Store (cubic-feet) 0	Cum.Store (cubic-feet) 0			
88.0 89.0	)0 2 )0 2	213,338 217,483	106,153 215,411	106,153 321,564			
90.0	0 2	221,654	219,569	541,132			
Device	Routing	Invert	Outlet Devic	es			
#1 #2	Discarded Primary	87.50' 88.50'	••••••	xfiltration over Surface are 0.0' long x 1.50' rise Sharp- = 3.20)			
Discard	<b>Discarded OutFlow</b> Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge)						

**1=Exfiltration** (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

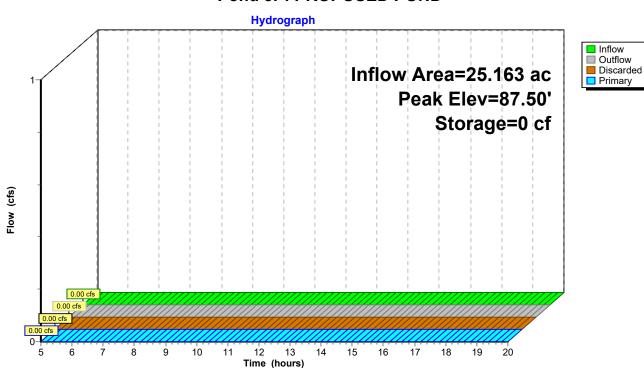
#### Staging Area 3 HydroCAD Report Prepared by HP Inc.

 Type II 24-hr 1.00 hrs
 100-YR - 1HR. Rainfall=4.20"

 Printed
 3/16/2020

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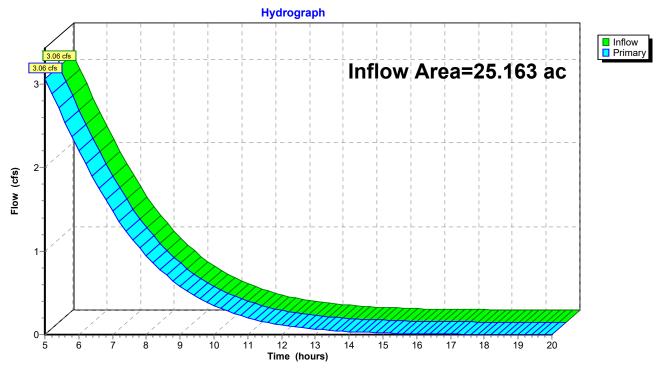


# Pond 3P: PROPOSED POND

## Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Area	a =	25.163 ac,	0.00% Impervious, Inflow D	epth > 0.31" for 100-YR - 1HR. event
Inflow	=	3.06 cfs @	5.00 hrs, Volume=	0.644 af
Primary	=	3.06 cfs @	5.00 hrs, Volume=	0.644 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

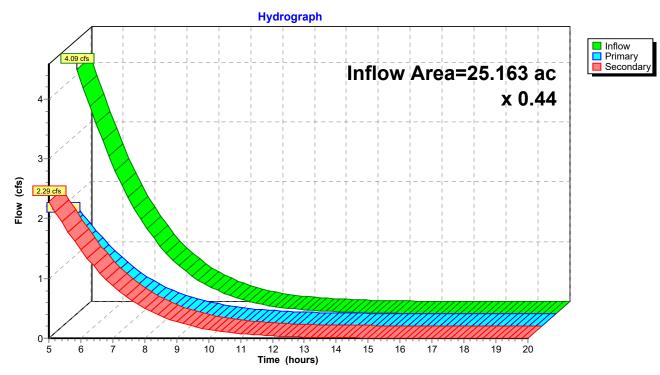


# Link 1L: EXISTING OUTFALL LOCATION

## Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow Depth > 0.33" for 100-YR - 1HR. event
Inflow =	4.09 cfs @	5.00 hrs, Volume= 0.700 af
Primary =	1.80 cfs @	5.00 hrs, Volume= 0.308 af, Atten= 56%, Lag= 0.0 min
Secondary =	2.29 cfs @	5.00 hrs, Volume= 0.392 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



### Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD Report Prepared by HP Inc.	Type II 24-hr 100-YF	R - 24HR. Rainfall=9.84" Printed 3/16/2020
HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software	e Solutions LLC	Page 69
Time span=5.00-20.00 hrs, d Runoff by SCS TR-20 method, UH=	· · ·	-CN

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: PRE DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>3.40" Flow Length=1,711' Slope=0.0016 '/' Tc=222.3 min CN=58 Runoff=15.68 cfs 7.122 af Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>4.27" Subcatchment2S: POST DEVELOPED Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=21.01 cfs 8.956 af Peak Elev=90.25' Storage=21,675 cf Inflow=9.24 cfs 3.941 af Pond 1P: ROCK LAYDOWN AREANo.1 Discarded=1.00 cfs 0.703 af Primary=9.69 cfs 2.742 af Outflow=10.69 cfs 3.445 af Peak Elev=90.33' Storage=13,418 cf Inflow=11.76 cfs 5.015 af Pond 2P: ROCK LAYDOWN AREANo.2 Discarded=0.62 cfs 0.462 af Primary=13.08 cfs 4.235 af Outflow=13.70 cfs 4.697 af Peak Elev=88.59' Storage=232,905 cf Inflow=19.83 cfs 6.977 af Pond 3P: PROPOSED POND Discarded=1.75 cfs 0.985 af Primary=4.41 cfs 0.708 af Outflow=6.15 cfs 1.694 af Link 1L: EXISTING OUTFALL LOCATION

Inflow=15.68 cfs 7.122 af Primary=15.68 cfs 7.122 af

Link 2L: POST DEVELOPED FLOW

x 0.44 Inflow=21.01 cfs 8.956 af Primary=9.24 cfs 3.941 af Secondary=11.76 cfs 5.015 af

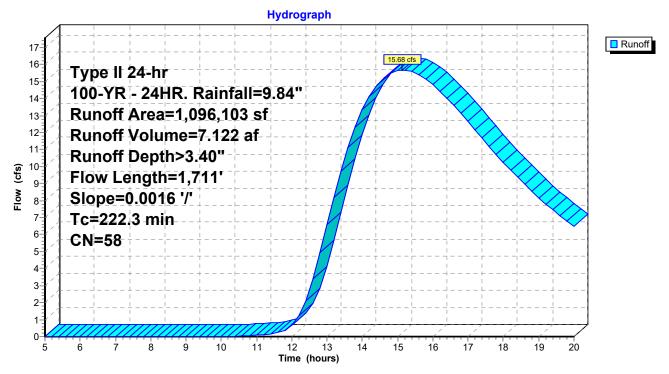
#### Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 15.68 cfs @ 15.14 hrs, Volume= 7.122 af, Depth> 3.40"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

Are	ea (sf)	CN E	escription					
1,09	6,103	58 N	58 Meadow, non-grazed, HSG B					
1,09	6,103	1	00.00% Pe	ervious Are	ea			
Tc   (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
222.3	1,711	0.0016	0.13		Lag/CN Method,			

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



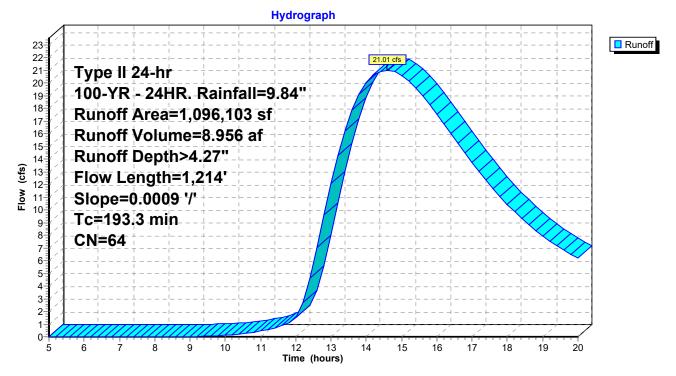
### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff 21.01 cfs @ 14.58 hrs, Volume= = 8.956 af, Depth> 4.27"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 100-YR - 24HR. Rainfall=9.84"

_	A	rea (sf)	CN [	Description		
*	5	76,632	65 l	Jncompact	ed Gravel(	35% Void Ratio)
	4	21,336	58 N	/leadow, no	on-grazed,	HSG B
_		98,135	85 (	Gravel road	ls, HSG B	
1,096,103 64 Weighted Average				Veighted A	verage	
	1,096,103 Tc Length Slo		1	00.00% Pe	ervious Are	ea
			Slope	Velocity	Capacity	Description
	(min)	Length (feet)	(ft/ft)	(ft/sec)	(cfs)	Description
_					(013)	
	193.3	1,214	0.0009	0.10		Lag/CN Method,

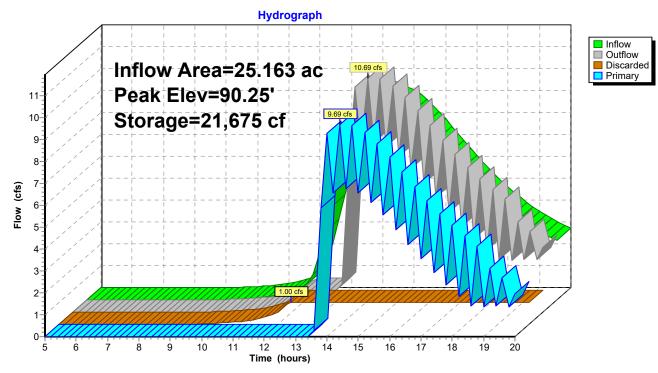
#### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Ar Inflow Outflow Discarde Primary	= 9.24 = 10.69 ed = 1.00	cfs @ 1 cfs @ 1 cfs @ 1	00% Impervious, Inflow Depth > 1.88" for 100-YR - 2 4.58 hrs, Volume= 3.941 af 4.40 hrs, Volume= 3.445 af, Atten= 0%, Lag= 0 2.40 hrs, Volume= 0.703 af 4.40 hrs, Volume= 2.742 af					
	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.25' @ 14.40 hrs Surf.Area= 123,855 sf Storage= 21,675 cf							
	f-Mass det. time	e= 22.0 m	in calculated for 3.400 af (86% of inflow) in(963.5 - 941.5) rage Storage Description					
-								
#1	89.50'	21,6	75 cf <b>Custom Stage Data (Prismatic)</b> Listed below (Rec 61,928 cf Overall x 35.0% Voids	calc)				
Elevatio	n Surf.A	rea	Inc.Store Cum.Store					
(fee	t) (so	q-ft)	(cubic-feet) (cubic-feet)					
89.5			0 0					
90.0			61,928 61,928					
00.0		000	01,020					
Device	Routing	Invert	Outlet Devices					
#1	Primary	89.90'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangula</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32	r Weir				
#2	Discarded	89.50'	0.350 in/hr Exfiltration over Surface area Phase-In=	0.01'				
Discarded OutFlow Max=1.00 cfs @ 12.40 hrs HW=89.52' (Free Discharge)								

**Primary OutFlow** Max=9.69 cfs @ 14.40 hrs HW=90.25' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 9.69 cfs @ 1.72 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

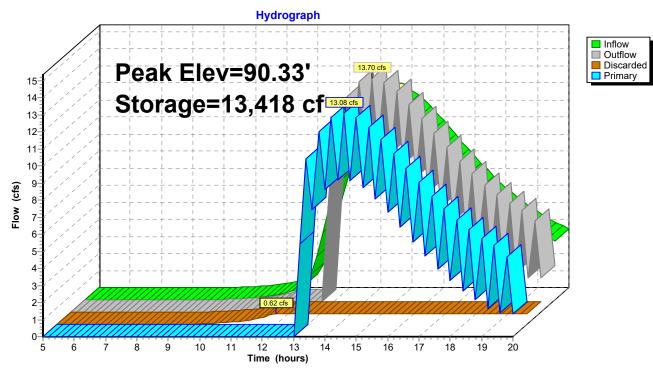
Inflow =	11.76 cfs @	14.58 hrs, Volume=	5.015 af
Outflow =	13.70 cfs @	14.60 hrs, Volume=	4.697 af, Atten= 0%, Lag= 1.4 min
Discarded =	0.62 cfs @	12.00 hrs, Volume=	0.462 af
Primary =	13.08 cfs @	14.60 hrs, Volume=	4.235 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.33' @ 14.60 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 26.4 min calculated for 4.635 af (92% of inflow) Center-of-Mass det. time= 11.0 min (952.6 - 941.5)

Volume	Invert	Avail.Stor	age Storage l	Description		
#1 89.50' 13,41			<b>Stage Data (Pr</b> f Overall x 35.0	r <b>ismatic)</b> Listed be 0% Voids	∍low (Recalc)	
Elevatio (fee		.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
89.5	50 7	6,672	0	0		
90.0	0 7	6,672	38,336	38,336		
Device	Routing	Invert	Outlet Devices	6		
#1	Primary	89.90'	•	0.5' breadth Bro 20 0.40 0.60	oad-Crested Red	tangular Weir
			· · ·	) 2.80 2.92 3.0		
#2	Discarded	89.50'			Surface area P	hase-In= 0.01'
<b>Discarded OutFlow</b> Max=0.62 cfs @ 12.00 hrs HW=89.51' (Free Discharge) <b>1</b> → <b>2=Exfiltration</b> (Exfiltration Controls 0.62 cfs)						

Primary OutFlow Max=13.07 cfs @ 14.60 hrs HW=90.33' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 13.07 cfs @ 1.92 fps)



# Pond 2P: ROCK LAYDOWN AREA No.2

#### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow	Depth > 3.33"	for 100-YR - 24HR. event
Inflow =	19.83 cfs @	14.60 hrs, Volume=	6.977 af	
Outflow =	6.15 cfs @	19.06 hrs, Volume=	1.694 af, Atte	en= 69%, Lag= 267.5 min
Discarded =	1.75 cfs @	19.06 hrs, Volume=	0.985 af	
Primary =	4.41 cfs @	19.06 hrs, Volume=	0.708 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 88.59' @ 19.06 hrs Surf.Area= 215,787 sf Storage= 232,905 cf

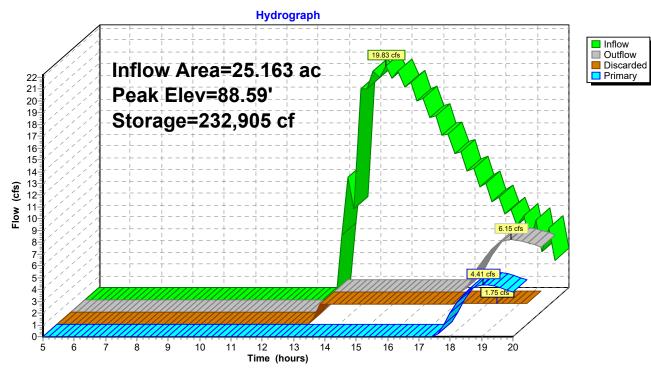
Plug-Flow detention time= 220.3 min calculated for 1.671 af (24% of inflow) Center-of-Mass det. time= 100.4 min (1,059.9 - 959.5)

Volume	Invert	Avail.Stor	rage Storage	Description	
#1	87.50'	541,13	32 cf Custon	n Stage Data (Pri	smatic)Listed below (Recalc)
Elevatio (fee 87.5 88.0 89.0 90.0	et) 50 2 <sup>2</sup> 00 2 <sup>2</sup> 00 2 <sup>2</sup>	Surf.Area (sq-ft) 211,274 213,338 217,483		Cum.Store (cubic-feet) 0 106,153 321,564 541,132	
Device	Routing	Invert	Outlet Device	es	
#1 #2	Discarded Primary	87.50' 88.50'		0.0' long x 1.50' i	Surface area Phase-In= 0.01' rise Sharp-Crested Vee/Trap Weir
<b>.</b>			,		

**Discarded OutFlow** Max=1.75 cfs @ 19.06 hrs HW=88.59' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.75 cfs)

Primary OutFlow Max=4.36 cfs @ 19.06 hrs HW=88.59' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir (Weir Controls 4.36 cfs @ 0.96 fps) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

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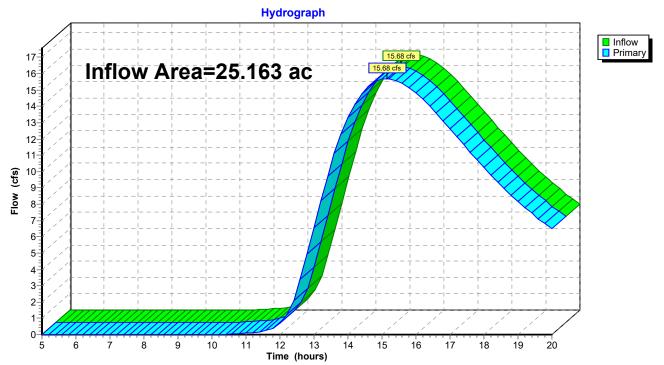


# Pond 3P: PROPOSED POND

## Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Area	a =	25.163 ac,	0.00% Impervious, Inflow De	pth > 3.40"	for 100-YR - 24HR. event
Inflow	=	15.68 cfs @	15.14 hrs, Volume=	7.122 af	
Primary	=	15.68 cfs @	15.14 hrs, Volume=	7.122 af, Att	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



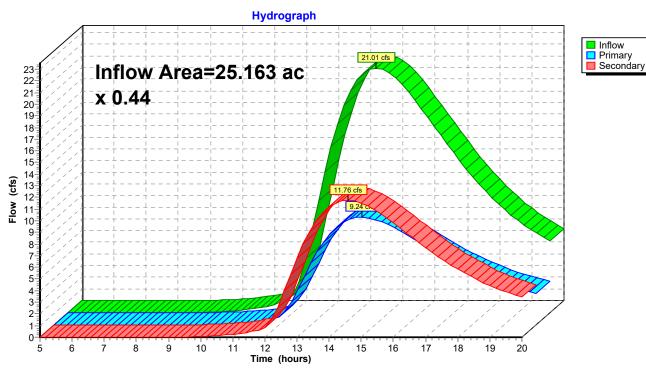
# Link 1L: EXISTING OUTFALL LOCATION

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## Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow	Depth > 4.27" for 100-YR - 24HR. event
Inflow =	21.01 cfs @	14.58 hrs, Volume=	8.956 af
Primary =	9.24 cfs @	14.58 hrs, Volume=	3.941 af, Atten= 56%, Lag= 0.0 min
Secondary =	11.76 cfs @	14.58 hrs, Volume=	5.015 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



# Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD ReportType II 24-hr 2.00 hrs100-YR - 2HR. Rainfall=5.10"Prepared by HP Inc.Printed 3/16/2020HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLCPage 80

Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: PRE DEVELOPEDRunoff Area=1,096,103 sf0.00% ImperviousRunoff Depth>0.62"Flow Length=1,711'Slope=0.0016 '/'Tc=222.3 minCN=58Runoff=5.67 cfs1.297 af
Subcatchment2S: POST DEVELOPEDRunoff Area=1,096,103 sf0.00% ImperviousRunoff Depth>0.66"Flow Length=1,214'Slope=0.0009 '/'Tc=193.3 minCN=64Runoff=7.52 cfs1.381 af
Pond 1P: ROCK LAYDOWN AREANO.1         Peak Elev=89.74'         Storage=10,516 cf         Inflow=3.31 cfs         0.608 af           Discarded=1.00 cfs         0.608 af         Primary=0.00 cfs         0.000 af         Outflow=1.00 cfs         0.608 af
Pond 2P: ROCK LAYDOWN AREANO.2Peak Elev=90.01' Storage=13,418 cfInflow=4.21 cfs0.774 afDiscarded=0.62 cfs0.545 afPrimary=1.67 cfs0.229 afOutflow=2.29 cfs0.774 af
Pond 3P: PROPOSED POND         Peak Elev=87.51'         Storage=3,147 cf         Inflow=1.67 cfs         0.229 af           Discarded=1.02 cfs         0.229 af         Primary=0.00 cfs         0.000 af         Outflow=1.02 cfs         0.229 af
Link 1L: EXISTING OUTFALLLOCATIONInflow=5.67 cfs1.297 afPrimary=5.67 cfs1.297 af
Link 2L: POST DEVELOPED FLOW x 0.44 Inflow=7.52 cfs 1.381 af

x 0.44 Inflow=7.52 cfs 1.381 at Primary=3.31 cfs 0.608 af Secondary=4.21 cfs 0.774 af

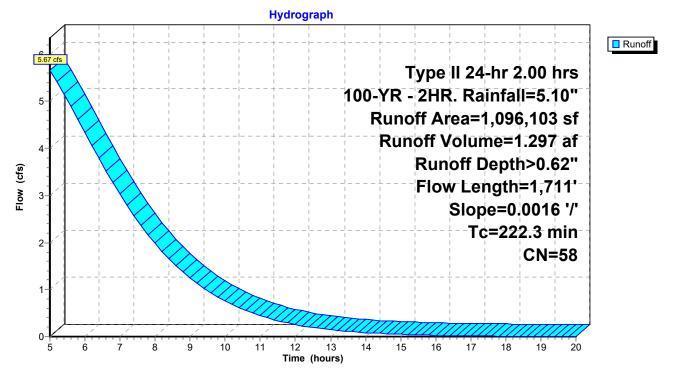
## Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 5.67 cfs @ 5.00 hrs, Volume= 1.297 af, Depth> 0.62"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

Area	a (sf)	CN E	Description					
1,096	,103	58 N	58 Meadow, non-grazed, HSG B					
1,096	,103	100.00% Pervious Area			ea			
Tc Lo (min)	ength (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
222.3	1,711	0.0016	0.13		Lag/CN Method,			

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



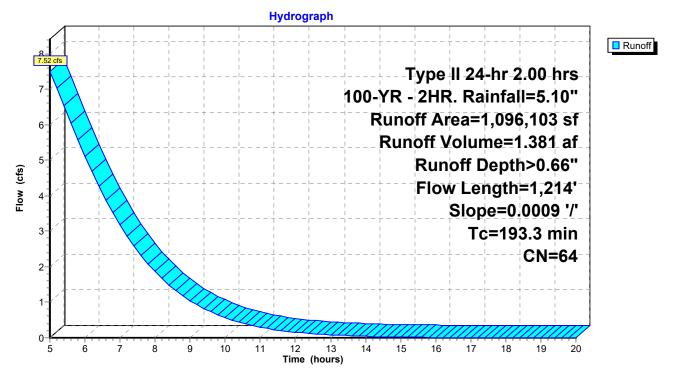
### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff = 7.52 cfs @ 5.00 hrs, Volume= 1.381 af, Depth> 0.66"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 2.00 hrs 100-YR - 2HR. Rainfall=5.10"

_	A	rea (sf)	CN [	Description		
*	5	76,632	65 l	Jncompact	( 35% Void Ratio)	
	421,336 58 Meadow, non-grazed, I				on-grazed,	HSG B
_		98,135	85 (	Gravel road	ls, HSG B	
	1,0	96,103	64 \	Veighted A	verage	
	1,0	96,103		100.00% Pervious Ar		ea
	-		~		<b>o</b> "	
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	193.3	1,214	0.0009	0.10		Lag/CN Method,
						-

#### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



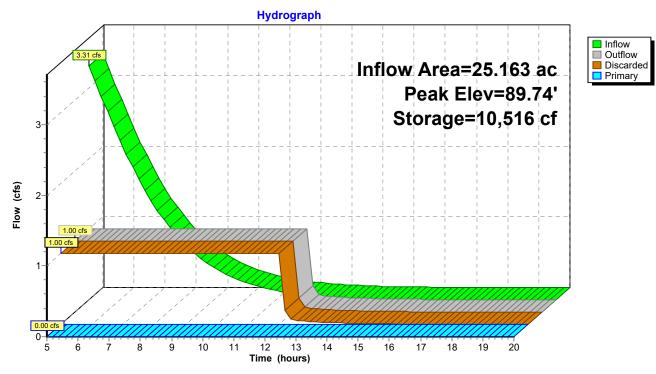
## Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area = Inflow = Outflow = Discarded = Primary =	3.31 cfs @ 1.00 cfs @ 1.00 cfs @	0.00% Impervious, 5.00 hrs, Volume 5.00 hrs, Volume 5.00 hrs, Volume 5.00 hrs, Volume	e= 0.608 af, Atten= 70%, Lag= 0.0 min e= 0.608 af				
Routing by Stor-	nd method, Tim	e Span= 5.00-20.	00 hrs, dt= 0.20 hrs				
Peak Elev= 89.7	4'@7.64 hrs S	Surf.Area= 123,85	5 sf Storage= 10,516 cf				
Center-of-Mass	Plug-Flow detention time= 130.2 min calculated for 0.589 af (97% of inflow) Center-of-Mass det. time= 110.8 min ( 515.0 - 404.2 )						
-	vert Avail.St	<u> </u>	Description				
#1 89	.50' 21,6		Stage Data (Prismatic)Listed below (Recalc) Overall x 35.0% Voids				
		01,020 01					
Elevation	Surf.Area	Inc.Store	Cum.Store				
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)				
89.50	123,855	0	0				
90.00	123,855	61,928	61,928				
Device Routing	n Invert	Outlet Devices					

DCVICC	rtouting	meen	Odiet Devices
#1	Primary	89.90'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Discarded	89.50'	0.350 in/hr Exfiltration over Surface area Phase-In= 0.01'

**Discarded OutFlow** Max=1.00 cfs @ 5.00 hrs HW=89.52' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 1.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=89.52' (Free Discharge)



# Pond 1P: ROCK LAYDOWN AREA No.1

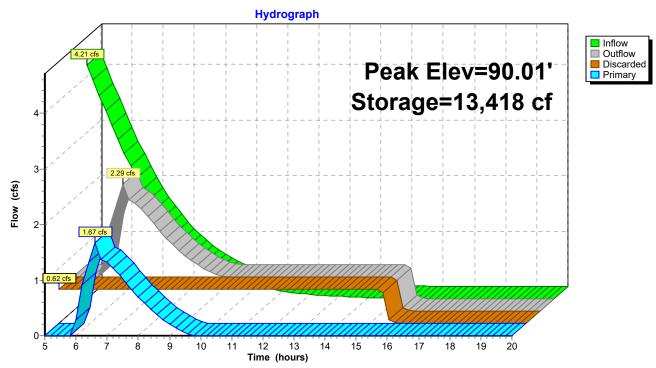
#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.01' @ 6.61 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 179.5 min calculated for 0.744 af (96% of inflow) Center-of-Mass det. time= 155.6 min ( 559.8 - 404.2 )

Volume Invert Avail.Storag		age Storage I	Description					
#1	89.50'	13,41		3 cf <b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) 38,336 cf Overall x 35.0% Voids				
			30,330 0		olds			
Elevatio	on Surf.	.Area	Inc.Store	Cum.Store				
(fee	et) (	sq-ft)	(cubic-feet)	(cubic-feet)				
89.5	50 76	6,672	0	0				
90.0	0 76	6,672	38,336	38,336				
Device	Routing	Invert	Outlet Devices	6				
#1	Primary	89.90'			-Crested Rectangular Weir			
			Head (feet) 0.20 0.40 0.60 0.80 1.00					
		00 501		) 2.80 2.92 3.08 3				
#2 Discarded 89.50'		0.350 in/hr Ex	filtration over Sur	face area Phase-In= 0.01'				
Discarded OutFlow Max=0.62 cfs @ 5.00 hrs HW=89.55' (Free Discharge) ☐ 2=Exfiltration (Exfiltration Controls 0.62 cfs)								

Primary OutFlow Max=1.65 cfs @ 6.61 hrs HW=90.01' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 1.65 cfs @ 0.93 fps)



# Pond 2P: ROCK LAYDOWN AREA No.2

### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	epth = 0.11" for 100-YR - 2HR. event
Inflow =	1.67 cfs @	6.61 hrs, Volume=	0.229 af
Outflow =	1.02 cfs @	7.50 hrs, Volume=	0.229 af, Atten= 39%, Lag= 53.7 min
Discarded =	1.02 cfs @	7.50 hrs, Volume=	0.229 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

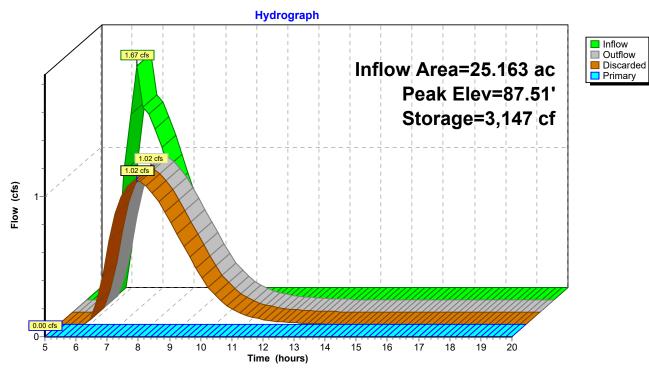
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 87.51' @ 7.50 hrs Surf.Area= 211,335 sf Storage= 3,147 cf

Plug-Flow detention time= 54.1 min calculated for 0.229 af (100% of inflow) Center-of-Mass det. time= 51.4 min (485.8 - 434.4)

Volume	Inver	t Avail.Sto	rage Storag	e Description				
#1	87.50	541,13	32 cf Custo	f Custom Stage Data (Prismatic)Listed below (Reca				
Elevatic (fee 87.5 88.0 89.0 90.0	et) 50 00 00	Gurf.Area (sq-ft) 211,274 213,338 217,483 221,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132				
Device	Routing	Invert	Outlet Devic	es				
#1 Discarded 87.50' #2 Primary 88.50'			50.0' long x 1.50' ri	urface area Phase-In= 0.01' ise Sharp-Crested Vee/Trap Weir				
Discard	<b>Discarded OutFlow</b> Max=1 71 cfs @ 7 50 hrs_HW=87 51' (Free Discharge)							

**Discarded OutFlow** Max=1.71 cfs @ 7.50 hrs HW=87.51' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.71 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge) 2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs) HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC

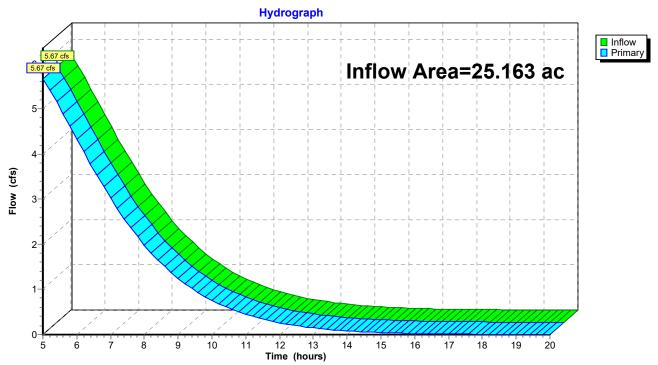


# Pond 3P: PROPOSED POND

## Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Area	a =	25.163 ac,	0.00% Impervious, Inflow D	epth > 0.62" for 100-YR - 2HR. event
Inflow	=	5.67 cfs @	5.00 hrs, Volume=	1.297 af
Primary	=	5.67 cfs @	5.00 hrs, Volume=	1.297 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

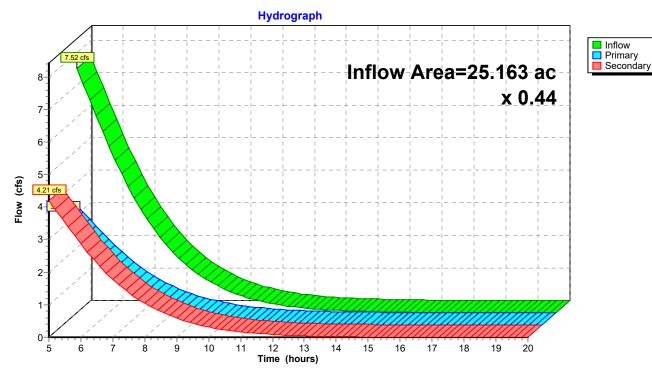


## Link 1L: EXISTING OUTFALL LOCATION

## Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow De	epth > 0.66" for 100-YR - 2HR. event
Inflow =	7.52 cfs @	5.00 hrs, Volume=	1.381 af
Primary =	3.31 cfs @	5.00 hrs, Volume=	0.608 af, Atten= 56%, Lag= 0.0 min
Secondary =	4.21 cfs @	5.00 hrs, Volume=	0.774 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



### Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD ReportType II 24-hr 4.00 hrs100-YR - 4HR. Rainfall=6.08"Prepared by HP Inc.Printed 3/16/2020HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLCPage 91

Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: PRE DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>1.32" Flow Length=1,711' Slope=0.0016 '/' Tc=222.3 min CN=58 Runoff=8.97 cfs 2.763 af Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>1.47" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=12.88 cfs 3.073 af Peak Elev=90.09' Storage=21,675 cf Inflow=5.67 cfs 1.352 af Pond 1P: ROCK LAYDOWN AREANo.1 Discarded=1.00 cfs 0.938 af Primary=3.64 cfs 0.415 af Outflow=4.64 cfs 1.352 af Peak Elev=90.18' Storage=13,418 cf Inflow=7.21 cfs 1.721 af Pond 2P: ROCK LAYDOWN AREANo.2 Discarded=0.62 cfs 0.634 af Primary=7.20 cfs 1.087 af Outflow=7.82 cfs 1.721 af Peak Elev=87.68' Storage=38,334 cf Inflow=7.06 cfs 1.502 af Pond 3P: PROPOSED POND Discarded=1.72 cfs 1.502 af Primary=0.00 cfs 0.000 af Outflow=1.72 cfs 1.502 af Link 1L: EXISTING OUTFALL LOCATION Inflow=8.97 cfs 2.763 af Primary=8.97 cfs 2.763 af Link 2L: POST DEVELOPED FLOW x 0.44 Inflow=12.88 cfs 3.073 af

Primary=5.67 cfs 1.352 af Secondary=7.21 cfs 1.721 af

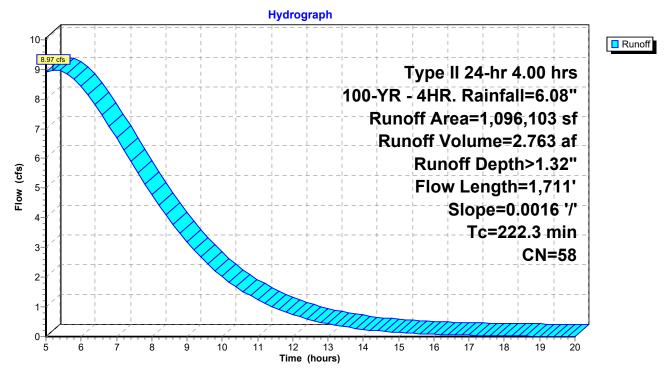
## Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 8.97 cfs @ 5.20 hrs, Volume= 2.763 af, Depth> 1.32"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 4.00 hrs 100-YR - 4HR. Rainfall=6.08"

	A	rea (sf)	CN I	CN Description						
1,096,103 58 Meadow, non-grazed, HSG B						HSG B				
	1,0	96,103		100.00% P	ervious Are	ea				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
2	222.3	1,711	0.0016	0.13		Lag/CN Method,				

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



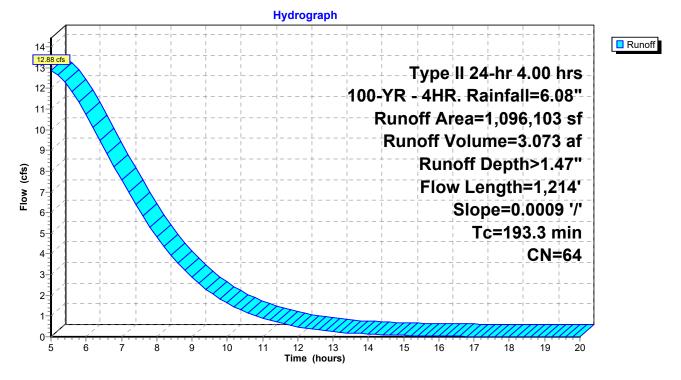
### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff = 12.88 cfs @ 5.00 hrs, Volume= 3.073 af, Depth> 1.47"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 4.00 hrs 100-YR - 4HR. Rainfall=6.08"

_	A	rea (sf)	CN [	Description				
* 576,632 65 Uncompacted Gravel( 35% Void Ra						35% Void Ratio)		
	4	21,336	58 N	leadow, no	on-grazed,	HSG B		
_		98,135	85 (	Gravel road	ls, HSG B			
1,096,103 64 Weighted Average					verage			
	1,096,103 100.00% Pervious Area				ervious Are	a		
	Tc Length		Slope	Velocity	Capacity	Description		
(min) (feet) (ft/ft) (ft/sec) (cfs)			(ft/sec)	(cfs)				
	193.3	1,214	0.0009	0.10		Lag/CN Method,		
						-		

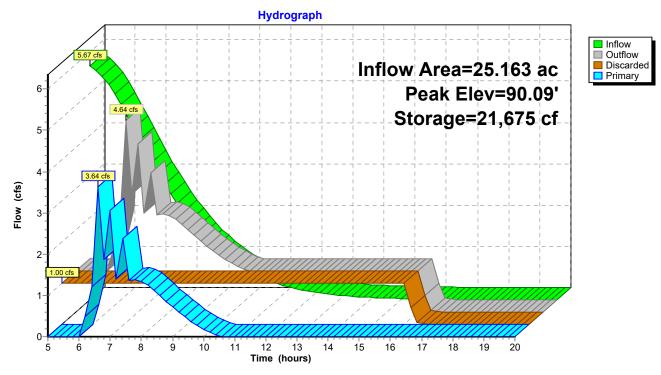
#### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



## Summary for Pond 1P: ROCK LAYDOWN AREA No.1

Inflow Area Inflow Outflow Discarded Primary	= 5.67 c = 4.64 c = 1.00 c	fs @ 5 fs @ 6 fs @ 5	00% Impervious, 5.00 hrs, Volume 5.62 hrs, Volume 5.00 hrs, Volume 5.62 hrs, Volume	e= ^ e= ^	1.352 at	f f, Atten= f	or 100-YR - 4HR. event = 18%, Lag= 96.9 min		
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.09' @ 6.62 hrs Surf.Area= 123,855 sf Storage= 21,675 cf									
	Mass det. time:	= 158.5 m	hin calculated for hin(578.5 - 419	.9)	97% of i	inflow)			
-			age Storage D		(5.1	41 11 1			
#1	89.50'	21,67		Overall x 3			ed below (Recalc)		
			01,920 01		55.070 V	lus			
Elevation	Surf.Ar	ea	Inc.Store	Cum.Sto	ne				
(feet)			(cubic-feet)	(cubic-fee					
89.50		/	0	(00010100	0				
90.00	,		61,928	61,92	•				
30.00	120,0	55	01,920	01,92	20				
Device R	Routing	Invert	Outlet Devices						
-	Primary	89.90'			Broad-	Crester	d Rectangular Weir		
<i>"</i> ····	liniary	00.00	Head (feet) 0.2						
			Coef. (English)				2		
#2 D	Discarded	89.50'					<b>a</b> Phase-In= 0.01'		
<b>Discarded OutFlow</b> Max=1.00 cfs @ 5.00 hrs HW=89.54' (Free Discharge) <b>1 −2=Exfiltration</b> (Exfiltration Controls 1.00 cfs)									

**Primary OutFlow** Max=3.47 cfs @ 6.62 hrs HW=90.08' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 3.47 cfs @ 1.19 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

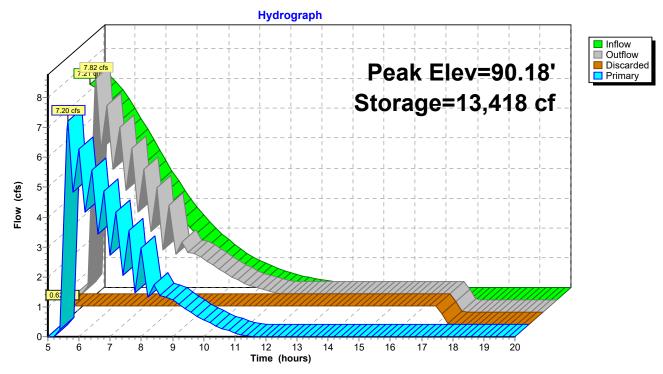
Inflow	=	7.21 cfs @	5.00 hrs, Volume=	1.721 af
Outflow	=	7.82 cfs @	5.65 hrs, Volume=	1.721 af, Atten= 0%, Lag= 39.2 min
Discarded	=	0.62 cfs @	5.00 hrs, Volume=	0.634 af
Primary	=	7.20 cfs @	5.65 hrs, Volume=	1.087 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.18' @ 5.60 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 110.6 min calculated for 1.666 af (97% of inflow) Center-of-Mass det. time= 92.0 min ( 511.9 - 419.9 )

Volume	Invert	Avail.Stor	rage Storage	Description		
#1	89.50'	13,41		<b>Stage Data (Pr</b> of Overall x 35.0		below (Recalc)
Elevatio (fee		f.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
89.5	50 7	6,672	0	0		
90.0	00 7	6,672	38,336	38,336		
Device	Routing	Invert	Outlet Device	S		
#1	Primary	89.90'	Head (feet) 0	<b>0.5' breadth Bro</b> 0.20 0.40 0.60 ( n) 2.80 2.92 3.0	0.80 1.00	Rectangular Weir
#2	Discarded	89.50'				Phase-In= 0.01'
	Discarded OutFlow Max=0.62 cfs @ 5.00 hrs HW=89.59' (Free Discharge) <sup>●</sup> —2=Exfiltration (Exfiltration Controls 0.62 cfs)					

Primary OutFlow Max=6.33 cfs @ 5.65 hrs HW=90.17' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 6.33 cfs @ 1.47 fps)



# Pond 2P: ROCK LAYDOWN AREA No.2

#### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	Depth > 0.72" for 100-YR - 4HR. event
Inflow =	7.06 cfs @	6.59 hrs, Volume=	1.502 af
Outflow =	1.72 cfs @	9.18 hrs, Volume=	1.502 af, Atten= 76%, Lag= 155.1 min
Discarded =	1.72 cfs @	9.18 hrs, Volume=	1.502 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 87.68' @ 9.18 hrs Surf.Area= 212,022 sf Storage= 38,334 cf

Plug-Flow detention time= 224.8 min calculated for 1.502 af (100% of inflow) Center-of-Mass det. time= 224.2 min ( 656.0 - 431.8 )

Volume	Invert	Avail.Sto	rage Storage	e Description		
#1	87.50'	541,13	32 cf Custor	n Stage Data (Pı	<b>'ismatic)</b> Listed below (Recalc)	
Elevatio (fee 87.5 88.0 89.0 90.0	et) 50 2 00 2 00 2	urf.Area (sq-ft) 211,274 213,338 217,483 221,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132		
Device	Routing	Invert	Outlet Device	es		
#1	Discarded	87.50'			Surface area Phase-In= 0.01'	
#2	Primary	88.50'	<b>43.6 deg x 5</b> Cv= 2.56 (C=	•	rise Sharp-Crested Vee/Trap Weir	
Discard	<b>Discarded OutFlow</b> Max=1 72 cfs $@$ 9.18 brs HW=87.68' (Free Discharge)					

**Discarded OutFlow** Max=1.72 cfs @ 9.18 hrs HW=87.68' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.72 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir(Controls 0.00 cfs)

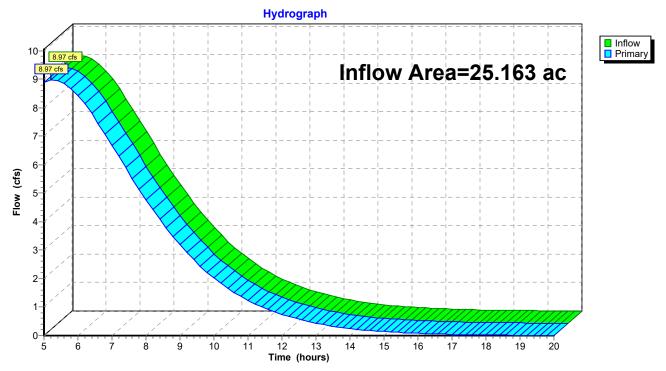
Hydrograph InflowOutflow Discarded
 Primary Inflow Area=25.163 ac Peak Elev=87.68' 7 Storage=38,334 cf 6 5 Flow (cfs) 4 3-1.72 cfs 2 1 0.0 0-5 6 ź 8 ģ 10 11 12 14 15 16 17 18 19 20 13 Time (hours)

# Pond 3P: PROPOSED POND

# Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Are	a =	25.163 ac,	0.00% Impervious, Inflow De	epth > 1.32" for 100-YR - 4HR. event
Inflow	=	8.97 cfs @	5.20 hrs, Volume=	2.763 af
Primary	=	8.97 cfs @	5.20 hrs, Volume=	2.763 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

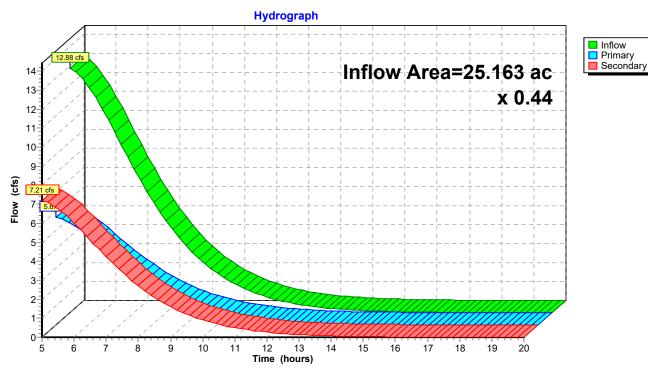


# Link 1L: EXISTING OUTFALL LOCATION

# Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow Depth > 1.47" for 100-YR - 4HR. event	
Inflow =	12.88 cfs @	5.00 hrs, Volume= 3.073 af	
Primary =	5.67 cfs @	5.00 hrs, Volume= 1.352 af, Atten= 56%, Lag= 0.0 min	
Secondary =	7.21 cfs @	5.00 hrs, Volume= 1.721 af	

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



# Link 2L: POST DEVELOPED FLOW

Staging Area 3 HydroCAD Report Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36" Prepared by HP Inc. Printed 3/16/2020 HydroCAD® 10.00-25 s/n 11141 © 2019 HydroCAD Software Solutions LLC Page 102

> Time span=5.00-20.00 hrs, dt=0.20 hrs, 76 points Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: PRE DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>2.62" Flow Length=1,711' Slope=0.0016 '/' Tc=222.3 min CN=58 Runoff=11.56 cfs 5.495 af Subcatchment2S: POST DEVELOPED Runoff Area=1,096,103 sf 0.00% Impervious Runoff Depth>3.22" Flow Length=1,214' Slope=0.0009 '/' Tc=193.3 min CN=64 Runoff=16.18 cfs 6.751 af Peak Elev=90.24' Storage=21,675 cf Inflow=7.12 cfs 2.971 af Pond 1P: ROCK LAYDOWN AREANo.1 Discarded=1.00 cfs 1.204 af Primary=9.30 cfs 1.767 af Outflow=10.30 cfs 2.971 af Peak Elev=90.28' Storage=13,418 cf Inflow=9.06 cfs 3.781 af Pond 2P: ROCK LAYDOWN AREANo.2 Discarded=0.62 cfs 0.780 af Primary=10.91 cfs 2.983 af Outflow=11.53 cfs 3.763 af Peak Elev=88.26' Storage=161,133 cf Inflow=15.24 cfs 4.749 af Pond 3P: PROPOSED POND Discarded=1.74 cfs 2.039 af Primary=0.00 cfs 0.000 af Outflow=1.74 cfs 2.039 af Link 1L: EXISTING OUTFALL LOCATION Inflow=11.56 cfs 5.495 af Primary=11.56 cfs 5.495 af

> x 0.44 Inflow=16.18 cfs 6.751 af Primary=7.12 cfs 2.971 af Secondary=9.06 cfs 3.781 af

Link 2L: POST DEVELOPED FLOW

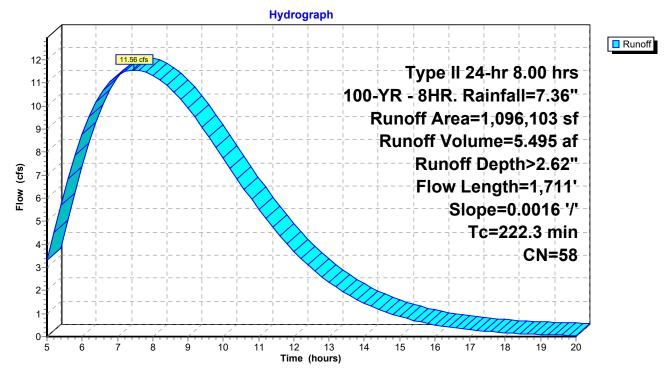
## Summary for Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1

Runoff = 11.56 cfs @ 7.46 hrs, Volume= 5.495 af, Depth> 2.62"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

Are	ea (sf)	CN D	<b>Description</b>				
1,09	6,103	58 N	Meadow, non-grazed, HSG B				
1,09	6,103	1	00.00% Pe	ervious Are	ea		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
222.3	1,711	0.0016	0.13		Lag/CN Method,		

#### Subcatchment 1S: PRE DEVELOPED DRAINAGE AREA 1



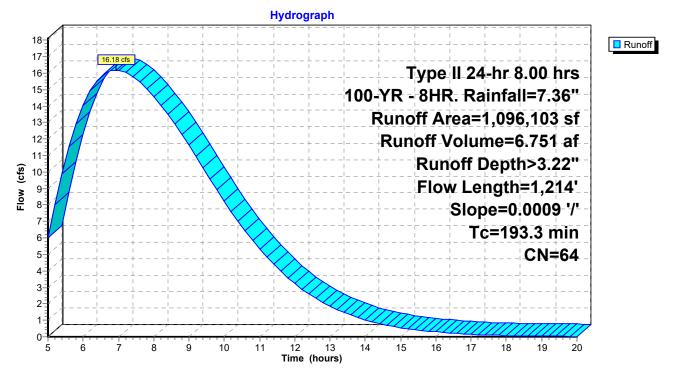
### Summary for Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1

Runoff = 16.18 cfs @ 6.94 hrs, Volume= 6.751 af, Depth> 3.22"

Runoff by SCS TR-20 method, UH=Georgia-323, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Type II 24-hr 8.00 hrs 100-YR - 8HR. Rainfall=7.36"

_	A	rea (sf)	CN E	Description				
*	5	76,632	65 L	Jncompact	ed Gravel(	35% Void Ratio)		
	4	21,336	58 N	Meadow, non-grazed, HSG B				
_		98,135	85 (	Gravel roads, HSG B				
	1,096,103 64 Weighted Average			Veighted A	verage			
	1,096,103 100.00% Per		ervious Are	a				
	_		~		•			
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	193.3	1,214	0.0009	0.10		Lag/CN Method,		

#### Subcatchment 2S: POST DEVELOPED DRAINAGE AREA 1



# Summary for Pond 1P: ROCK LAYDOWN AREA No.1

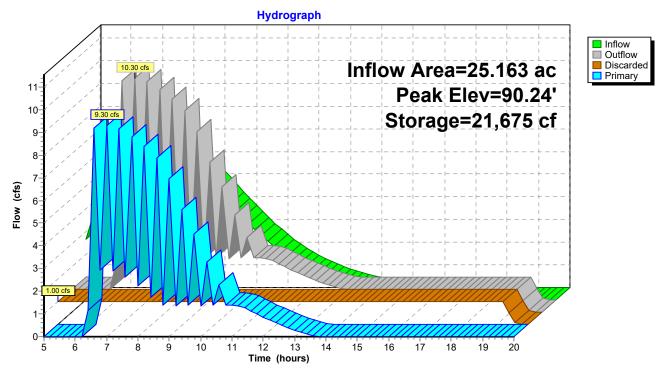
Inflow Area = Inflow = Outflow = Discarded = Primary =	25.163 ac, 7.12 cfs @ 10.30 cfs @ 1.00 cfs @ 9.30 cfs @	6.94 hrs 7.00 hrs 5.00 hrs	pervious, s, Volume: s, Volume: s, Volume: s, Volume: s, Volume:	= 2.9 = 2.9 = 1.20	71 af	for 100-YR - 8HR. event en= 0%, Lag= 3.7 min	
• •	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.24' @ 7.00 hrs Surf.Area= 123,855 sf Storage= 21,675 cf						
Plug-Flow detention time= 104.2 min calculated for 2.918 af (98% of inflow) Center-of-Mass det. time= 102.4 min(600.1 - 497.8)							
Volume Ir	nvert Avail.	Storage S	Storage De	escription			
#1 89	9.50' 2´			a <b>ge Data (P</b> i )verall x 35.0		Listed below (Recalc)	
Elevation	Surf.Area	Inc.S	Store	Cum.Store			

	Sull.Alea	110.01016	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
89.50	123,855	0	0
90.00	123,855	61,928	61,928

Device	Routing	Invert	Outlet Devices
#1	Primary	89.90'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Discarded	89.50'	0.350 in/hr Exfiltration over Surface area Phase-In= 0.01'

**Discarded OutFlow** Max=1.00 cfs @ 5.00 hrs HW=89.51' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 1.00 cfs)

**Primary OutFlow** Max=9.29 cfs @ 7.00 hrs HW=90.24' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 9.29 cfs @ 1.69 fps)



# Pond 1P: ROCK LAYDOWN AREA No.1

#### Summary for Pond 2P: ROCK LAYDOWN AREA No.2

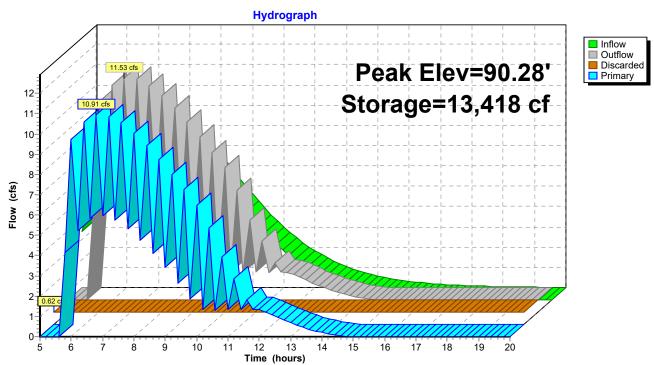
Inflow =	9.06 cfs @	6.94 hrs, Volume=	3.781 af
Outflow =	11.53 cfs @	6.80 hrs, Volume=	3.763 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.62 cfs @	5.00 hrs, Volume=	0.780 af
Primary =	10.91 cfs @	6.80 hrs, Volume=	2.983 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 90.28' @ 6.80 hrs Surf.Area= 76,672 sf Storage= 13,418 cf

Plug-Flow detention time= 56.6 min calculated for 3.691 af (98% of inflow) Center-of-Mass det. time= 53.5 min (551.3 - 497.8)

Volume	Invert	Avail.Stor	age Storage	Description			
#1	89.50'	13,41		Stage Data (Prismatic)Listed b Overall x 35.0% Voids	elow (Recalc)		
Elevatio (fee		.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
89.5	50 7	6,672	0	0			
90.0		6,672	38,336	38,336			
Device	Routing	Invert	Outlet Devices				
#1	Primary	89.90'	•	.5' breadth Broad-Crested Re	ctangular Weir		
			( )	20 0.40 0.60 0.80 1.00 ) 2.80 2.92 3.08 3.30 3.32			
#2	Discarded	89.50'		filtration over Surface area F	hase-In= 0.01'		
<b>Discarded OutFlow</b> Max=0.62 cfs @ 5.00 hrs HW=89.54' (Free Discharge) <b>2=Exfiltration</b> (Exfiltration Controls 0.62 cfs)							

Primary OutFlow Max=10.88 cfs @ 6.80 hrs HW=90.28' (Free Discharge) ←1=Broad-Crested Rectangular Weir (Weir Controls 10.88 cfs @ 1.79 fps)



# Pond 2P: ROCK LAYDOWN AREA No.2

#### Summary for Pond 3P: PROPOSED POND

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	epth = 2.26" for 100-YR - 8HR. event
Inflow =	15.24 cfs @	7.00 hrs, Volume=	4.749 af
Outflow =	1.74 cfs @	12.37 hrs, Volume=	2.039 af, Atten= 89%, Lag= 322.4 min
Discarded =	1.74 cfs @	12.37 hrs, Volume=	2.039 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

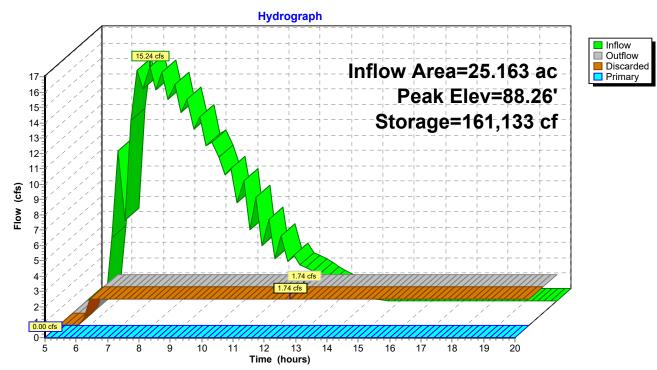
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs Peak Elev= 88.26' @ 12.37 hrs Surf.Area= 214,404 sf Storage= 161,133 cf

Plug-Flow detention time= 360.4 min calculated for 2.012 af (42% of inflow) Center-of-Mass det. time= 275.0 min (779.0 - 504.0)

Volume	Inver	t Avail.Sto	rage Storage	e Description				
#1	87.50	' 541,13	32 cf Custor	n Stage Data (Pı	<b>ismatic)</b> Listed below (Recalc)			
Elevatio (fee 87.5 88.0 89.0 90.0	et) 50 00 00	urf.Area (sq-ft) 211,274 213,338 217,483 221,654	Inc.Store (cubic-feet) 0 106,153 215,411 219,569	Cum.Store (cubic-feet) 0 106,153 321,564 541,132				
Device	Routing	Invert	Outlet Device	es				
#1	Discarded	000			Surface area Phase-In= 0.01'			
#2	Primary	88.50'	<b>43.6 deg x 5</b> Cv= 2.56 (C=		rise Sharp-Crested Vee/Trap Weir			
	0v - 2.00(0 - 0.20)							
Discard	Discarded OutFlow Max=1 74 cfs @ 12 37 brs. HW=88 26' (Free Discharge)							

**Discarded OutFlow** Max=1.74 cfs @ 12.37 hrs HW=88.26' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.74 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=87.50' (Free Discharge) ←2=Sharp-Crested Vee/Trap Weir(Controls 0.00 cfs)

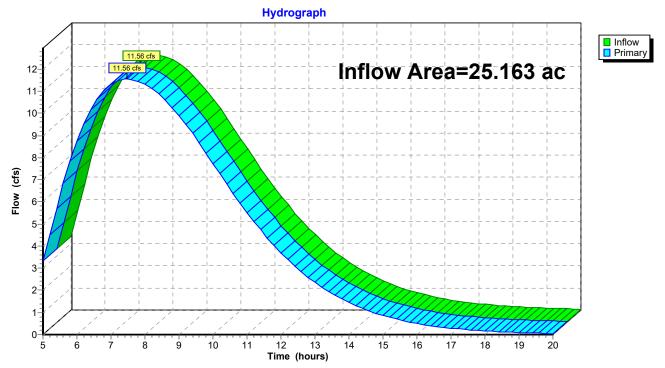


# Pond 3P: PROPOSED POND

# Summary for Link 1L: EXISTING OUTFALL LOCATION

Inflow Are	a =	25.163 ac,	0.00% Impervious, Inflow De	epth > 2.62" for 100-YR - 8HR. event
Inflow	=	11.56 cfs @	7.46 hrs, Volume=	5.495 af
Primary	=	11.56 cfs @	7.46 hrs, Volume=	5.495 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs

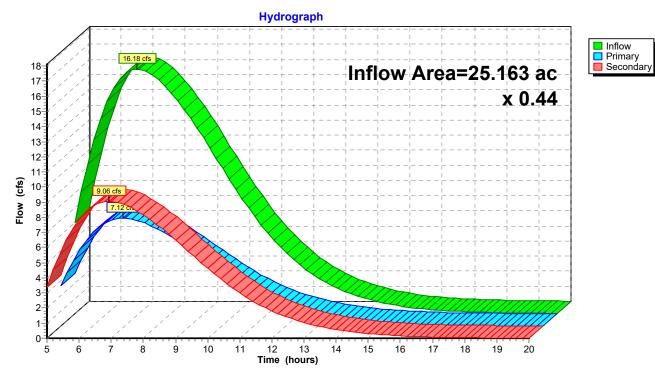


# Link 1L: EXISTING OUTFALL LOCATION

### Summary for Link 2L: POST DEVELOPED FLOW

Inflow Area =	25.163 ac,	0.00% Impervious, Inflow D	Pepth > 3.22" for 100-YR - 8HR. event
Inflow =	16.18 cfs @	6.94 hrs, Volume=	6.751 af
Primary =	7.12 cfs @	6.94 hrs, Volume=	2.971 af, Atten= 56%, Lag= 0.0 min
Secondary =	9.06 cfs @	6.94 hrs, Volume=	3.781 af

Primary outflow = Inflow x 0.44, Time Span= 5.00-20.00 hrs, dt= 0.20 hrs



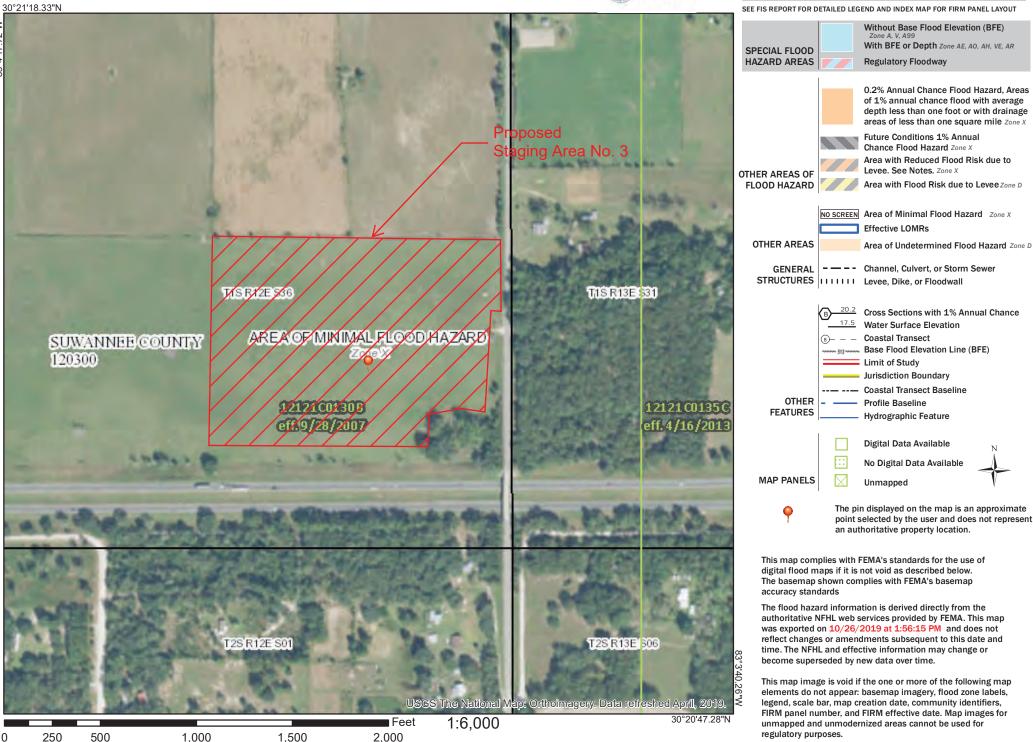
### Link 2L: POST DEVELOPED FLOW

Appendix C – FEMA Firm Map

# National Flood Hazard Layer FIRMette



# Legend



Appendix D – Rainfall Distribution Data

# Appendix D

# **District Rainfall Distribution Data**

# Values for P<sub>total</sub> (inches)<sup>1</sup>

For the counties of Madison, Hamilton, Suwannee, Columbia, Baker and Union.

Frequency	Duration (hours)							
(years)	1	2	4	8	24	72	168	240
3	2.50	2.64	3.08	3.52	4.56	5.80	7.30	8.00
10	3.05	3.70	4.40	5.12	6.72	8.30	10.10	11.80
25	3.45	4.30	5.12	6.00	7.92	10.00	12.30	14.00
100	4.20	5.10	6.08	7.36	9.84	12.40	14.00	16.10

For the counties of Taylor, Lafayette, Dixie, Gilchrist, Levy, Alachua and Bradford.

Frequency	Duration (hours)							
(years)	1	2	4	8	24	72	168	240
3	2.60	3.20	3.80	4.48	6.00	7.60	9.50	10.80
10	3.20	4.00	4.80	5.84	7.92	8.90	11.00	12.50
25	3.60	4.40	5.28	6.56	8.64	11.00	13.00	15.00
100	4.40	5.40	6.72	8.00	11.04	13.80	16.00	18.00

# **1-HOUR DURATION**

T(hrs)	P/P <sub>total</sub>	I/P <sub>total</sub>
0	0	0
.1	.020	.200
.2	.080	.600
.3	.200	1.200
.4	.410	2.100
.5	.625	2.150
.6	.805	1.800
.7	.915	1.100
.8	.985	0.700
.9	.995	0.100
1.0	1.000	0

<sup>&</sup>lt;sup>1</sup> Values for durations through 24 hours were taken from Florida Department of Transportation intensity curves. Values for durations greater than 24 hours were taken from National Weather Service Technical Paper No. 49, 1964.

Appendix E – Water Management District Boundary

# Appendix E

Part VII APPENDICES Appendix



**District Boundary**